

~~TOP SECRET~~
No. [REDACTED]

Copy No. [REDACTED]

CORONA J

PERFORMANCE EVALUATION REPORT

MISSION 1026-1 and 1026-2

FTV 1620; J-25

20 June 1965

Approved:

[REDACTED]
Mgr.

Advanced Projects

Declassified and Released by the NRO

In Accordance with E. O. 12958

on NOV 26 1997

Approved:

[REDACTED]
Mgr.

Program

~~TOP SECRET~~

No. [REDACTED]

~~TOP SECRET~~
NO. [REDACTED]

22 July 1966

To: V. Webb
C. Murphy
A. Johnson
[REDACTED]

Thru: [REDACTED]

From: [REDACTED]

Subject: MISSION 1026-1 AND 1026-2 FINAL REPORT

Enclosed is the Final Performance Evaluation Report for
Mission 1026-1 and 1026-2.

[REDACTED]
Manager
Advanced Projects

ch

~~IF ENCLOSURES ARE WITHDRAWN OR NOT ATTACHED THE CLASSIFICATION
OF THIS DOCUMENT WILL BE CHANGED TO UNCLASSIFIED~~

~~TOP SECRET~~ [REDACTED]

~~TOP SECRET~~

No. [REDACTED]

FOREWORD

This report details the performance of the payload system during the operational phase of the [REDACTED] Flight Test Vehicle 1620.

Lockheed Missiles and Space Company has the responsibility for evaluating payload performance under the Systems Integration and "J" System contracts.

This document is the final payload test and performance evaluation report for Missions 1026-1 and 1026-2 which was launched on 28 October 1965.

~~TOP SECRET~~ [REDACTED]

TOP SECRET

No. [REDACTED]

TABLE OF CONTENTS

	Page
TITLE PAGE	
FOREWORD	i
TABLE OF CONTENTS	ii
LIST OF TABLES	iii
LIST OF ILLUSTRATIONS	iv
INTRODUCTION	1
SECTION 1 - SYSTEM PERFORMANCE	2
SECTION 2 - PRE-FLIGHT SYSTEMS TEST	6
SECTION 3 - FLIGHT OPERATIONS	17
SECTION 4 - MISSION 1026-1 RECOVERY SYSTEM	27
SECTION 5 - MISSION 1026-2 RECOVERY SYSTEM	31
SECTION 6 - MASTER (FWD) PANORAMIC CAMERA	31
SECTION 7 - SLAVE (AFT) PANORAMIC CAMERA	34
SECTION 8 - PANORAMIC CAMERA EXPOSURE	36
SECTION 9 - DIFFUSE DENSITY MEASUREMENTS	49
SECTION 10 - PERFORMANCE MEASUREMENTS	52
SECTION 11 - OBSERVED DATA	53
SECTION 12 - MISSION 1026-1 STELLAR-INDEX CAMERA	54
SECTION 13 - MISSION 1026-2 STELLAR-INDEX CAMERA	56
SECTION 14 - VEHICLE ATTITUDE	57
SECTION 15 - IMAGE SMEAR ANALYSIS	70
SECTION 16 - RADIATION DOSAGE	84
SECTION 17 - RELIABILITY	85
SECTION 18 - SUMMARY DATA	89
SECTION A - APPENDIX	95

TOP SECRET

LIST OF TABLES

Table		Page
2-1	J-25 TASC Pan Cycle Rates	9
3-1	Engineering Operations Cycle Rates	19
3-2	Clock/System Time Correlation	21
3-3 & 3-4	Mission Temperature Summary	22-23
4-1	Mission 1026-1 Recovery Sequence	28
5-1	Mission 1026-2 Recovery Sequence	30
9-1	Processing - Exposure Summary	51
15-1	Mission 1026 V/h Ratio and Resolution Limits	71
17-1	Estimated Reliability Summary	92
18-1	Mission Summary	99
18-2	Performance Summary	100
18-3	Exposure - Processing Summary	93
A-1	Mission 1026-1 FWD Camera Density Distribution	A1 - A6
A-2	Mission 1026-1 AFT Camera Density Distribution	A16 - A21
A-3	Mission 1026-2 FWD Camera Density Distribution	A31 - A36
A-4	Mission 1026-2 AFT Camera Density Distribution	A46 - A51

LIST OF ILLUSTRATIONS

Figure		Page
● -1	Mission 1026 Inboard Profile	3
2-1	Pan Camera TASC Temperature	13
2-2	Master Camera Pre-Flight Resolution	14
2-3	Slave Camera Pre-Flight Resolution	15
3-1 to 3-3	System Temperatures Predicted vs Actual	24-26
8-1	Mission 1026-1 Solar Elevations	37
8-2	Mission 1026-1 Solar Azimuth	38
8-3	Mission 1026-2 Solar Elevations	39
8-4	Mission 1026-2 Solar Azimuth	40
8-5 to 8-12	Nominal Exposure Points	41-48
14-1 to 14-6	Mission 1026-1 Attitude Angle & Rate Error Distributions	58-63
14-7 to 14-12	Mission 1026-2 Attitude Angle & Rate Error Distributions	64-69
15-1 to 15-6	Mission 1026-1 V/h Error & Resolution Limits Distribution	72-77
15-7 to 15-12	Mission 1026-2 V/h Error & Resolution Limits Distribution	78-83
A-1 to A-9	Mission 1026-1 FWD Camera Density Distribution	A7 - A15
A-10 to A-18	Mission 1026-1 AFT Camera Density Distribution	A22 - A30
A-19 to A-27	Mission 1026-2 FWD Camera Density Distribution	A37 - A45
A-28 to A-36	Mission 1026-2 AFT Camera Density Distribution	A52-- A60

TOP SECRET [REDACTED]

No. [REDACTED]

INTRODUCTION

This report presents the final performance evaluation of Missions 1026-1 and 1026-2 of the Corona Program. The purpose of this report is to define the performance characteristics of the J-25 payload system and to identify the source of in-flight anomalies.

The performance evaluation was jointly conducted by representatives of Lockheed Missiles and Space Company (LMSC) and ITEK at the facilities of NPIC and AFSPPF. The off-line evaluation using Corona engineering photography acquired over the United States was performed at the individual contractors plants.

The quantitative data used for this report is obtained from government organizations. The diffuse density data, and MTF/AIM resolution are produced by AFSPPF. The vehicle attitude error values and correlation times are made at NPIC who also supply the Processing Summary and MTF/AIM resolution reports published [REDACTED]

Computer programs developed by A/P are utilized to calculate and plot the frequency distribution of the various contributors to image smear to permit analysis and correlation of the conditions of photography to the information content and quality of the acquired pictures. Computer analysis of the exposure, processing and illumination data provides the necessary data to analyze the exposure criteria selected for the mission.

TOP SECRET [REDACTED]

SECTION I

SYSTEM PERFORMANCE

A. MISSION OBJECTIVES

The payload section of Mission 1026, placed into orbit by Flight Test Vehicle #1620 and LV-2A booster #439, consisted of two panoramic cameras, two Stellar-Index cameras, two Mark 5A recovery capsules and a space structure to enclose the cameras and provide mounting surfaces for all equipments. Figure 1-1 presents an inboard profile of the J-25 payload system. This Corona "J" system is designed to acquire search and reconnaissance photography of selected areas of the earth from orbital altitudes. The planned mission was two, 5 day photographic periods with no deactivate period.

B. MISSION DESCRIPTION

The payload was launched from Vandenberg Air Force Base (VAFB) at 2117:12 Z (1417:12 PDT) on 28 October 1965. Ascent and injection were normal and the achieved orbit was within nominal tolerances. Tracking and command support was effected by the Air Force Satellite Control Facility consisting of tracking and command stations at [REDACTED]

[REDACTED] under central control of the Satellite Test Center at Sunnyvale, California. Mission 1026-1 consisted of a 5 day operation and was completed by air recovery on 2 November 1965. Mission 1026-2 was completed with an air recovery on 7 November 1965 following a 5 day photographic operation.

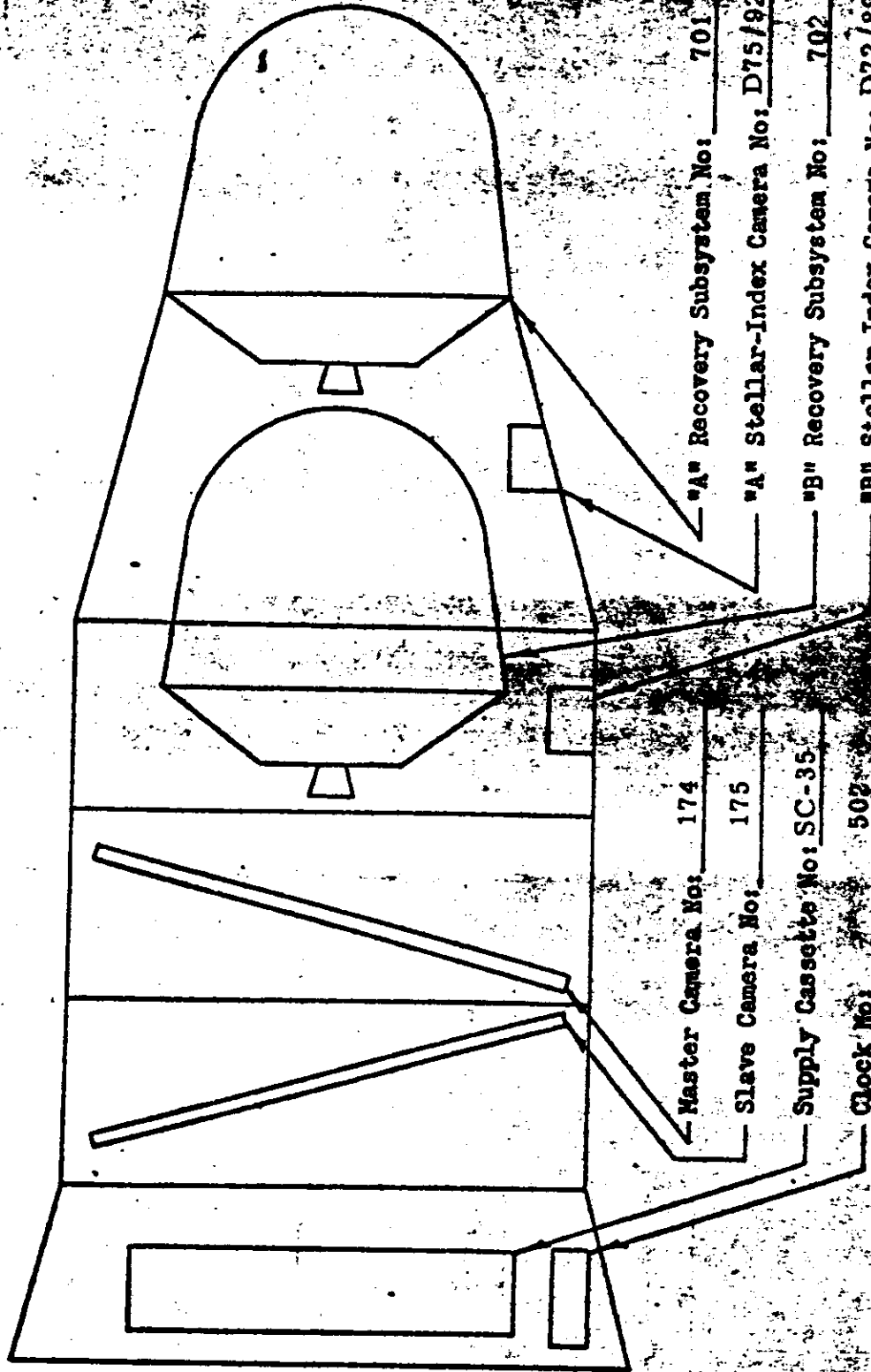
The comparison of the planned and actual orbit parameters is tabulated as follows:

TOP SECRET

No. [REDACTED]

SCHEMATIC INBOARD PROFILES - CORONA J SYSTEM

MISSION 1026



Pressure Make-up Unit No: 1015

TOP SECRET

No. [REDACTED]

ORBITAL PARAMETERS

<u>Parameter</u>	<u>Predicted</u>	<u>Orbit 1 Actuals</u>
Period (Min.)	90.72	90.77
Perigee (N. M.)	99.8	95.12
Apogee (N. M.)	238.1	240.6
Inclination (Deg.)	75.00	74.98
Perigee Latitude (Deg. N.)	23.00	10.05
Eccentricity	0.0192	0.02041

C. PANORAMIC CAMERAS

The Master instrument operated normally through both missions. The photo quality suffered from heavy haze, low sun elevations and 50% cloud cover.

The Slave instrument photo quality was rated as being slightly better than the Master. The center of format switch operated intermittently from pass D-24 thru D-70.

The horizon cameras on the sun side of the vehicle exhibited veiling on both missions.

D. STELLAR-INDEX CAMERAS

The "A" S/I produced star imagery adequate to determine the vehicle attitude. Four stellar frames were affected by shutter malfunction. The index camera produced no anomalies.

The "B" S/I camera operation is rated as excellent.

E. OTHER SUB-SYSTEMS

The clock, instrumentation, command and thermal control subsystems performed satisfactorily.

TOP SECRET

No. [REDACTED]

F. CONCLUSIONS

Mission 1026 achieved its objective of search and reconnaissance, however atmospheric conditions obscured some target areas.

TOP SECRET [REDACTED]

TOP SECRET

No. [REDACTED]

SECTION 2

PRE-FLIGHT SYSTEMS TESTS

A. ENVIRONMENTAL TESTING

1. Test Objective

As a standard procedure, the J payload systems are subjected to thermal/altitude environmental testing which simulates orbital environment. One of the purposes of this test is to demonstrate the system susceptibility to corona discharge. Such discharge fogs the film thus degrading the operational photography.

2. Test Summary

The J-25 payload system was subjected to an environmental TASC Chamber test from July 10 through July 17, 1965. The environmental test consisted of 13 orbits in the "B" mode. The payload was removed from the chamber on two occasions as a result of two fail-safes. This was done between orbit 13 in the "A" mode and the "A" recovery sequence.

Panoramic camera #1 experienced erratic payload metering, cycle period in excess of the 2.15 sec. maximum at one point, cycle rate errors ranging from 1.9% fast to 2.9% slow, and two fail-safes.

Instrument #2 performance was satisfactory except the cycle rate errors ranged from 0 to 4.5% slow in the "A" mode and 0.4% to 2.6% slow in the "B" mode.

The stellar/index camera performance was satisfactory throughout both the "A" and "B" mode of operation.

The clock performance was out of allowable offset limits.

The instrumentation system performance was satisfactory with the exception of several noisy idler commutators and Sanborn channel setup discrepancies.

TOP SECRET [REDACTED]

TOP SECRET

No. [REDACTED]

The PMU system operation was satisfactory with the average gas depletion rate being somewhat higher than normal.

The temperature environment was cold for the "A" mode and near 70° for the "B" mode.

3. Panoramic Camera Performance

Instrument #1 performance disclosed the following problems:

- a. Erratic metering in the "A" mode.
- b. Cycle rate predictability exceeded the 1% specification limit in the "A" mode.
- c. Two fail-safes occurred in the "A" mode and the payload was pulled out of the rails.
- d. Cycle period exceeded the maximum limit of 2.15 sec. on one operation.

Payload metering was erratic as observed on the takeup idler. Uneven payload motion was also indicated on the supply idler monitor. On orbit 2, "B" mode, the cycle period exceeded the maximum allowable of 2.15 secs. This occurred at 2130 seconds up the ramp of R4A1 and was 1.9% faster than predicted. A cycle period was obtained in orbit 2, "A" mode, which was within 1% of the predicted cycle period.

The instrument had two fail-safes during the test. The first occurred near the end of orbit 13 during the mono portion of a stereo surpress operation. The chamber was brought to atmospheric pressure and the system was inspected and no anomalies were detected. The system was reinstalled in the environmental chamber and the test was restarted at orbit 12 of the "A" mode. Fail-safe occurred again during the stereo portion of the stereo surpress operation in orbit 13. The system was again removed from the chamber. The master instrument film was found to be out of the rails and the takeup cassettes of the "A" SRV was found to be rubbing. Erratic payload metering was evident on both instruments prior to each fail-safe. The system

TOP SECRET [REDACTED]

was transferred to the "B" mode by performing a cut and wrap recovery sequence. A confidence run was made and the system reinstalled in the chamber. Instrument #1 completed the test without further problems.

Instrument #2 performance was satisfactory except cycle rate errors ranged from 0 to 4.5% slow in the "A" mode and 0.4 to 2.6% slow in the "B" mode. The chamber temperature was low in the "A" mode and more nearly normal in the "B" mode. Analysis is continuing to establish the degree of correlation, if any, between cycle rate error and temperature.

The supply cassette rotation monitor indicated supply cassette rotation in the latter half of the "B" mode of operation.

A tabulation of cycle rate data from the chamber test is included as Table 2-1.

4. Stellar/Index Performance

Both the "A" and the "B" stellar/index cameras performed properly throughout the test. The "A" index idler T/M was noisy.

5. Clock Performance

The clock offset was 1 millisecond per hour in both the "A" and "B" mode when compared to IRIG C. This exceeds the offset limit of 2 milliseconds per 12 hours.

6. Instrumentation Performance

Instrumentation performance throughout the test was satisfactory. Minor problems such as improper Sanborn calibrations and noisy idler contacts occurred.

The status commutator and temperature commutator has no open points.

The film footage pots and cycle counters showed good correlation throughout the test. †

J-25 TASC CHAMBER TEST NO 1 TEST CYCLE RATES

REV/MODE	RAMP	T.U.R.	INST 174			INST 175			174/175 DIFF.
			ACT.	SEEK CALIB.	DEV.	ACT.	SEEK CALIB.	DEV.	
0 A	8 2	0	5.570	5.479	-1.66	5.600	5.539	-1.10	0.54
1 A	7 7	400	3.525	3.494	-0.90	3.520	3.489	-0.88	-0.14
2 A	4 1	1430	2.190	2.216	1.18				
2 A	4 1	1610				2.208	2.207	-0.07	
2 A	4 1	2130	2.170	2.189	0.89	2.200	2.200	0.01	1.38
3 A	5 8	730	2.893	2.879	-0.48	2.887	2.869	-0.61	-0.21
3 A	5 8	1550	2.458	2.446	-0.47	2.460	2.437	-0.95	0.08
4 A	7 7	2280	2.580	2.559	-0.83	2.580	2.549	-1.22	-0.95
5 A	8 2	340	5.130	5.076	-1.07	5.178	5.117	-1.19	0.95
6 A	5 8	1090	2.733	2.693	-1.47	2.753	2.683	-2.60	0.73
6 A	5 8	1440	2.518	2.493	-1.01	2.535	2.483	-2.09	0.68
7 A	7 7	1180	2.927	2.875	-1.81	2.957	2.865	-3.21	1.02
7 A	7 7	1590	2.610	2.562	-1.86	2.627	2.552	-2.92	0.65
8 A	7 7	2530	2.767	2.723	-1.63	2.793	2.713	-2.97	0.94
9 A	4 1	1015	2.767	2.743	-0.86	2.823	2.733	-3.29	2.02
9 A	4 1	3200	3.500	3.405	-2.78	3.540	3.400	-4.13	1.14
9 A	11 1	890	4.585	4.459	-2.82	4.680	4.477	-4.53	2.07
10 A	11 1	1880	2.283	2.271	-0.53	2.320	2.263	-2.54	1.62
10 A	11 1	2970	4.470	4.384	-1.95	4.560	4.400	-3.64	2.01

TABLE 2-1

REV/MODE	RAMP	T.U.R.	INST-174			INST 175			174/175 DIFF.	
			ACT.	MM. CALIB.	DEV.	ACT.	MM. CALIB.	DEV.		
10	A	7 7	130	3.700	3.598	-2.83	3.760	3.595	-4.58	1.62
11	A	7 7	1910	2.527	2.476	-2.05	2.550	2.467	-3.38	0.91
11	A	7 7	2270	2.603	2.554	-1.92	2.630	2.544	-3.37	1.04
12	A	8 2	1045	3.263	3.229	-1.04	3.333	3.222	-3.45	2.15
12	A	8 2	1850				2.265	2.229	-1.60	
13	A	8 2	835	3.785	3.726	-1.58	3.870	3.726	-3.88	2.25
13	A	4 1	2625	2.390	2.336	-2.30	2.420	2.327	-3.98	1.26
	A	11 1	1755	2.385	2.319	-2.86	2.350	2.310	-1.74	-1.47
1	B	7 7	390	3.523	3.499	-0.68	3.575	3.495	-2.29	1.48
2	B	4 1	2130	2.148	2.189	1.89	2.218	2.200	-0.81	3.26
2	B	5 8	730	2.875	2.879	0.15	2.893	2.869	-0.82	0.63
3	B	5 8	1550	2.440	2.446	0.26	2.468	2.437	-1.27	1.15
4	B	7 7	2380	2.615	2.614	-0.02	2.635	2.604	-1.18	0.76
5	B	8 2	1795	2.178	2.225	2.13				
5	B	8 2	2315				2.318	2.307	-0.46	
5	B	11 1	1460	2.640	2.653	0.47	2.658	2.643	-0.59	0.68
6	B	11 1	2040	2.255	2.282	1.17	2.295	2.273	-0.96	1.77
6	B	5 8	1190	2.613	2.632	0.74	2.637	2.622	-0.56	0.92
6	B	5 8	1545	2.425	2.448	0.95	2.450	2.439	-0.46	1.03
7	B	7 7	1280	2.767	2.780	0.47	2.787	2.770	-0.61	0.72
7	B	7 7	1690	2.505	2.520	0.59	2.520	2.510	-0.40	0.60
8	B	7 7	0	3.630	3.608	-0.61	3.675	3.605	-1.94	1.24

TABLE 2-1

No. [REDACTED]

REV/MODE	RAMP	I.U.R.	INST 174			INST 175			174/175 DIFF.	
			ACT.	ACT. CALIB.	DEV.	ACT.	ACT. CALIB.	DEV.		
8	B	8 2	0	5.490	5.479	-0.20	5.610	5.539	-1.28	2.19
8	B	4 1	1115	2.587	2.581	-0.23	2.613	2.571	-1.63	1.01
9	B	4 1	3410	3.850	3.849	-0.03	3.900	3.851	-1.28	1.30
9	B	11 1	1090	3.690	3.693	0.07	3.745	3.691	-1.45	1.49
10	B	11 1	2080	2.288	2.297	0.39	2.313	2.288	-1.07	1.09
10	B	11 1	3120	5.170	5.114	-1.10	5.290	5.157	-2.59	2.32
10	B	7 7	305	3.570	3.542	-0.79	3.615	3.538	-2.17	1.26
13	B	4 1	2630	2.363	2.344	-0.80	2.375	2.335	-1.69	0.51
13	B	11 1	1975	2.260	2.268	0.34	2.277	2.259	-0.76	0.15

DEV. AND DIFF. ARE IN PERCENT
THE (-) SIGN INDICATES THAT THE INST IS SLOWER THAN
PREDICTED OR THAT INST 1 IS SLOWER THAN INST 2

TABLE 2-1

7. Pressure Make-Up System Performance

The pressure make-up system performed satisfactorily. The gas consumption rate was a little higher than normal at 9.0 psia/minute of operate for the "A" mode. A flow rate check of the system after the test showed the flow rate to be high but within allowable tolerances.

Because of the two chamber dives, the "B" mode chamber pressure did not go below 1 micron.

8. Temperature Summary

The chamber temperatures were cold during the "A" mode and near normal for the "B" mode. Instrument mainplate temperature is shown in Figure 2-1.

B. RESOLUTION TEST

Resolution and theodolite tests were performed on 23 July 1965. Results of the thru-focus resolution tests of pan instruments 174 and 175 show the following characteristics:

Master Pan Instrument No. 174

Maximum high contrast resolution 194 lines/mm at + .001 focal position.

Maximum low contrast resolution 120 lines/mm at + .001 focal position.

Slave Instrument No. 175

Maximum high contrast resolution 194 lines/mm at + .001 focal position.

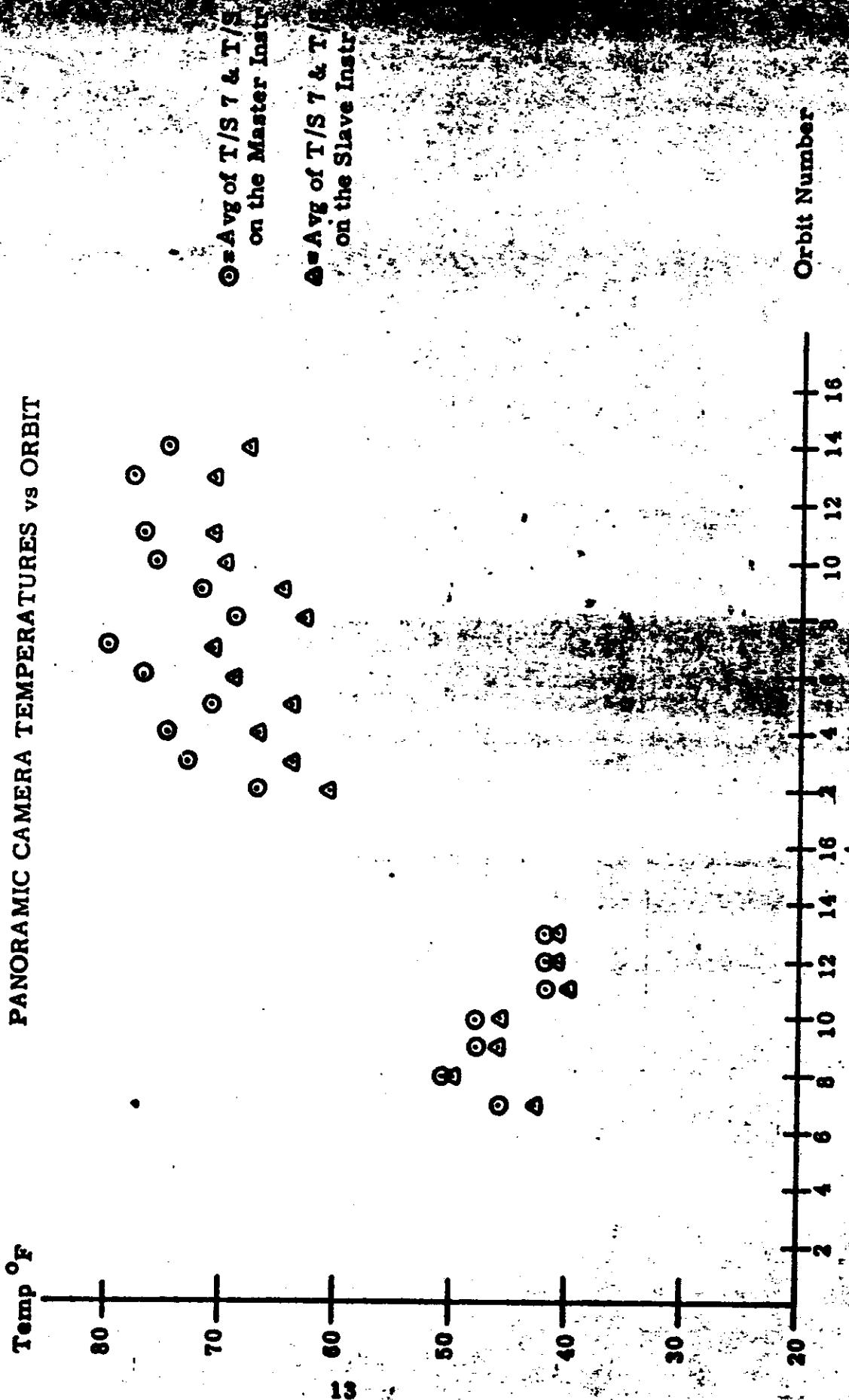
Maximum low contrast resolution 120 lines/mm at + .001 focal position.

The test data for both instruments is shown in Figures 2-2 and 2-3. Both instruments met the system requirements specification.

TOP SECRET

No.

PANORAMIC CAMERA TEMPERATURES vs ORBIT



"A" "B"

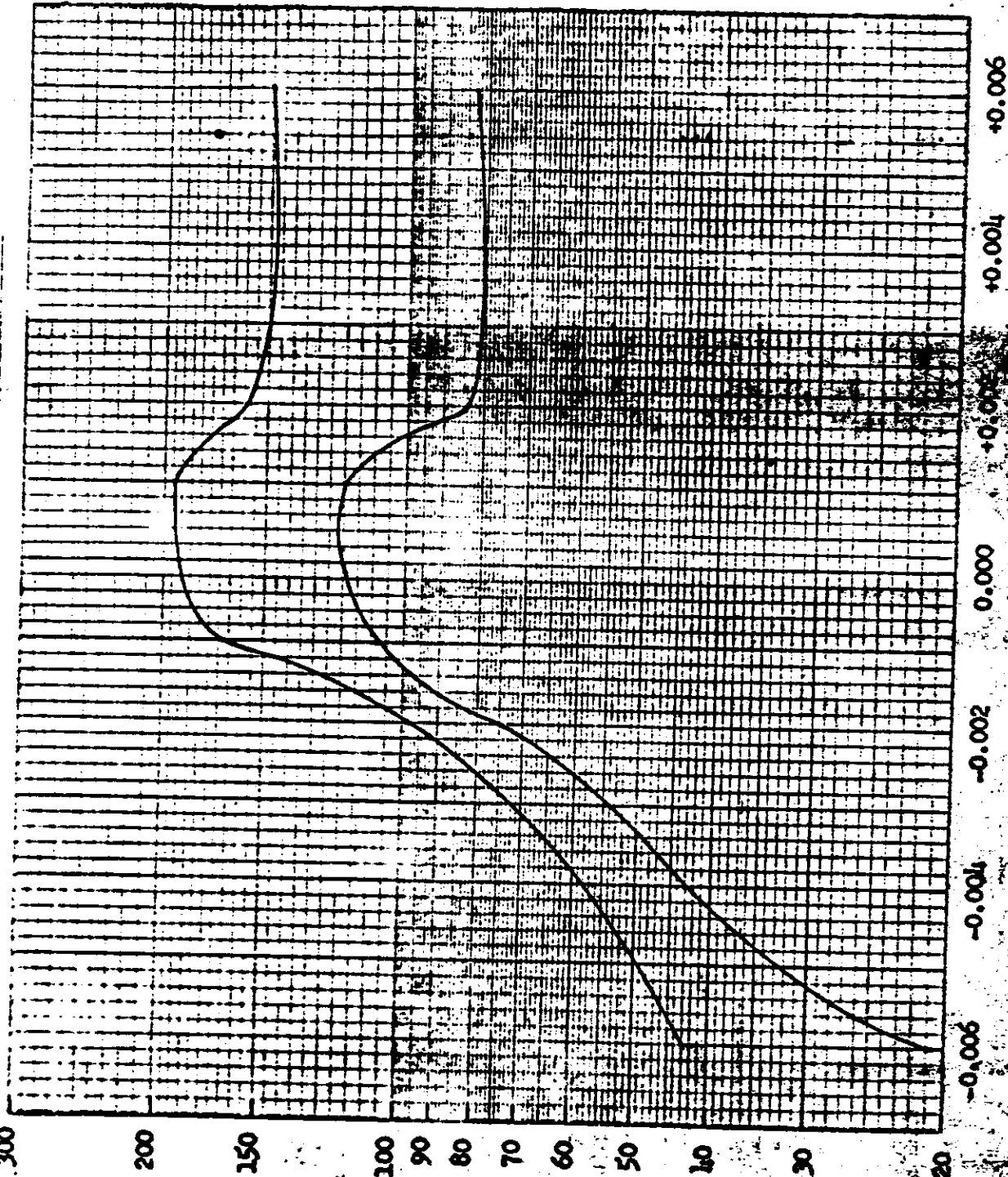
TOP SECRET

FIGURE

TOP SECRET

No.

PRE-FLIGHT DYNAMIC RESOLUTION



PHOTOGRAPHIC RESOLUTION (Lines per Millimeter)

THROUGH FOCUS INCREMENTS (mm)

Camera No: 171

Payload No: J-25

Resolution (1/mm)

High Contrast: 15°

Low Contrast: 0°

Film Type: 3104

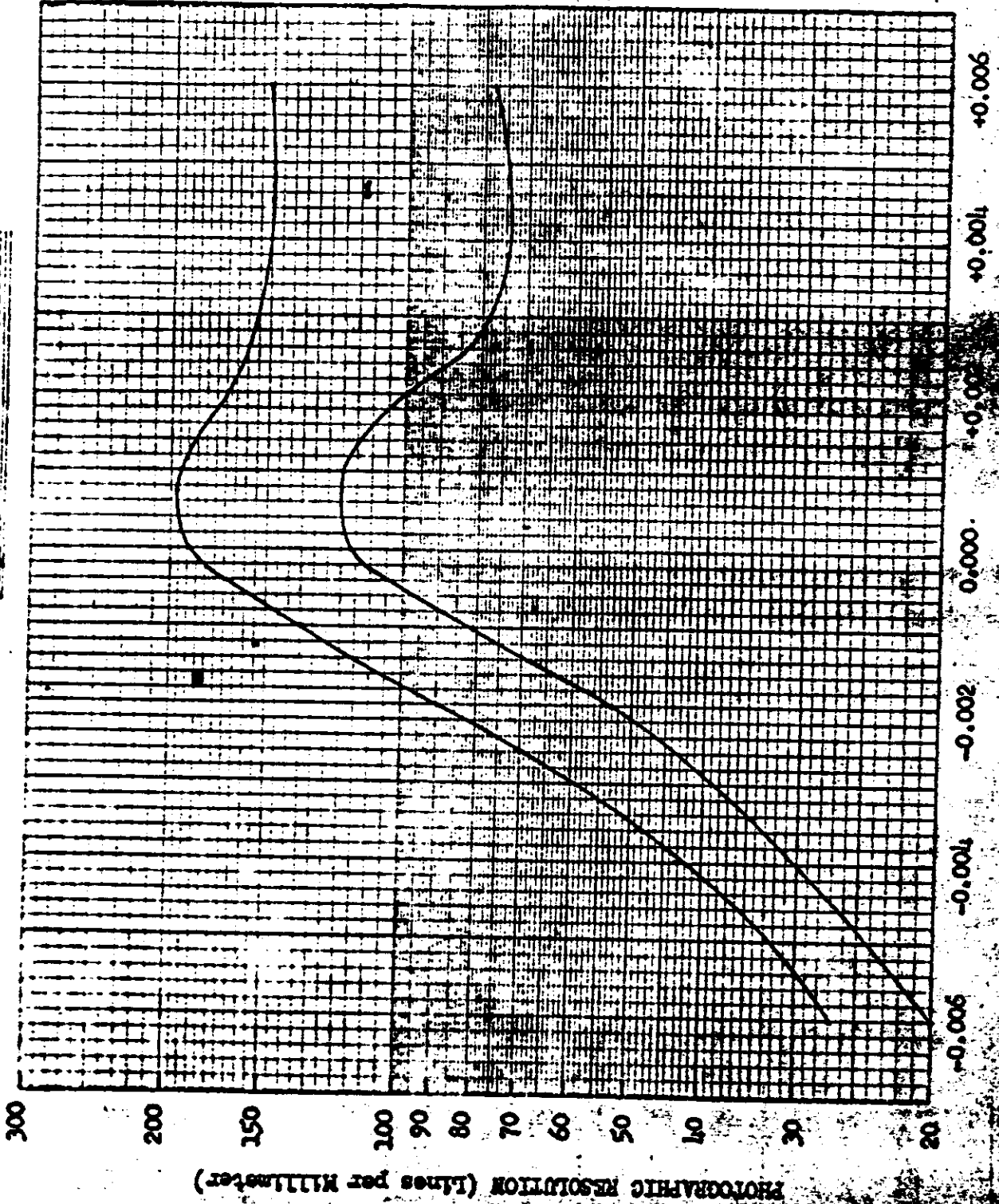
Test Date: 7/23/68

TOP SECRET

TOP SECRET

No.

PRE-FLIGHT DYNAMIC RESOLUTION



PHOTOGRAPHIC RESOLUTION (lines per millimeter)

THROUGH FOCUS INCREMENTS (micrometers)

FIGURE

Camera No: 175
 Payload No: J-25
 Resolution (l/mm): 150
 High Contrast: 150
 Low Contrast: 0°
 Film Type: 3101
 Test Date: 7/23/65

TOP SECRET

~~TOP SECRET~~ [REDACTED]

No. [REDACTED]

C. LIGHT LEAK TEST

The J-25 system was tested for light leaks on 1 September 1965.

A minor light leak fogged three small areas (2 x 1/4 inches each) of the test film in instrument 174 and 175. The first photomultiplier search failed to detect the light leak. The second photomultiplier search located the light leak at the drum/felt seal of the master instrument.

Fog marks measured approximately 0.4 to 0.6 density as a result of the 1/2 hour light leak test and 0.04 density as a result of the 1/4 hour light leak test exposure. The felt seal was inspected to assure a flight acceptable configuration.

D. FLIGHT LOADING AND CERTIFICATION

The J-25 flight readiness test was performed and the resulting pan instrument payload was examined at VAFB on 21 October 1965. The initial readiness test payload showed the master instrument end-of-pass mark to be missing and two minus density streaks due to foreign matter were on the filter. Investigation showed the EOP lamp to be burned out and lint was found on the filter. These items were corrected and the readiness test was re-run. In this test, the condition of the master instrument payload was satisfactory. The slave instrument payload was satisfactory in both tests.

The loading of flight payload into the supply cassette was performed on 25 October 1965. After final system assembly, payload splices and tracking were observed to be normal.

~~TOP SECRET~~ [REDACTED]

SECTION 3

FLIGHT OPERATIONS

A. INSTRUMENTATION AND COMMAND SYSTEM PERFORMANCE

All instrumentation performed satisfactorily throughout the mission with the exception of the fairing temp sensor No. 1. The telemetry monitor indicated an out of band low condition for the duration of Phase I.

Command System Performance

The command system operation was satisfactory throughout both phases of the mission.

Both emergency operate programs (Programs 10 and 11) were utilized on engineering operations during [REDACTED] acquisitions on orbit 167 and 174. All instrument functions operated satisfactory.

The following operational problems were encountered during this mission.

1. A vehicle H-timer reset was issued 100 seconds early on orbit 33 which caused all events on orbit 34 and 35 to occur 100 seconds early.
2. The V/h programmer failed to operate on orbit 88. An RTC 10 command (V/h ramp start delay) was issued on orbit 87 stepping from position 9 to position 8, while brush 27 (V/h programmer start brush) was stepping between position 8 and 9.

B. PANORAMIC CAMERA PERFORMANCE

Both panoramic camera system dynamic operation, 99/101% clutch operation, startup, shutdown, and transport functions were normal for all passes monitored. The slave instrument center of format switch (S-105) failed to close on 37 frames in the -1 mission causing missing data block, horizon optics, blanking pulse and errors in cycle counter readings. The switch closure was observed to fail randomly from D-24 to D-70. There was no reported failure of the switch during the -2 mission.

Cycle periods taken from telemetry data during [REDACTED] acquisition are listed in Table 3-1. The cut and wrap sequence performed satisfactorily.

Panoramic Film Consumption - Frames

These data are based on cycle counters and nominal supply length.

	<u>Nominal</u>	<u>Actual</u>	
		<u>Master</u>	<u>Slave</u>
Preload samples	18	17	17
Prelaunch checkout	100	101	100
-1 Mission	2950	2929	2897*
-2 Mission	2981	3002	3055
TOTAL	6049	6049**	6049**

*Slave counter known to be missing counts, therefore unreliable.

**Depletion was predicted near or during orbit 151 descending.

C. FMC MATCH

In general, FMC was accomplished within the desirable 5% tolerance, although on the slow side. However, driving the system well into the cycle rate limiter was necessitated by perigee displacement (4.7 N.M. low, 13° south); this could produce rates nominally as much as 5% slow for orbit match.

The limiter affected operations for a 30 to 35 degree (latitude) range; between 225° - 305° early in the mission, to between 250° to 215° late in the mission.

Certain operations occurred outside the expected tolerance:

Revs 1 thru 6 - Commanding occurred previous to complete orbit definition; only partial compensation made for perigee shift - errors up to 10%.

Revs 34 and 35 - An intolerable reset on Rev 33 caused all functions to occur 100 sec. early; displacing operations northward and yielding approximately 5 - 6% error for actual photography.

Rev 87 - Due to a command problem, the programmer was not started, yielding very high indicated error for the operation run at the "bottom of the ramp".

J-25/1620 MISSION 1026, ENGINEERING OPERATIONS CYCLES RATES

REV/MODE	RAMP	T.U.R.	INST 174			INST 175			174/175 DIFF.	
			ACT.	CAL.	DEV.	ACT.	CAL.	DEV.		
009	1	7 3	0	4.760	4.755	0.10S	4.765	4.784	0.39F	0.11
016	1	7 3	1554	2.340	2.295	1.97S	2.322	2.286	1.57S	-0.77
031	1	7 3	1625	2.258	2.239	0.85S	2.279	2.240	1.72S	0.93
040	1	7 3	123	4.722	4.725	0.06F	4.755	4.752	0.06S	0.70
047	1	7 3	1630	2.265	2.236	1.31S	2.262	2.240	0.98S	-0.13
063	1	7 3	1659	2.264	2.233	1.39S	2.282	2.238	1.98S	0.80
079	1	7 2	1695	2.233	2.221	0.52S	2.255	2.228	1.22S	0.99
88	2	7 2	252	4.888	4.864	0.49S	4.936	4.896	0.81S	0.98
94	2	7 2	1685	2.240	2.222	0.80S	2.245	2.229	0.74S	0.27
94	2	7 2	1825	2.224	2.214	0.45S	2.240	2.222	0.85S	0.72
103	2	7 2	288	4.845	4.804	0.85S	4.875	4.834	0.84S	0.62
110	2	7 2	1855	2.240	2.213	1.21S	2.240	2.221	0.86S	-0.00
126	2	7 2	1856	2.235	2.213	0.98S	2.244	2.221	1.04S	0.40
142	2	7 2	1850	2.250	2.213	1.66S	2.250	2.221	1.31S	-0.00
158	2	6 3	1925	2.223	2.210	0.58S	2.225	2.218	0.30S	0.09

DEV. AND DIFF. ARE IN PERCENT
THE (-) SIGN INDICATES THAT INST 1 IS SLOWER THAN INST 2
F=FAST AND S=SLOW

TABLE 3-1

~~TOP SECRET~~ [REDACTED]

No. [REDACTED]

D. STELLAR/INDEX CAMERA PERFORMANCE

Both the -1 and -2 Stellar/Index cameras operated properly throughout the mission. Metering was normal on all engineering passes and shutter pulses were present on all daytime operations. The -1 index film was not depleted on orbit 79 [REDACTED] but depleted prior to good T/M on cut and wrap slew operation. The -2 index film was depleted at orbit 158 [REDACTED].

E. CLOCK PERFORMANCE

Clock system performance was normal throughout both phases of the mission. Good time correlation between system time and clock time was obtained. A tabulation of the time correlation data is included in Table 3-2.

F. PRESSURE MAKEUP SYSTEM PERFORMANCE

The pressure makeup system performed satisfactorily throughout both phases of the mission. The average gas consumption was 7.4 lbs/min. for a total operate time of 262 minutes, which compares favorably with previous systems.

G. THERMAL ENVIRONMENT

Tables 3-3 and 3-4 contain the temperature data acquired from the [REDACTED] acquisitions. The actual system temperature versus the predicted system temperature for major components is included in Figure 3-1, 3-2 and 3-3.

~~TOP SECRET~~ [REDACTED]

J-25 MISSION 1026 CLOCK/SYSTEM TIME CORRELATION

SYS TIME I/P		ORDER FIT 1 CL TIME I/P		COMP SYS TM	DELTA ST	REV	STA
0.379451380	05	0.7058127000	04	0.3794513710	05	0.0009	9
0.775228780	05	0.4663587000	05	0.7752288000	05	-0.0020	16
0.331500580	05	0.8866304300	05	0.3315005290	05	0.0051	24
0.727992380	05	0.1283122260	06	0.7279923590	05	0.0021	31
0.337557850	05	0.1756687740	06	0.3375578380	05	0.0012	40
0.732930180	05	0.2152060080	06	0.7329301770	05	0.0003	47
0.341302400	05	0.2624432340	06	0.3413024360	05	-0.0036	56
0.738440770	05	0.3021570690	06	0.7384407850	05	-0.0015	63
0.348531280	05	0.3495661160	06	0.3485312550	05	0.0025	72
0.743516780	05	0.3890646720	06	0.7435168140	05	-0.0034	79
0.353397480	05	0.4364527460	06	0.3533975530	05	-0.0073	88
0.694847580	05	0.4705977480	06	0.6948475720	05	0.0008	94
0.303616680	05	0.5178746570	06	0.3036166620	05	0.0010	103
0.699103610	05	0.2055244200	05	0.6991036310	05	-0.0021	110
0.307714830	05	0.6781355700	05	0.3077147800	05	0.0050	119
0.703024550	05	0.1073445370	06	0.7030245790	05	-0.0029	126
0.310362180	05	0.1544782980	06	0.3103621880	05	-0.0008	135
0.705458780	05	0.1939879590	06	0.7054587980	05	-0.0018	142
0.314430480	05	0.2412851280	06	0.3144304870	05	-0.0007	151
0.708617740	05	0.2807038470	06	0.7086176760	05	0.0064	158

A0= 0.30887010100 05 A1= 0.999999981740 00
 SIGMA=0.00317 NO. POINTS= 20
 RATIO OF CLOCK TIME TO SYS TIME= 0.100000001030 01

SYS TIME I/P		ORDER FIT 2 CL TIME I/P		COMP SYS TM	DELTA ST	REV	STA
0.379451380	05	0.7058127000	04	0.3794513930	05	-0.0013	9
0.775228780	05	0.4663587000	05	0.7752288160	05	-0.0036	16
0.331500580	05	0.8866304300	05	0.3315005390	05	0.0041	24
0.727992380	05	0.1283122260	06	0.7279923630	05	0.0017	31
0.337557850	05	0.1756687740	06	0.3375578370	05	0.0013	40
0.732930180	05	0.2152060080	06	0.7329301720	05	0.0008	47
0.341302400	05	0.2624432340	06	0.3413024280	05	-0.0028	56
0.738440770	05	0.3021570690	06	0.7384407750	05	-0.0005	63
0.348531280	05	0.3495661160	06	0.3485312420	05	0.0038	72
0.743516780	05	0.3890646720	06	0.7435168010	05	-0.0021	79
0.353397480	05	0.4364527460	06	0.3533975400	05	-0.0060	88
0.694847580	05	0.4705977480	06	0.6948475600	05	0.0020	94
0.303616680	05	0.5178746570	06	0.3036166510	05	0.0029	103
0.699103610	05	0.2055244200	05	0.6991036220	05	-0.0012	110
0.307714830	05	0.6781355700	05	0.3077147750	05	0.0055	119
0.703024550	05	0.1073445370	06	0.7030245780	05	-0.0028	126
0.310362180	05	0.1544782980	06	0.3103621920	05	-0.0012	135
0.705458780	05	0.1939879590	06	0.7054588070	05	-0.0027	142
0.314430480	05	0.2412851280	06	0.3144305030	05	-0.0023	151
0.708617740	05	0.2807038470	06	0.7086176990	05	0.0041	158

A0= 0.30887012460 05 A1= 0.9999999802430 00
 A2= 0.21800048741270-13
 SIGMA=0.00295 NO. POINTS= 20

TABLE 8-2

TABLE 3-3

J-25 TEMPERATURE SUMMARY

<u>SENSOR</u>	<u>ORBITS ACQUIRED</u>																		
<u>Master Camera</u>	9	16	24	31	40	47	56	63	72	79	88	94	103	110	119	126	135	142	151
3	78	75	79	76	79	76	77	74	76	74	71	67	68	64	66	64	66	64	67
4	85	81	85	80	85	81	83	80	81	79	79	73	75	69	73	69	73	69	73
5	91	87	91	88	90	87	89	86	87	84	83	78	78	75	77	74	75	74	76
6	92	88	91	89	90	87	88	85	86	84	80	77	76	73	73	72	73	71	71
7	90	87	90	88	89	86	87	85	85	83	80	77	76	74	74	72	73	72	72
8	93	88	93	89	92	87	91	87	89	85	84	80	81	77	79	76	79	75	78
9	95	91	95	91	94	89	92	87	90	85	85	80	81	77	80	75	79	74	78
10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
11	92	89	93	86	90	85	89	84	86	83	73	74	75	71	73	69	72	68	70
12	79	74	79	75	80	75	79	73	77	74	73	67	70	65	69	65	70	65	70
13	85	83	85	82	83	81	82	79	79	78	71	69	69	68	67	66	67	67	65
AVG	88	84	88	85	87	83	86	82	84	81	78	74	72	71	71	70	73	73	71
<u>Slave Camera</u>																			
3	85	83	85	84	84	82	83	78	80	76	74	68	68	64	65	62	64	61	62
4	85	79	84	80	84	80	83	77	82	76	77	69	71	66	69	64	68	63	66
5	85	82	86	83	86	82	85	82	83	81	80	74	75	71	73	71	72	71	71
6	80	78	81	80	81	79	80	79	78	78	74	71	70	68	68	67	69	67	67
7	84	82	84	83	84	82	83	80	81	79	76	72	72	70	70	69	70	68	69
8	82	78	83	80	83	79	82	79	81	78	77	71	72	68	71	67	70	67	69
9	78	77	81	78	80	78	81	77	79	77	76	71	73	69	71	68	71	69	71
10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
11	74	72	74	77	76	73	76	73	73	72	71	64	63	61	62	60	63	60	62
12	88	81	89	83	87	81	87	81	84	79	79	72	75	69	72	67	71	66	69
13	75	73	77	77	76	75	75	74	73	73	69	64	64	63	62	61	62	62	61
AVG	82	78	82	80	82	79	81	76	79	77	75	70	71	67	68	66	68	66	87
<u>Supply Spool</u>																			
1	66	68	70	70	72	72	72	72	72	71	68	65	64	62	62	61	62	61	61
2	87	75	79	77	81	77	81	77	79	75	75	69	69	67	68	65	67	65	66

NOTE: All data corrected for self-heating, except injection.

TABLE 3-4

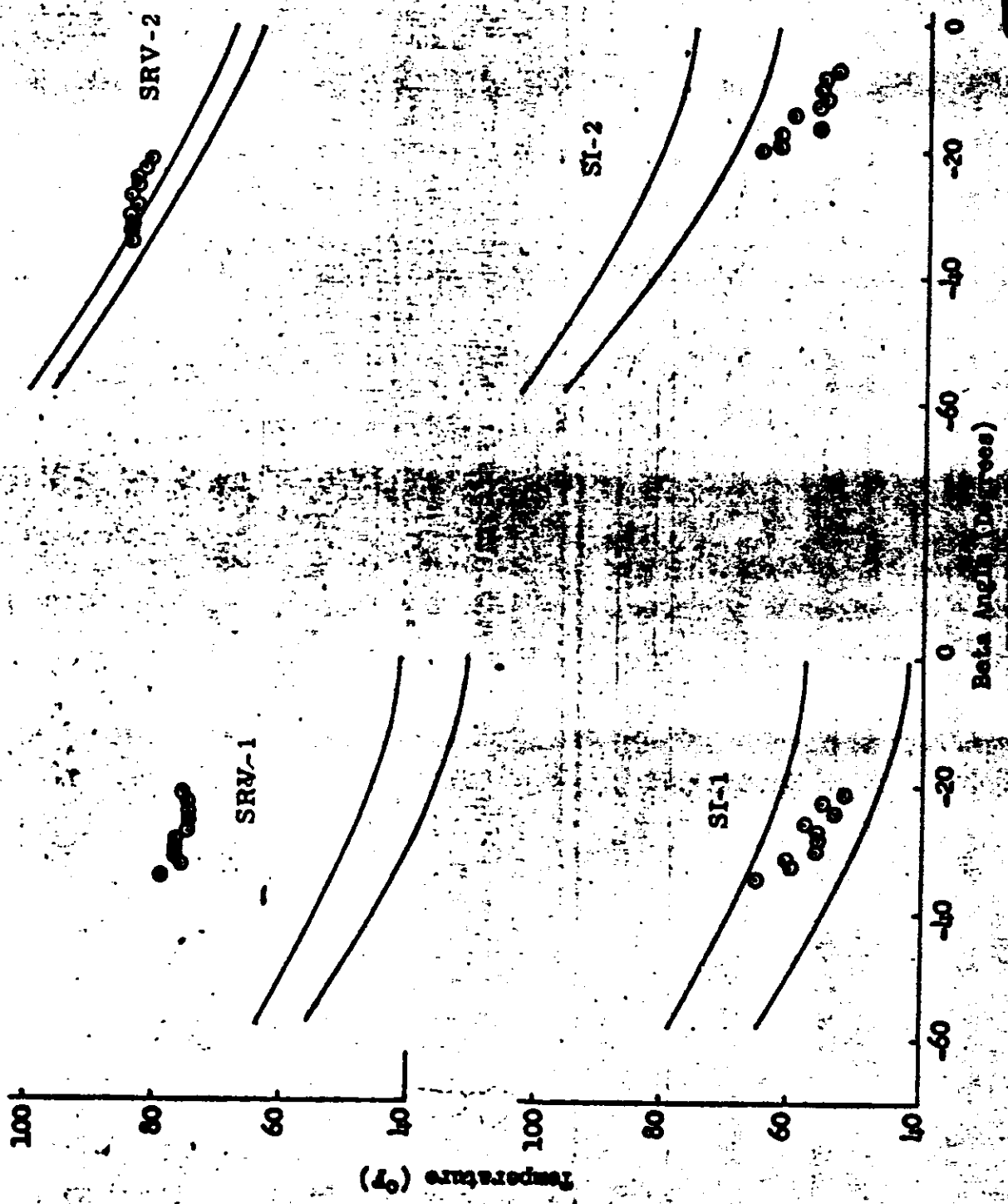
J-25 TEMPERATURE SUMMARY

SENSOR	ORBITS ACQUIRED																			
	Fair ("A") Barrel #1 ("B")	9	16	16	31	40	47	56	63	72	78	88	94	103	110	119	126	135	142	15
1	-	-	-	-	-	-	-	-	-	-	-	82	85	82	82	85	85	82	85	8
2	-5	-12	-2	-15	-5	-12	-2	-15	-2	-17	56	44	60	44	60	48	64	48	6	
3	-13	-13	-13	-11	-13	-13	-11	-13	-13	-13	79	96	76	93	79	93	76	82	7	
4	-	OBL	OBL	OBL	-	OBL	OBL	OBL	-	-	51	67	46	59	43	54	43	46	3	
5	71	68	68	60	60	52	68	48	56	44	40	47	33	37	33	33	26	30	1	
6	64	79	64	76	56	64	64	56	52	45	-	-	-	-	-	-	-	-	-	
<u>Barrel #2</u>																				
1	58	73	54	65	46	65	50	58	42	50	30	34	26	26	23	23	15	15	1	
2	61	92	61	92	58	80	61	75	55	69	49	66	46	61	46	52	41	43	3	
3	69	88	69	96	69	88	73	88	73	86	69	91	69	86	69	88	69	77	5	
4	62	53	66	53	66	56	72	59	69	56	66	56	66	53	69	59	72	59	7	
5	52	56	60	60	52	64	64	64	64	64	41	41	37	37	37	41	37	41	9	
<u>Conic Adapter</u>																				
1	57	62	54	57	51	51	54	46	49	43	35	30	33	25	30	22	25	22	2	
<u>Clock</u>																				
1	68	64	70	64	68	66	68	64	68	64	57	51	51	51	55	49	51	49	5	
2	81	77	83	79	70	79	83	79	81	77	70	66	68	62	68	62	66	62	6	
<u>Thrust Cone "A" to "B" SRV</u>																				
1	49	42	45	41	44	40	44	39	43	39	65	63	63	60	60	59	59	59	5	
2	69	61	64	58	61	56	59	55	57	52	74	70	69	67	67	65	65	64	6	
<u>Stellar/Index "A" to "B"</u>																				
1	67	60	63	57	57	57	60	54	57	54	54	51	51	47	51	47	44	47	4	
2	62	59	59	55	55	55	55	52	52	49	59	55	55	47	51	47	47	47	4	
<u>Recovery Battery "B" SRV</u>																				
1	75	75	75	75	74	75	74	74	73	72	80	83	81	79	83	78	80	78	7	
<u>Master Cassette "A" SRV</u>																				
2	79	76	77	77	77	75	75	75	75	76	-	-	-	-	-	-	-	-	-	

NOTE: Only Thrust Cone Data corrected for Self-heating.

TOP SECRET

J-25 FLIGHT
10/28/65 - 11/7/65

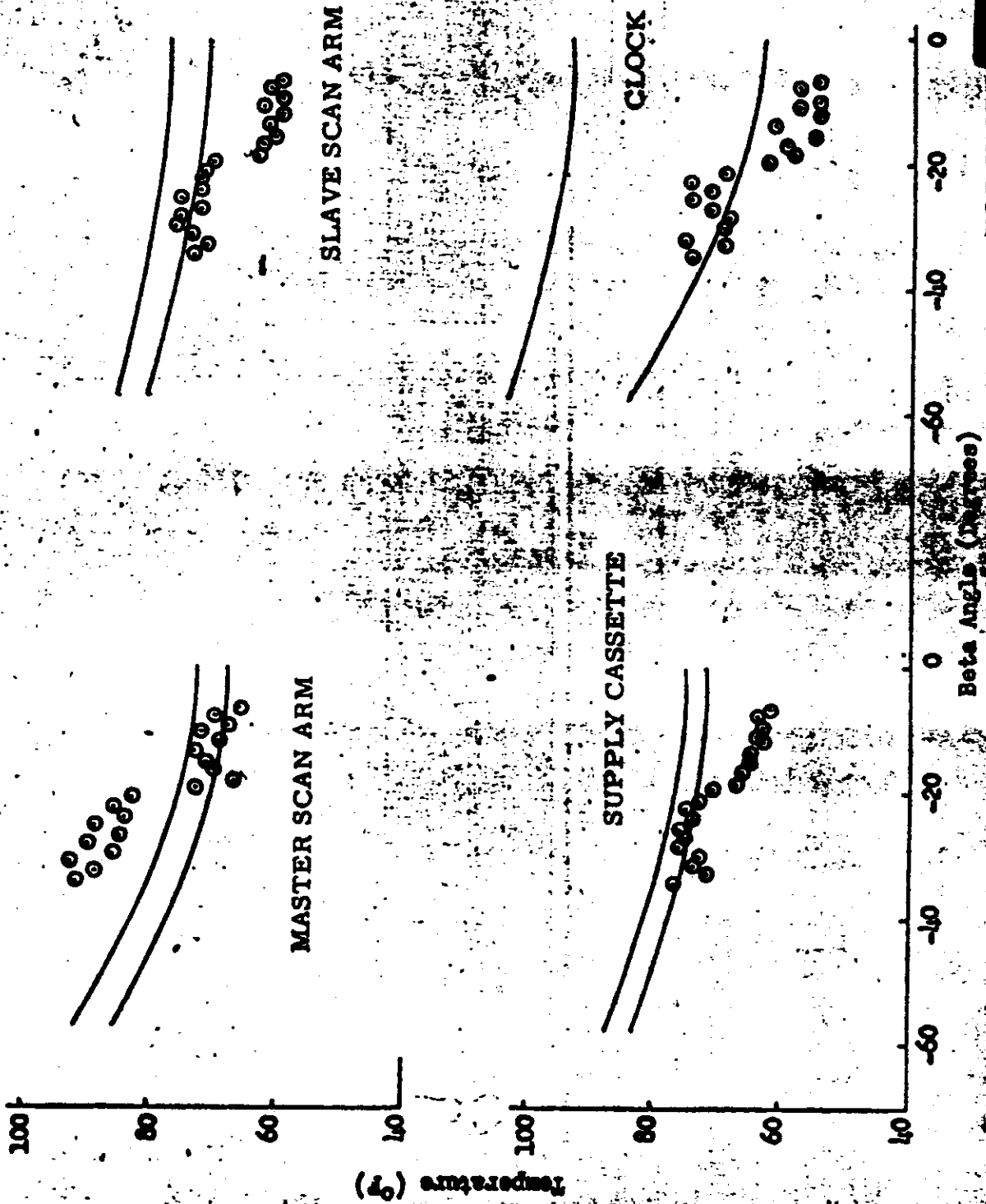


TOP SECRET

No.

J-25 FLIGHT

10/28/65 - 11/7/65



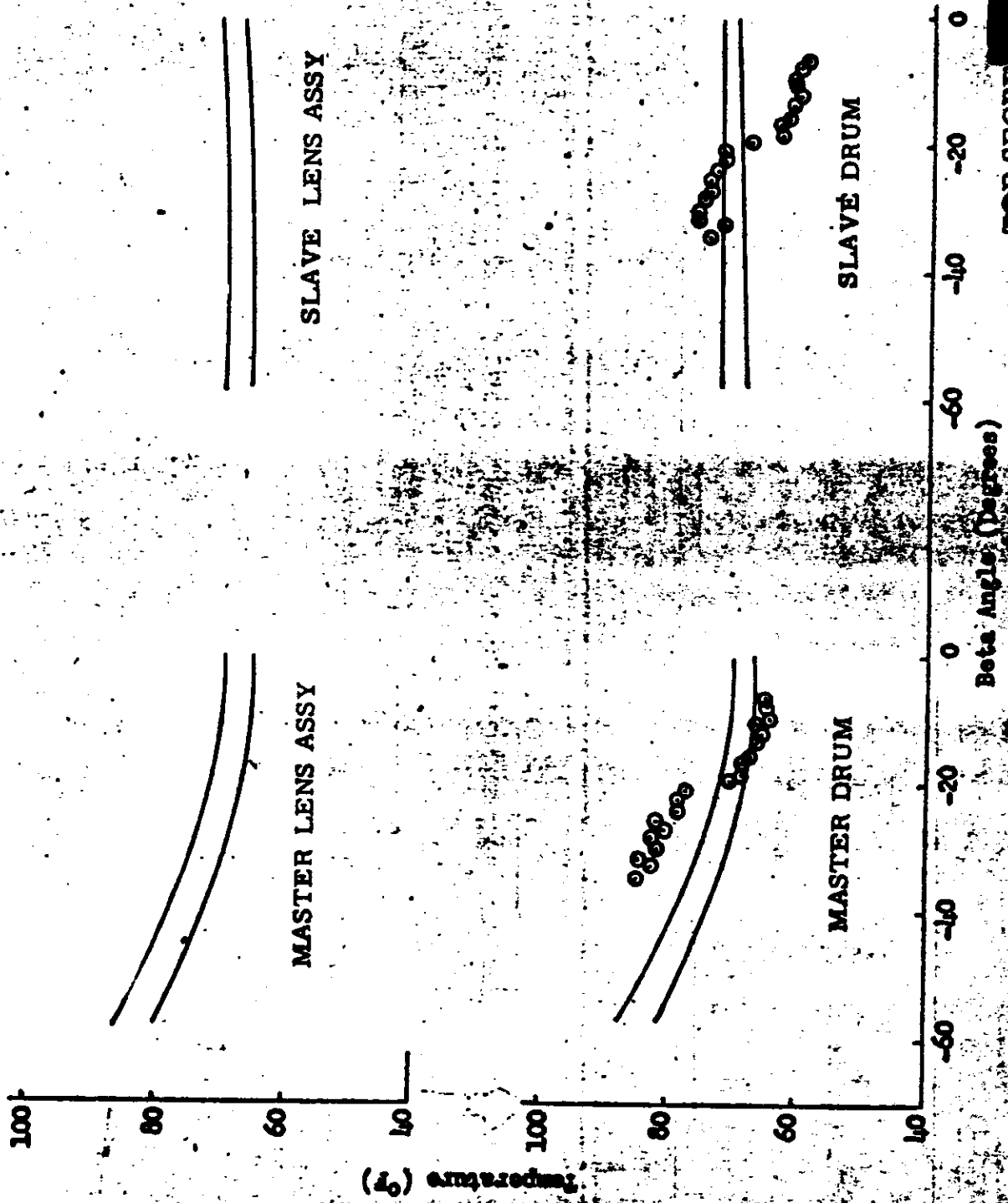
TOP SECRET

FIGURE 1

TOP SECRET

No

J-25 FLIGHT
10/28/65 - 11/7/65



TOP SECRET

FIGURE 2.1

~~TOP SECRET~~ [REDACTED]

No. [REDACTED]

SECTION 4

MISSION 1026-1 RECOVERY SYSTEM

SRV #701 was received at A/P on 7 May 1965. The receiving weight was 149.7 pounds. After modifications and incorporation of outstanding E.O.'s, the SRV was delivered to Systems Test for incorporation into the J-25 system.

The capsule was shipped to VAFB on 1 October 1965.

The -1 recovery system was successfully recovered by air catch from orbit 81 at 16:03 PST on 2 November 1965. The impact point was as follows:

Predicted Impact $24^{\circ}01.5'N/168^{\circ}46'W$

Actual Impact $23^{\circ}53'N/168^{\circ}37'W$

The condition of the recovered capsule was satisfactory with no damage other than normal paint blistering due to the re-entry environment.

Event times are shown in Table 4-1. There were no chute events recorded at orbit 81 [REDACTED] or T/M ship.

~~TOP SECRET~~ [REDACTED]

~~TOP SECRET~~

No. [REDACTED]

MISSION 1026-1
RECOVERY SEQUENCE OF EVENTS

<u>Event</u>	<u>Delta Time (Seconds)</u>	
	<u>Actual</u>	<u>Nominal</u> <u>Events + Δ T</u>
*Arm	76.99	77.0 + 1.0
*Transfer	2.3	2.0 + 0.25
Electrical Disconnect	1.0	0.900 + 0.430 - 0.400
Separation	---	---
**Spin	3.43	3.4 + 0.30
Retro	7.53	7.55 + 0.45
Despin	10.70	10.75 + 0.59
T/C Separation	1.50	1.5 + 0.15
***"G" Switch Open	N/A	469.7
Parachute Cover Off	N/A	34.0 + 1.5
Drogue Chute Deployed	N/A	0.63 + 0.08
Main Chute Bag Separate	N/A	10.25 + 1.5
Main Chute Deployed	N/A	0.52 + 0.13
Main Chute Disreef	N/A	4.5 + 0.80

- * From Separation
- ** From Electrical Disconnect
- *** From Retro

TABLE 4-1

~~TOP SECRET~~

No. [REDACTED]

SECTION 5

MISSION 1026-2 RECOVERY SYSTEM

SRV #702 was received at A/P on 7 May 1965. The receiving weight was 147.8 pounds. After modifications and incorporation of outstanding E. O. 's the unit was delivered to Systems Test for mating to the J-25 system.

The capsule was shipped to VAFB on 1 October 1965.

The -2 recovery system was successfully recovered by air catch from orbit 160 at 15:04 PST on 7 November 1965. The impact point was as follows:

Predicted Impact $24^{\circ}02'N/169^{\circ}49'W$.

Actual Impact $23^{\circ}53'N/169^{\circ}42'W$.

Event times are shown in Table 5-1.

The condition of the recovered capsule indicated no abnormal re-entry effects.

MISSION 1026-2
RECOVERY SEQUENCE OF EVENTS

<u>Event</u>	<u>Delta Time (Seconds)</u>	
	<u>Actual</u>	<u>Nominal</u> <u>Events + Δ T</u>
*Arm	76.84	77.0 + 1.0
*Transfer	2.03	2.0 + 0.25
Electrical Disconnect	0.89	0.900 +0.430 -0.400
Separation	---	----
**Spin	3.39	3.4 + 0.30
Retro	7.59	7.55 + 0.45
Despin	10.71	10.75 + 0.59
T/C Separation	1.51	1.5 + 0.15
***"G" Switch Open	469.07	469.7
Parachute Cover Off	33.88	34.0 + 1.5
Drogue Chute Deployed	0.59	0.63 + 0.08
Main Chute Bay Separate	11.05	10.25 + 1.5
Main Chute Deployed	0.55	0.52 + 0.13
Main Chute Disreef	4.45	4.45 + 0.80

- * From Separation
- ** From Electrical Disconnect
- *** From Retro

TABLE 5-1

SECTION 6

MASTER PANORAMIC CAMERA

A. COMPONENT ASSIGNMENT

<u>Component</u>	<u>Serial Number</u>
Main Camera	174
Main Camera Lens	1712435
Supply Horizon Camera	276-G2
Supply Horizon Camera Lens	816646
Take-up Horizon Camera	276-G1
Take-up Horizon Camera Lens	816825
Supply Cassette	SC-35

B. CAMERA DATA AND FLIGHT SETTINGS

Main Camera:

Lens	24" f/3.5
Slit Width	0.225"
Filter Type	Wratten 25
Film Type	Eastman Type 4404

Supply (Port) Horizon Camera:

Lens	55 mm f/6.8
Aperture Setting	f/6.8
Exposure Time	1/100 second
Filter Type	Wratten 25

~~TOP SECRET~~ [REDACTED]

No. [REDACTED]

Take-up (Starboard) Horizon Camera:

Lens	55 mm f/6.8
Aperture Setting	f/8.0
Exposure Time	1/100 second
Filter Type	Wratten 25

C. POST FLIGHT PERFORMANCE EVALUATION (Master Instrument)

The image quality of the photography produced by the Master camera was rated good but not equal to the quality of the previous two missions (1024 and 1025). Mission 1026-1 and 1026-2 were extensively affected by atmospheric conditions in combination with low solar elevations. Cloud cover ran up to 70% over some primary target areas and averaged approximately 50% for Mission 1026-1 and 1026-2.

The electro-mechanical operation of the camera system was good during both missions.

Light leaks fogged part of the first and third frames of most passes and the sixth frame from the end of most passes. Light leak fog was generally low density in the original negative. Light leak fog had a minor degrading effect on terrain imagery.

Fog on the first and third frames is attributed to a minor light leak in the vicinity of the master camera drum area. Fog on the sixth frame from the end of pass is attributed to a minor light leak in the vicinity of SRV #1. The main camera drum light leak is expected to be suppressed by application of a silicon elastomer on the suspect light leak area. Opaque film chutes will be added to eliminate the light leak fog occurring at the SRV #1 fairing interface area beginning approximately J-30 and up.

Auxiliary data recording such as the 200 pps track, blanked pulse, S/I slur pulse, instrument serial number, and start of pass mark were consistently good throughout Mission 1026-1 and 1026-2.

~~TOP SECRET~~ [REDACTED]

TOP SECRET

No. [REDACTED]

Horizon fiducials were consistently good. The imagery of the take-up horizon camera was veiled on passes D-03 through D-14. The cause of veiled horizon imagery is under investigation. Take-up horizon imagery was extremely overexposed in most passes after D-98, however, horizon arcs appear usable. Take-up horizon light fog is attributed to excessive light from high reflectance scenes on the sun side of the vehicle.

Traces of dendritic static are present intermittently along both edges of the film in passes D-40, D-70, D-72, D-78, D-79, D-84, D-85, D-86, and D-116 and along the binary edge in passes D-05 and D-51.

Minor scratches are present under the camera serial number, along the edge opposite the camera number and at the take-up end of each frame. Minor scratches are attributed to normal scan head roller action.

TOP SECRET

SECTION 7

SLAVE PANORAMIC CAMERA

A. COMPONENT ASSIGNMENT

<u>Component</u>	<u>Serial Number</u>
Main Camera	175
Main Camera Lens	1722435
Supply Horizon Camera	277-G2
Supply Horizon Camera Lens	816626
Take-up Horizon Camera	277-G1
Take-up Horizon Camera Lens	816631
Supply Cassette	SC-15

B. CAMERA DATA AND FLIGHT SETTINGS

Main Camera:

Lens	24" f/3.5
Slit Width	0.150
Filter Type	Wratten 21
Film Type	Eastman Type 4404

Supply (Starboard) Horizon Camera:

Lens	55 mm f/6.8
Aperture Setting	f/8.0
Exposure Time	1/100 second
Filter Type	Wratten 25

TOP SECRET

No. [REDACTED]

Take-up (Port) Horizon Camera

Lens	1	55 mm f/6.8
Aperture Setting		f/6.8
Exposure Time		1/100 second
Filter Type		Wratten 25

C. POST FLIGHT PERFORMANCE EVALUATION (Slave Instrument)

The photographic quality and information content of the imagery produced by the slave camera was rated slightly higher on the average than the master camera for Missions 1026-1 and 1026-2.

The binary index lamp, binary work, and camera number were absent on 57 frames and the horizon fiducials were absent on 27 frames of Mission 1026-1. Failure occurred randomly throughout Mission 1026-1 beginning with pass D-24 and ending with pass D-70. Failure of the subject auxiliary data recording is attributed to a faulty center of format switch. Center of format switch operation was acceptable throughout Mission 1026-2 as evidenced by the presence of good data recording on all frames of recorded material.

The horizon cameras were operational throughout Mission 1026-1 and 1026-2. However, the imagery recorded by the supply horizon camera of the slave instrument appeared out of focus or veiled throughout Mission 1026-1. This condition continues in Mission 1026-2 but gradually disappears. After pass D-110 the supply horizon photography is sharp. The cause of this phenomenon, although unknown at this time, is under investigation.

Minor light leak fog marks were observed on the first frame and the last three frames of most passes. Fogging is attributed to minor light leaks in the vicinity of the slave instrument drum area.

Minor dendritic static was present at random intervals along both edges of the slave camera film in several passes of photography.

Fine scratches were present under the camera number and at the take-up end of each frame. Scratches are attributed to normal scan head roller action.

TOP SECRET

SECTION 8

PANORAMIC CAMERA EXPOSURE

The Master camera contained a 0.225 inch slit and a Wratten 25 filter. The Slave camera had a 0.150 inch slit and a Wratten 21 filter. These conditions placed the nominal exposure on the full processing curve.

The frequency distributions of the solar elevations and solar azimuths encountered during the photographic operations are shown in Figures 8-1 to 8-4.

The nominal exposure times of the Master and Slave cameras are shown as a function of latitude for passes D-8, D-56, D-104 and D-152 in Figures 8-5 to 8-12. The predicted level of processing for the original negative is based on the in-flight performance estimate and is tabulated below with the processing levels reported by [REDACTED]

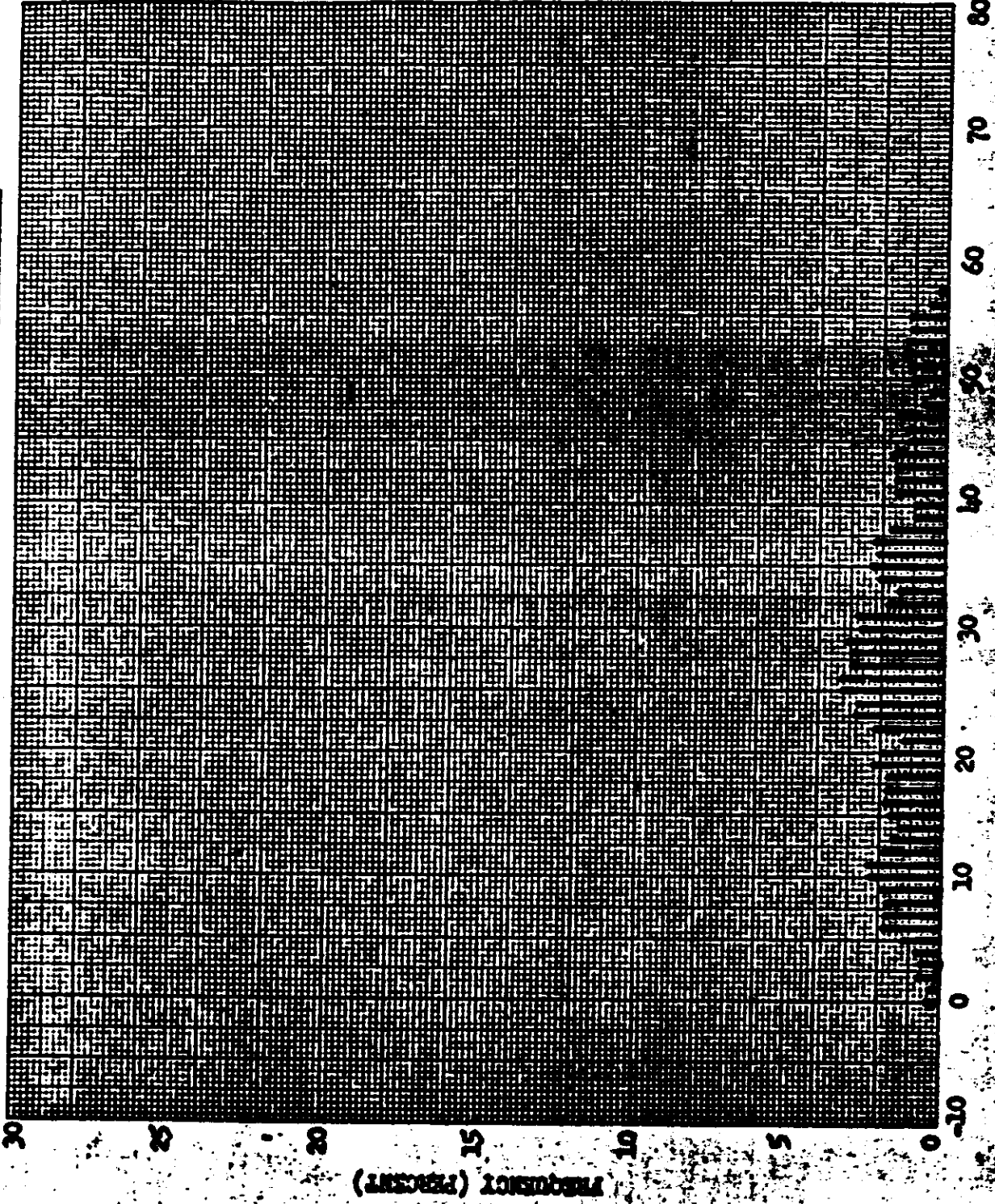
<u>Mission</u>	<u>Camera</u>		<u>Primary</u>	<u>Intermediate</u>	<u>Full</u>
1026-1	FWD	Predicted	0	4	96
		Reported	0	21	79
1026-1	AFT	Predicted	0	5	95
		Reported	0	4	96
1026-2	FWD	Predicted	1	0	99
		Reported	2	5	93
1026-2	AFT	Predicted	1	0	99
		Reported	2	5	93

On pass D-87 the V/h programmer did not operate due to a command error. The imagery was taken at a slow exposure and primary processing was predicted; [REDACTED] reported Full processing.

TOP SECRET

No.

SOLAR ELEVATION FREQUENCY DISTRIBUTION



Mission No: 1026-1

Payload No: J-25

Camera No: 174

Launch Date: 10/28/62

Launch Time: 2117 Z

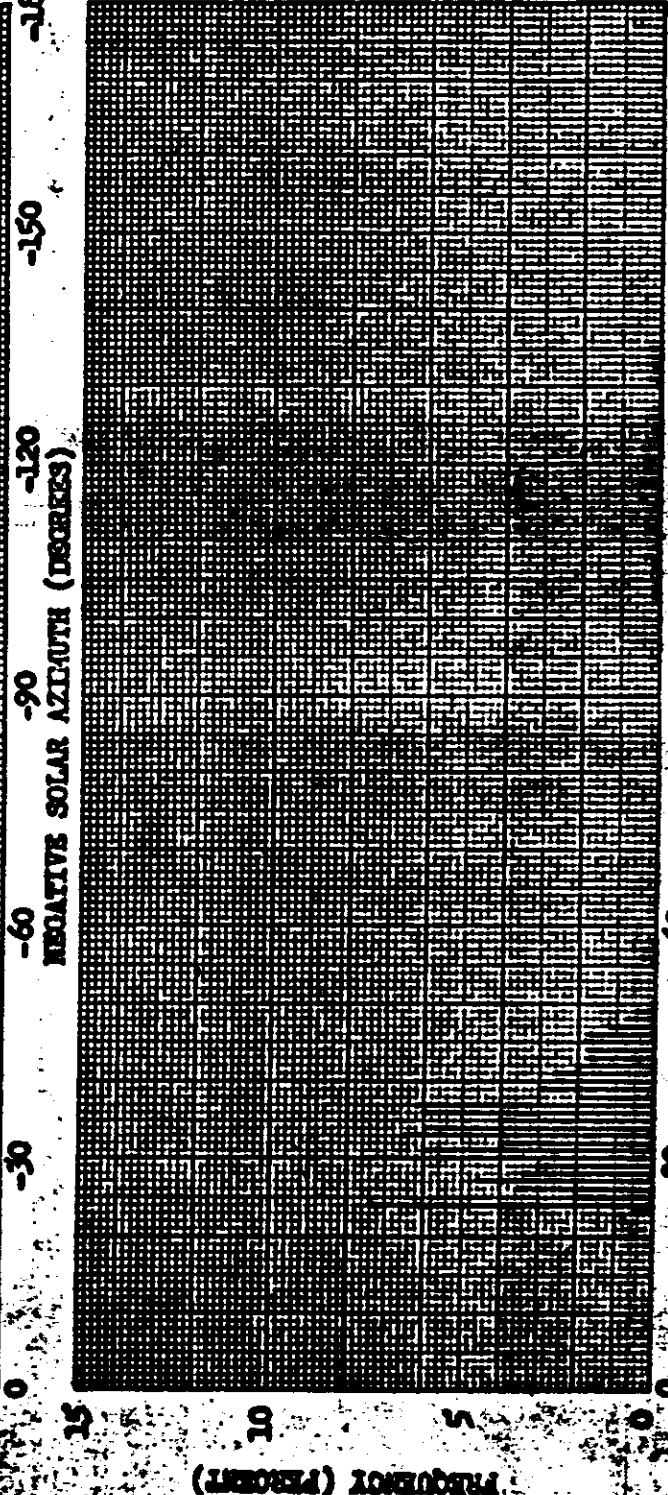
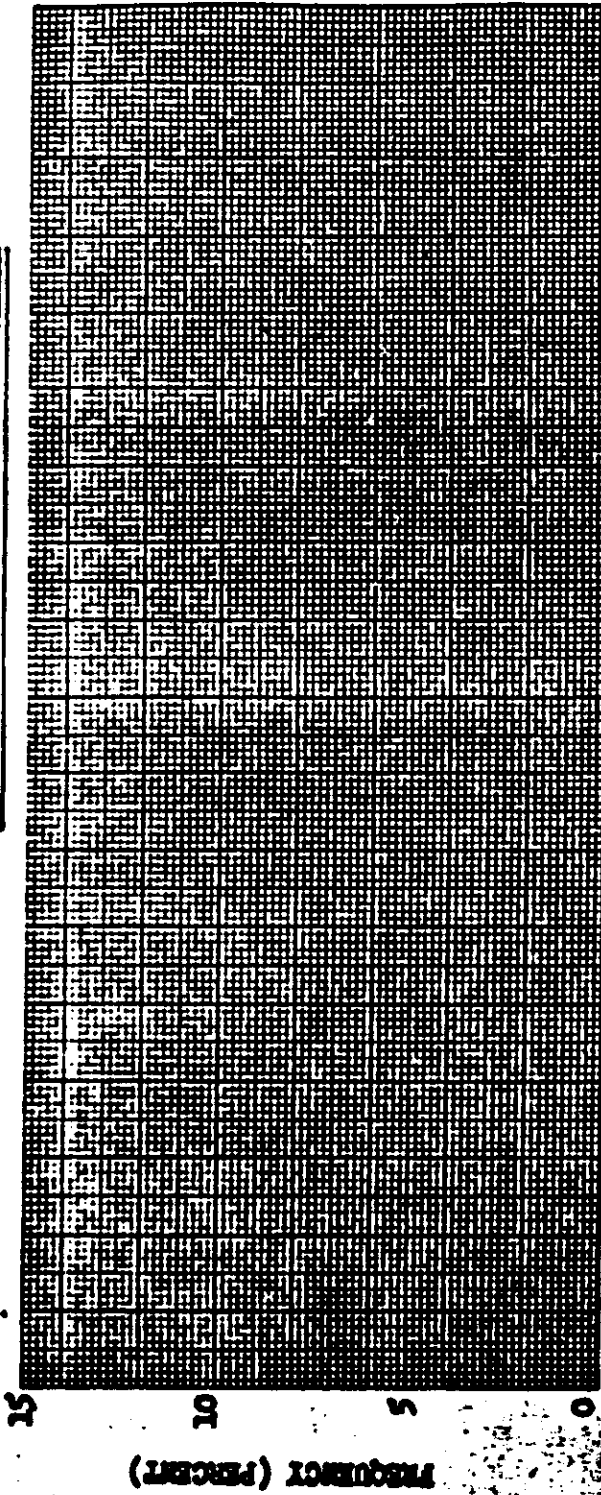
Inclination: 75°

TOP SECRET

TOP SECRET

No.

SOLAR AZIMUTH FREQUENCY DISTRIBUTION



Mission No: 1026-1

Payload No: J-25

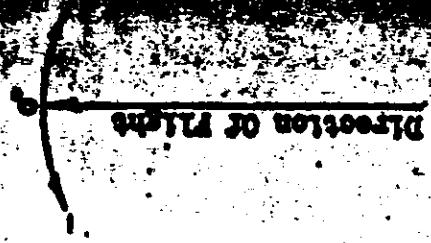
Camera No: 174

Launch Date: 10/28/65

Launch Time: 2117 Z

Inclination: 75°

SIGN NOTATION



150

120

90

60

30

0

15

10

5

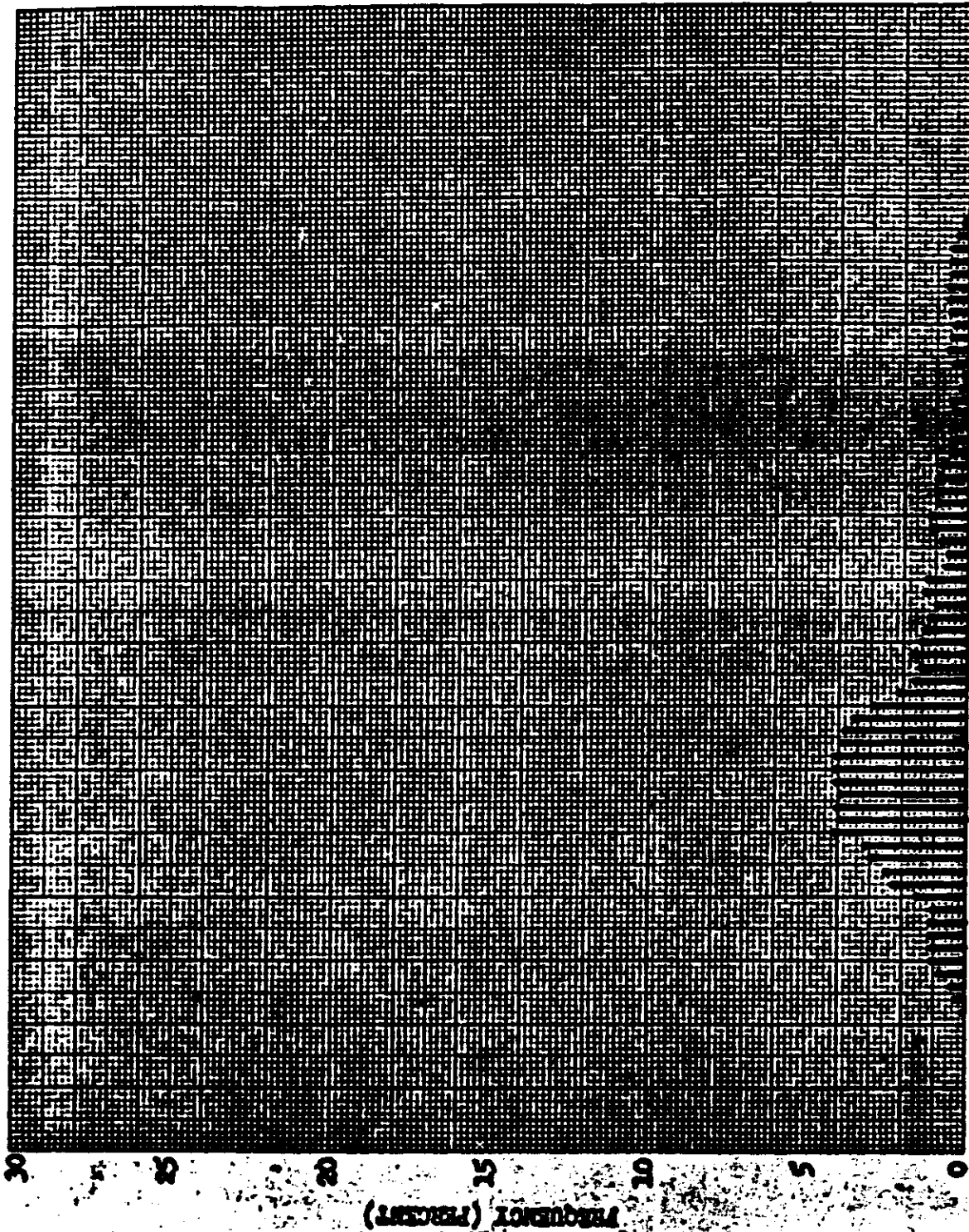
0

TOP SECRET

TOP SECRET

No.

SOLAR ELEVATION FREQUENCY DISTRIBUTION



Mission No: 1026-2

Payload No: J-25

Camera No: 174

Launch Date: 10/28/65

Launch Time: 2117 Z

Inclination: 75°

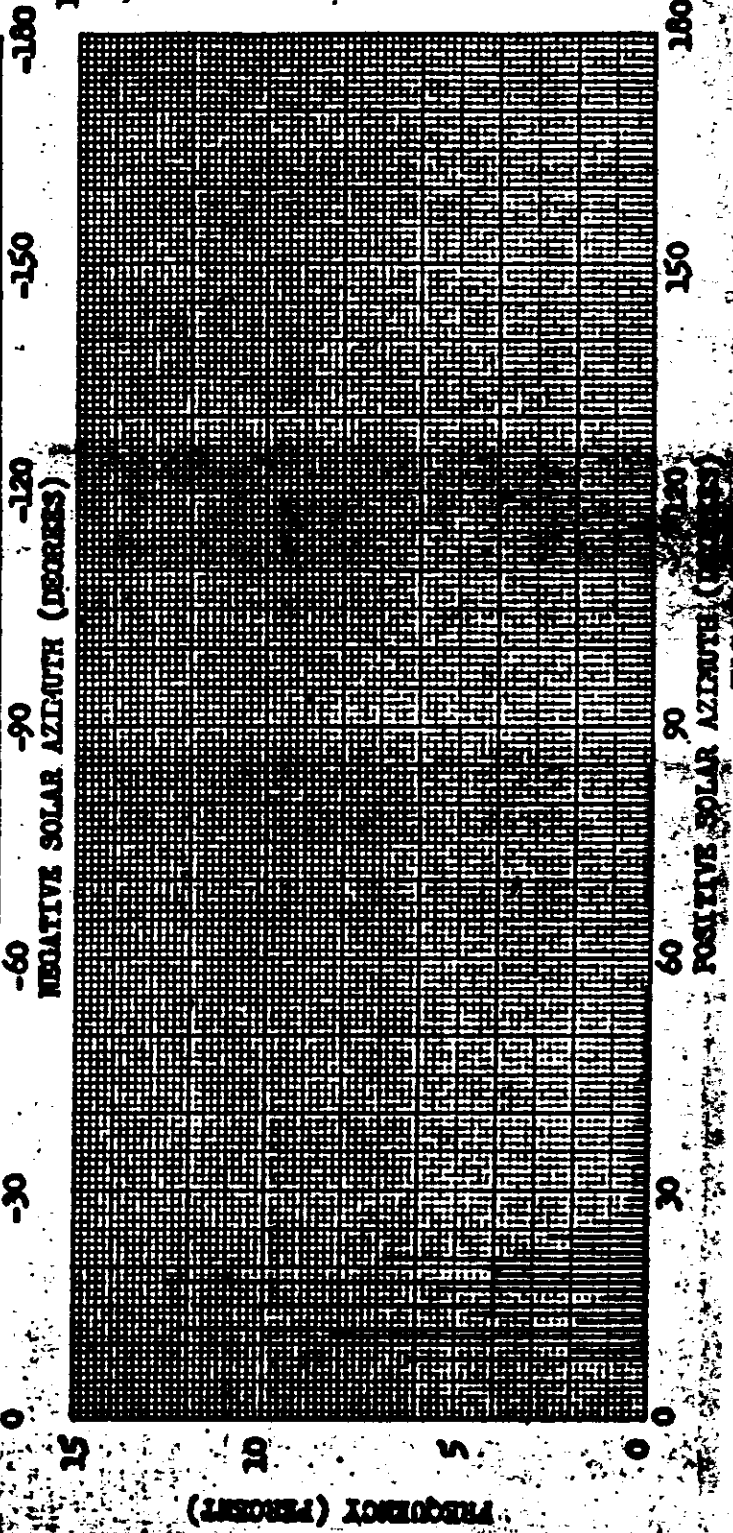
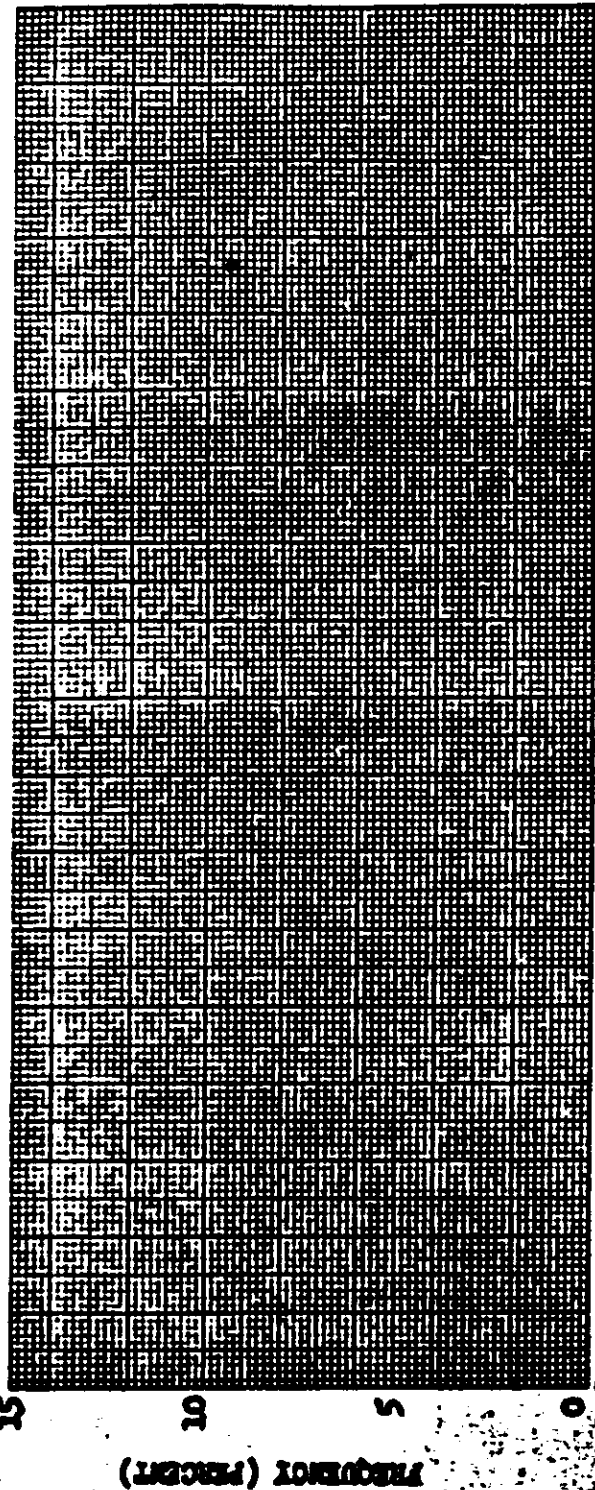
SOLAR ELEVATION (DEGREES)

FIGURE

TOP SECRET

TOP SECRET [REDACTED] No. [REDACTED]

SOLAR AZIMUTH FREQUENCY DISTRIBUTION



Mission No: 1026-2

Payload No: J-25

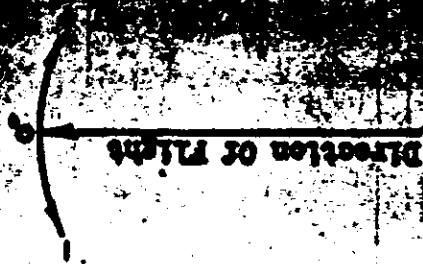
Camera No: 174

Launch Date: 10/28/65

Launch Time: 2117 Z

Inclination: 75°

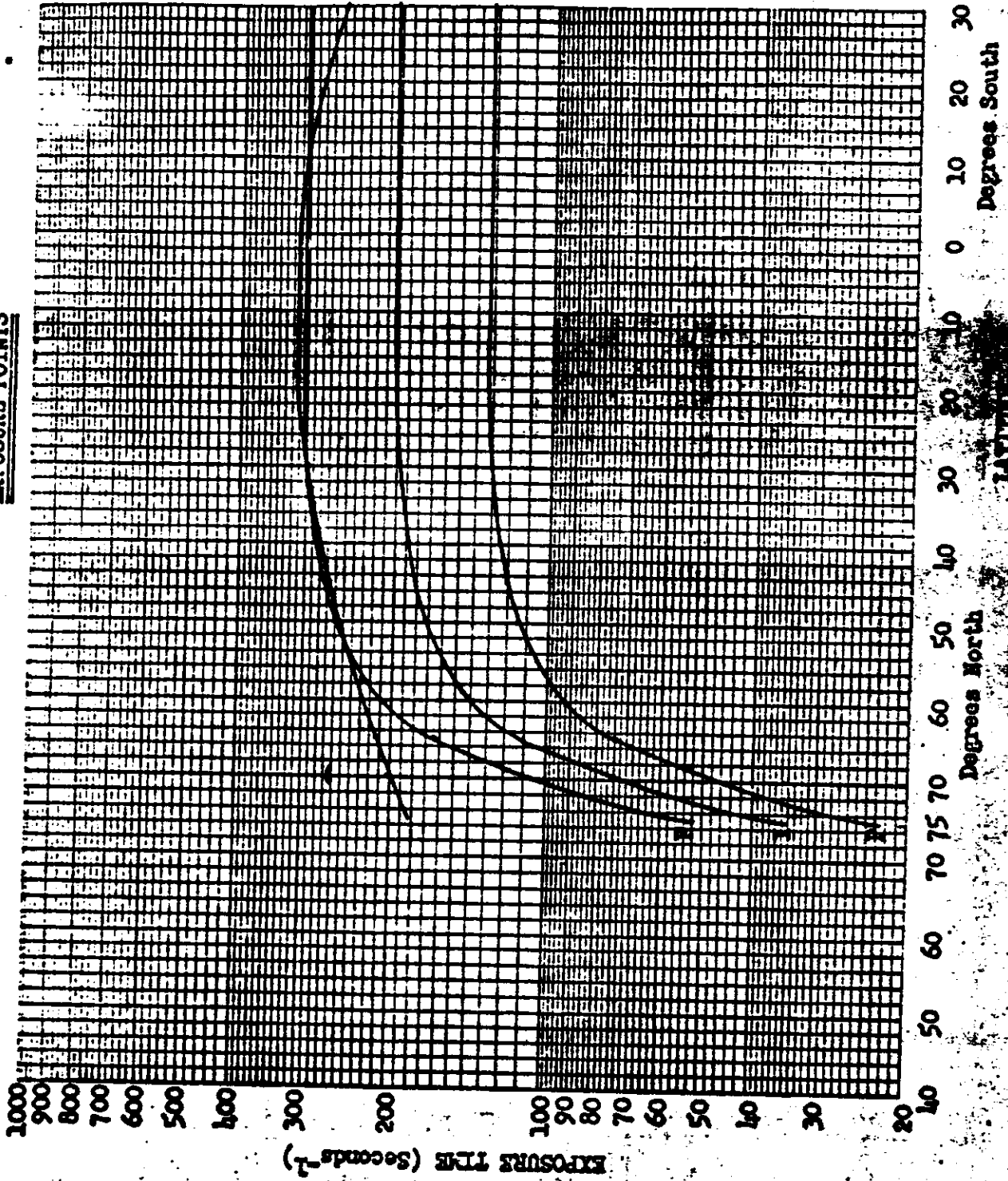
SIGN NOTATION



TOP SECRET

No. [REDACTED]

EXPOSURE POINTS



Mission No: 1026

Payload No: J-25

Camera No: 174

Pass No: 8

Launch Date: 10/28/65

Launch Time: 2117

Slit Width: .225

Filter Type: Wratten

Film Type: 3104

LATITUDE

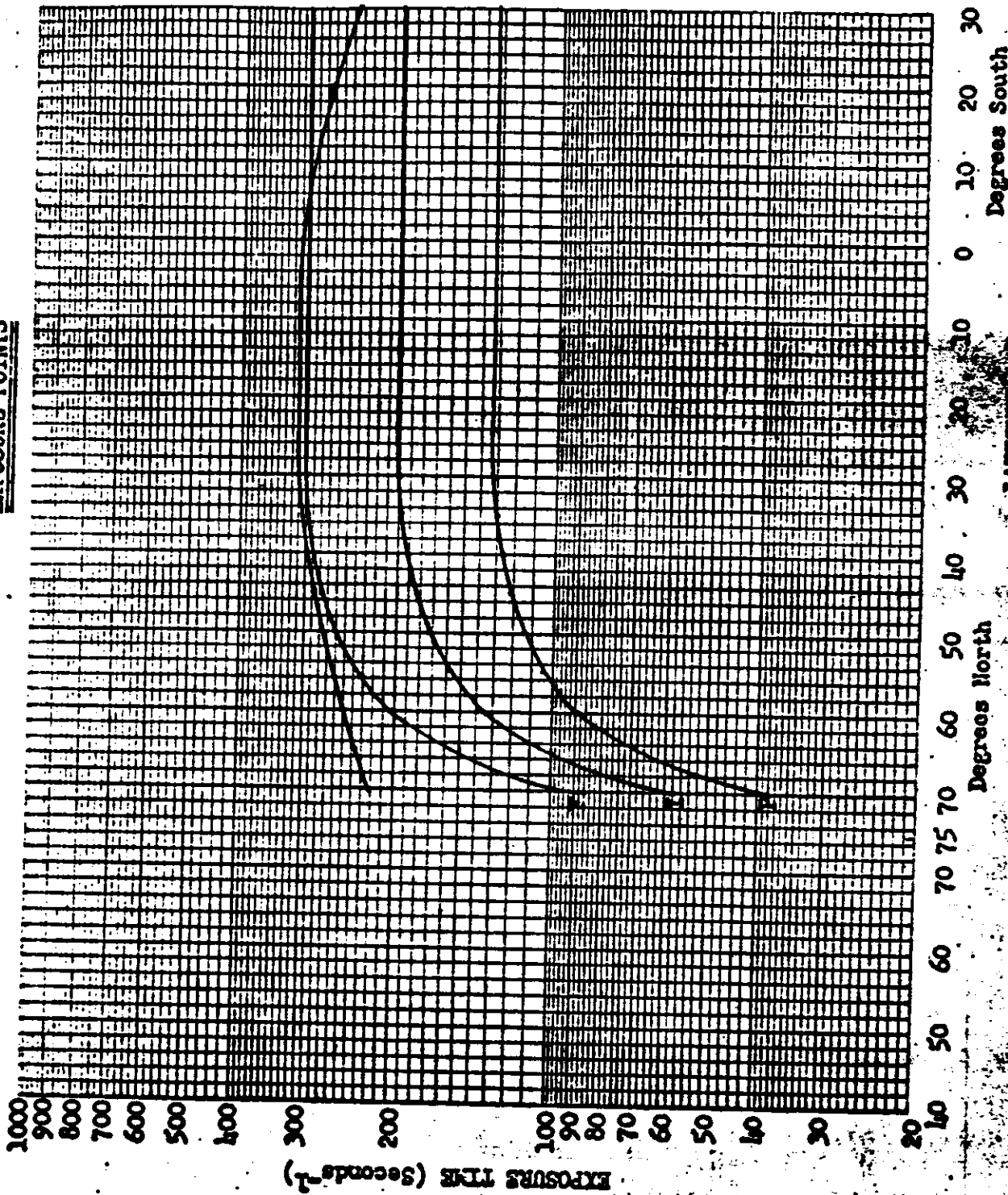
FIGURE

TOP SECRET

TOP SECRET

No.

EXPOSURE POINTS



Mission No: 1026

Payload No: J-25

Camera No: 174

Pass No: 56

Launch Date: 10/28/65

Launch Time: 2117 Z

Slit Width: .225

Filter Type: Wratten 2

Film Type: 3404

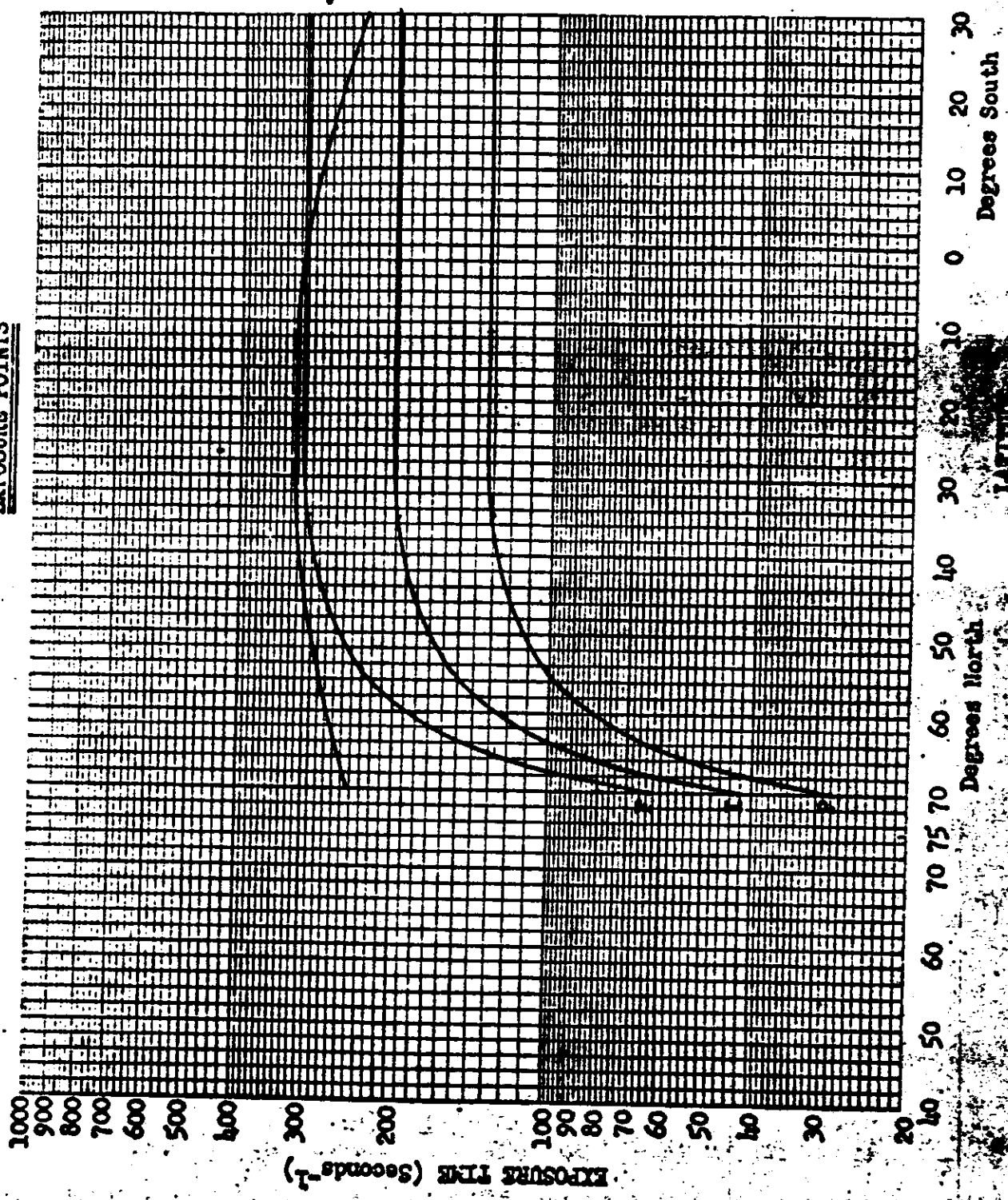
LATITUDE

FIGURE 1

TOP SECRET

TOP SECRET [REDACTED] No. [REDACTED]

EXPOSURE POINTS



Mission No: 1026

Payload No: J-25

Camera No: 174

Pass No: 104

Launch Date: 10/28/67

Launch Time: 2117 Z

Slit Width: .225

Filter Type: Wratten

Film Type: 3404

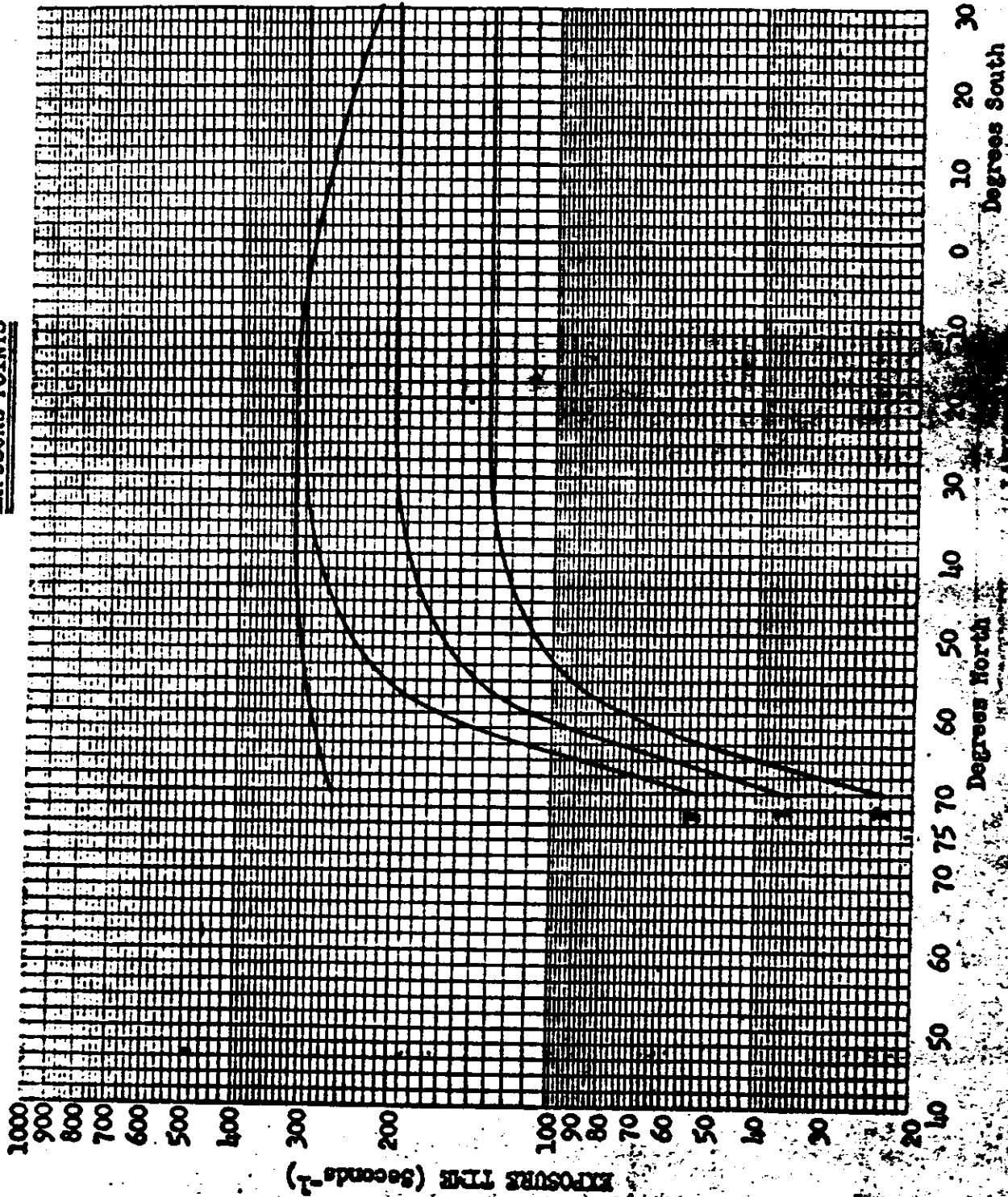
LASTED
FIGURE

TOP SECRET

TOP SECRET

No.

EXPOSURE POINTS



LABORATORY
FIGURE

Mission No: 1026

Payload No: J-25

Camera No: 17A

Pass No: 152

Launch Date: 10/28/65

Launch Time: 2117

Slit Width: .225

Filter Type: Wratten 25

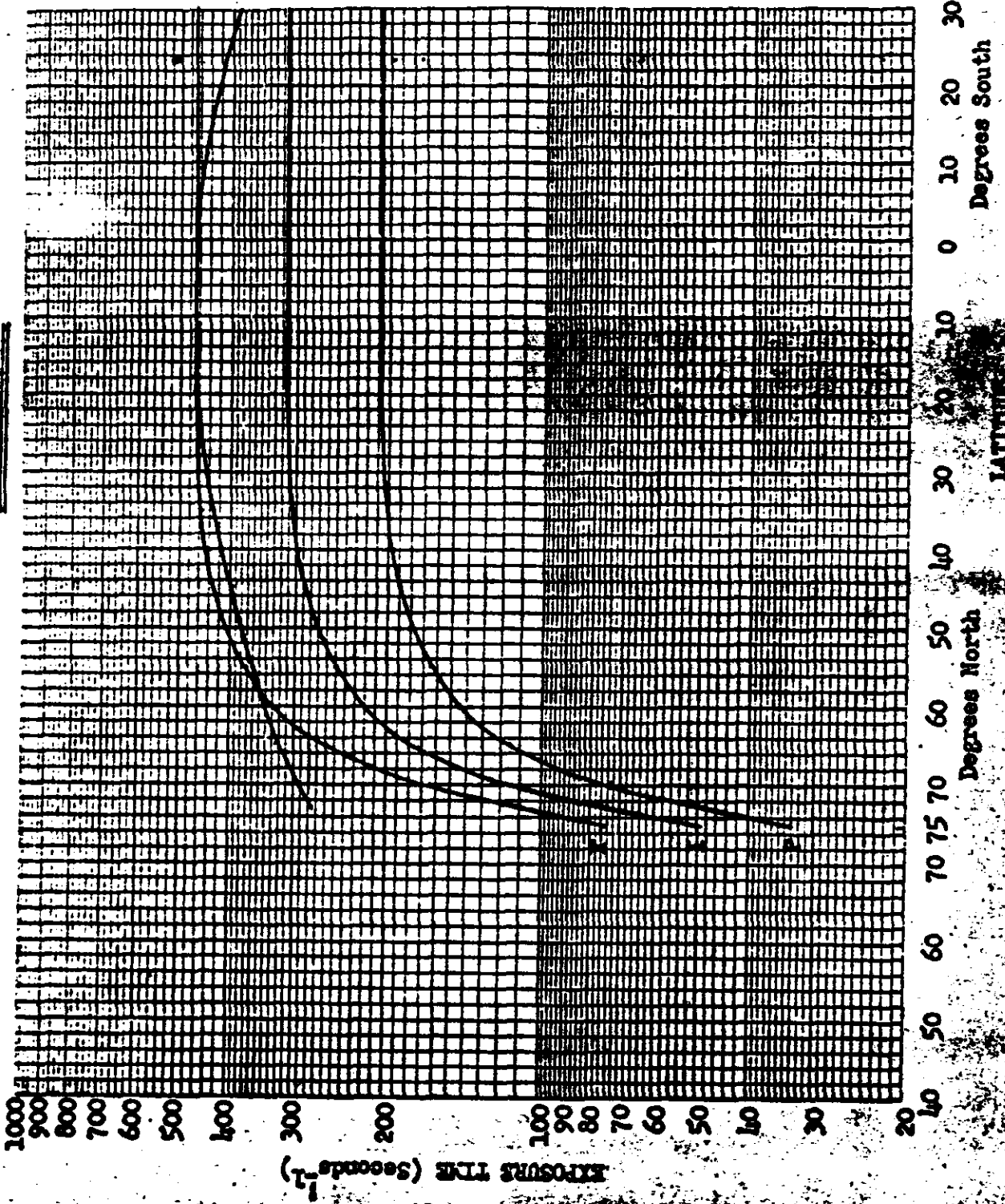
Film Type: 310A

TOP SECRET

TOP SECRET

No.

EXPOSURE POINTS



Mission No: 1026

Payload No: 1-25

Camera No: 175

Pass No: 8

Launch Date: 10/28/65

Launch Time: 2117 Z

Slit Width: 150

Filter Type: Wratten

Film Type: 304

LATITUDE

Degrees South

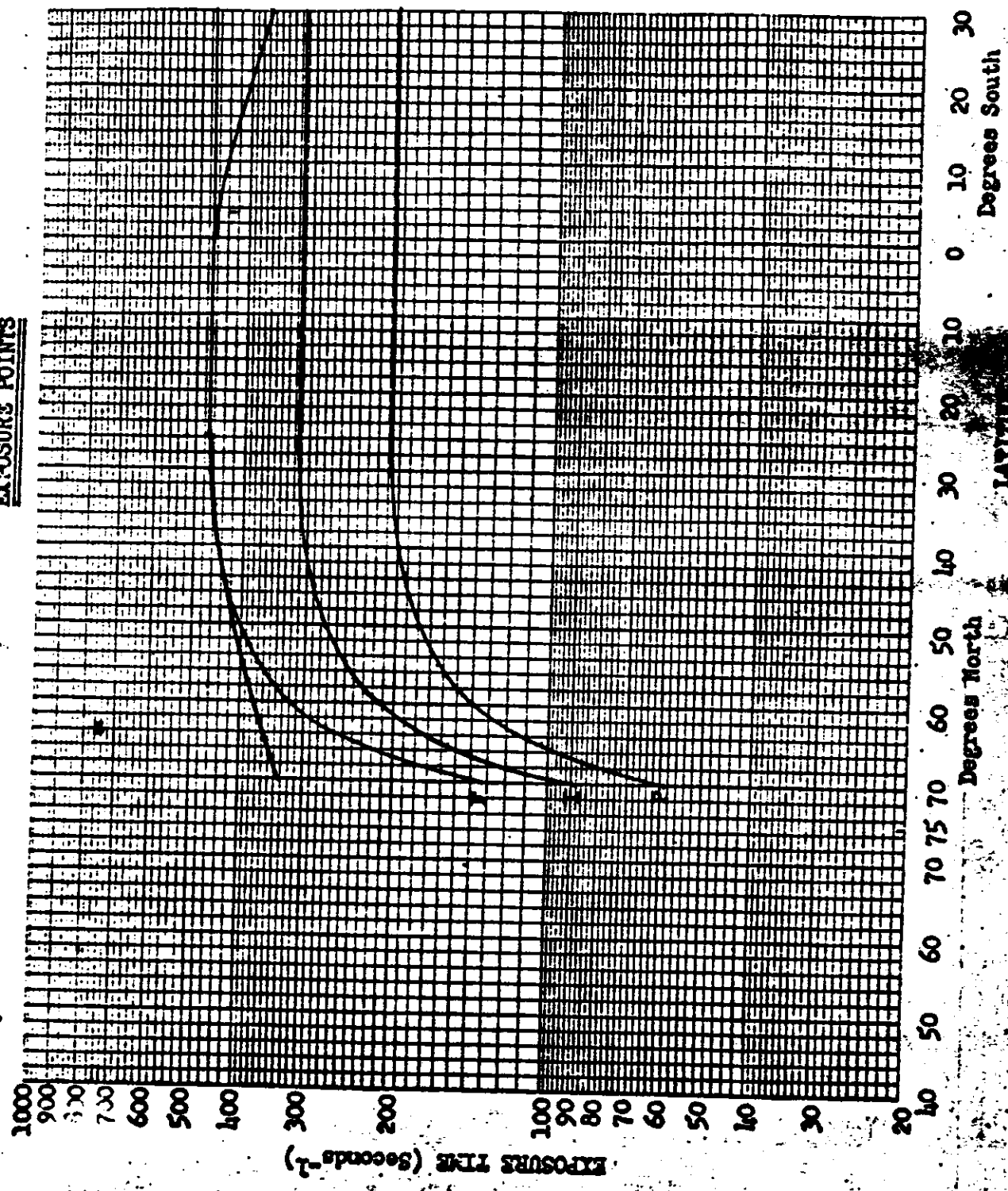
Degrees North

FIGURE

TOP SECRET

TOP SECRET [Redacted] No. [Redacted]

EXPOSURE POINTS



Mission No: 1026
Payload No: J-25
Camera No: 175
Pass No: 56
Launch Date: 10/28/65
Launch Time: 2117 Z
Slit Width: .150
Filter Type: Wratten 21
Film Type: 3104

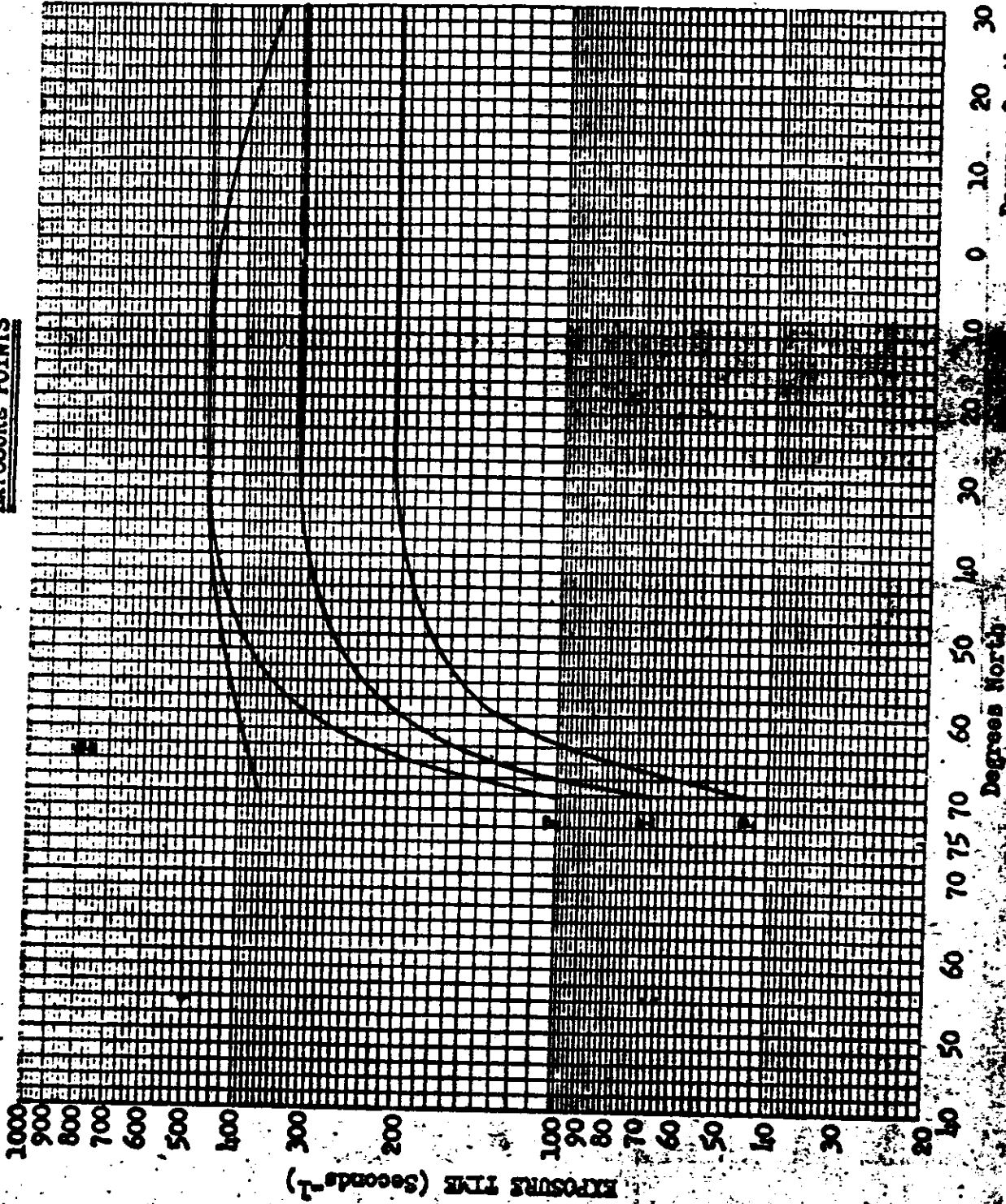
LAPTOP
FIGURE

TOP SECRET

TOP SECRET

No. [REDACTED]

EXPOSURE POINTS



Mission No: 1026
 Payload No: J-25
 Camera No: 175
 Pass No: 104
 Launch Date: 10/28/65
 Launch Time: 2117 Z
 Slit Width: 0.50
 Filter Type: Wratten 27
 Film Type: 3104

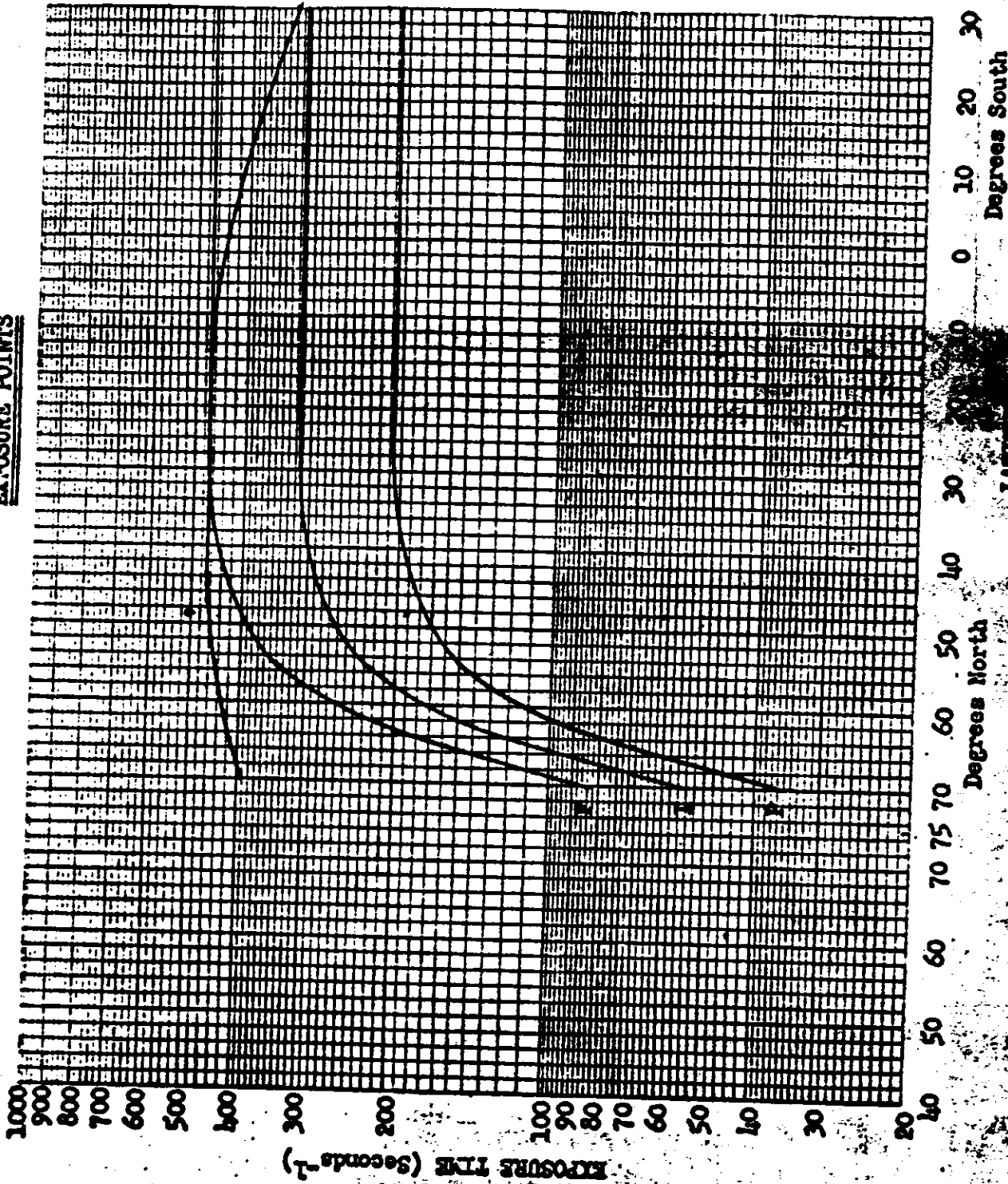
LAST IN
FIGURE

TOP SECRET

TOP SECRET

No.

EXPOSURE POINTS



Mission No: 1026

Payload No: J-25

Camera No: 175

Pass No: 152

Launch Date: 10/20/65

Launch Time: 2117 Z

Slit Width: .150

Filter Type: Wratten 21

Film Type: 3604

LATITUDE

FIGURE

TOP SECRET

SECTION 9

DIFFUSE DENSITY MEASUREMENTS

The diffuse density measurements made by AFSPPF were computer sorted at A/P to permit analysis of the density ranges encountered at the three processing levels. A study of sorting techniques showed that no absolute method was available to separate the density values as the accuracy of the Processing History published by [REDACTED] appears rather low and processing transition phases are not accounted for. The sorting technique selected uses the base plus fog density values where measurements up to 0.09 density are considered as having received Primary processing, 0.10 to 0.17 as Intermediate and above 0.17 density as Full. The percentage of original negative that was processed at each level, based on the computer sort, is tabulated below with the predicted and reported processing percentages.

<u>Mission</u>	<u>Camera</u>		<u>Primary</u>	<u>Intermediate</u>	<u>Full</u>
1026-1	FWD	Predicted	0	4	96
		Reported	0	21	79
		Computed	0	24	76
1026-1	AFT	Predicted	0	5	95
		Reported	0	4	96
		Computed	0	37	63
1026-2	FWD	Predicted	1	0	99
		Reported	2	5	93
		Computed	0	5	95
1026-2	AFT	Predicted	1	0	99
		Reported	2	5	93
		Computed	0	15	85

The tabulations of density frequency distributions for Missions 1026-1 and 1026-2 are included in Appendix A, Table A-1 thru A-4. The graphical presentation of the density distribution are computer plotted in Appendix A Figures A-1 thru A-36.

~~TOP SECRET~~ [REDACTED]

No. [REDACTED]

A summary of the processing and exposure analysis is shown in Table 9-1. The terrain D_{Min} criteria, (range) for proper exposure and processing is 0.40 to 0.90 density units. The area measured for D_{Min} is selected subjectively and is not necessarily the absolute D_{Min} in the photography.

~~TOP SECRET~~ [REDACTED]

TOP SECRET

CONTROL NO.

MISSION 1026-1 INSTR - FRWD 12/28/65 PROCESSING AND EXPOSURE ANALYSIS

PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0	0 PC	0 PC	0 PC	0 PC	0 PC
INTERMEDIATE	59	3 PC	53 PC	41 PC	3 PC	0 PC
FULL	184	74 PC	0 PC	24 PC	2 PC	0 PC
ALL LEVELS	243	57 PC	13 PC	28 PC	2 PC	0 PC

MISSION 1026-1 INSTR - AFT 12/28/65 PROCESSING AND EXPOSURE ANALYSIS

PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0	0 PC	0 PC	0 PC	0 PC	0 PC
INTERMEDIATE	90	0 PC	71 PC	27 PC	2 PC	0 PC
FULL	150	63 PC	0 PC	37 PC	1 PC	0 PC
ALL LEVELS	240	39 PC	27 PC	33 PC	1 PC	0 PC

MISSION 1026-2 INSTR - FRWD 12/28/65 PROCESSING AND EXPOSURE ANALYSIS

PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0	0 PC	0 PC	0 PC	0 PC	0 PC
INTERMEDIATE	12	0 PC	33 PC	18 PC	0 PC	0 PC
FULL	224	92 PC	0 PC	17 PC	1 PC	0 PC
ALL LEVELS	236	78 PC	2 PC	19 PC	1 PC	0 PC

MISSION 1026-2 INSTR - AFT 12/28/65 PROCESSING AND EXPOSURE ANALYSIS

PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0	0 PC	0 PC	0 PC	0 PC	0 PC
INTERMEDIATE	34	0 PC	79 PC	0 PC	0 PC	0 PC
FULL	194	70 PC	0 PC	12 PC	6 PC	3 PC
ALL LEVELS	228	60 PC	12 PC	25 PC	3 PC	0 PC

PROCESS LEVEL	BASE	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0:01-0:09	0:01-0:13	0:14-0:39	0:10-0:90	0:91-1:34	0:91 AND UP
INTERMEDIATE	0:10-0:17	0:01-0:20	0:21-0:39	0:10-0:90	0:91-1:34	1:35 AND UP
FULL	0:18 AND UP	0:01-0:39	0:14-0:39	0:10-0:90	0:91-1:69	1:70 AND UP

TOP SECRET

CONTROL NO.

TAB

SECTION 10

PERFORMANCE MEASUREMENTS

The photography acquired by both panoramic cameras during Missions 1026-1 and 1026-2 received a MIP rating of 85. A summary is tabulated below of the MTF/AIM resolution values measured by AFSPPF [REDACTED]

The microdensitometer slit used by AFSPPF [REDACTED] was 1 micron by 80 microns.

<u>Mission</u>	<u>Camera</u>	<u>AFSPPF</u>	[REDACTED]
1026-1	FWD	76	80
1026-2	AFT	88	97
1026-2	FWD	85	91
1026-2	AFT	93	90

The details of the measurement and computing techniques, targets measured and target locations are fully reported in the evaluation report published by AFSPPF and are not normally included in this report.

~~TOP SECRET~~

No. [REDACTED]

SECTION 11

OBSERVED DATA

Mission 1026-1 provided photographic coverage of 3 fixed and 2 mobile ground resolution targets. The best measurable performance was demonstrated on Pass D-47 where the Indian Springs high contrast CORN target was resolved to 7.7 feet by both Master and Slave cameras. Two frames later, (45 miles) Southwest of Indian Springs near Pahrump, Nevada, both cameras resolved 12 feet on a mobile medium contrast T-Bar target.

This indicates that on-orbit system resolution capability was at least 130 lines/mm for high contrast targets. The dynamic system resolution test at A/P showed a capability of 194 lines/mm. The on-orbit resolution limit, as computed from vehicle attitude rates and IMC error, was less than one foot along track and 5.8 feet cross track due, principally to earth rotation. This would limit on-orbit resolution to approximately 160 lines/mm. It is highly probable that the loss of resolution, from the limiting 160 lines/mm to the observed 130 lines/mm, is due to atmospheric attenuation and its attendant lowering of contrast.

~~TOP SECRET~~ [REDACTED]

SECTION 12

MISSION 1026-1 STELLAR-INDEX CAMERA

A. COMPONENT ASSIGNMENT

<u>Component</u>	<u>Serial Number</u>
Camera	D-75
Index Reseau	92
Stellar Reseau	93

B. CAMERA DATA AND FLIGHT SETTINGS

Stellar Camera:

Lens	85 mm f/1.8
Exposure Time	2 seconds
Filter Type	None
Film Type	Eastman Type 3401

Index Camera:

Lens	38 mm f/4.5
Exposure Time	1/500 second
Filter Type	Wratten 21
Film Type	Eastman Type 3400

C. POST FLIGHT EVALUATION

Approximately 20 star images were recorded on each frame of stellar photography throughout mission 1026-1 by S/I #D75/92/93. Although some star imagery was elongated due to vehicle motion during shutter open time, star imagery was adequate to determine vehicle attitude.

Four consecutive stellar frames out of 404 recovered frames from mission 1026-1 were affected by faulty shutter operation. Stellar frames 182 and 183 contained no star imagery and no flare fog imagery of any kind. It is assumed that the stellar shutter failed completely closed during the

~~TOP SECRET~~ [REDACTED]

No. [REDACTED]

normal exposure time of frames 182 and 183. Frame 184 and 185 contain gross fogging that reduced the star count in frame 184 to 50% of normal; frame 185 to 0% stars recorded. It is assumed that the stellar shutter failed either partly open or fully open during the normal exposure time of frames 184 and 185. Also, the frame line is exposed between frames 184 and 185 suggesting that the stellar shutter was partly open during film meter. Investigation of the stellar camera shutter anomaly has been initiated to determine the precise cause of the failure.

Minor edge static and no corona discharge marks were observed in stellar photography.

Stellar baffle flare fog was low on all but a few frames. The first 18 frames of stellar photography contain streaks of what is presumed to be particles of jettisoned fuel.

Emulsion cracking parallel to the minor axis of the film begins in frame 264 and continues until the tail end of the roll.

The index camera operated well throughout the mission producing 416 frames of good photography. No index camera malfunctions occurred. Dendritic static and corona discharge marks were absent from all index camera photography.

~~TOP SECRET~~ [REDACTED]

SECTION 13

MISSION 1026-2 STELLAR-INDEX CAMERA

A. COMPONENT ASSIGNMENT

<u>Component</u>	<u>Serial Number</u>
Camera	D-72
Index Reseau	89
Stellar Reseau	85

B. CAMERA DATA AND FLIGHT SETTINGS

Stellar Camera:

Lens	85 mm f/1.8
Exposure Time	2 seconds
Filter Type	None
Film Type	Eastman Type 3401

Index Camera:

Lens	38 mm f/4.5
Exposure Time	1/500 second
Filter Type	Wratten 21
Film Type	Eastman Type 3400

C. POST FLIGHT EVALUATION

S/I #D 72/89/85 operated normally throughout mission 1026-2. Stellar film was expended in frame 55 of pass D 148 after producing 388 frames of acceptable stellar photography containing approximately 20 stars per frame. Dendritic static and corona discharge were absent from stellar and index camera photography. The index camera operation was good throughout mission 1026-2 and produced 134 frames of recovered photography. Stellar/ Index camera operation is rated excellent throughout mission 1026-2.

SECTION 14

VEHICLE ATTITUDE

The vehicle attitude errors for both Mission 1026-1 and 1026-2 were derived from the reduction of the Stellar camera photography. This attitude data is supplied to A/P by NPIC.

The attitude errors for each frame and the attitude control rates are calculated at the A/P computer facility. The computer also plots the frequency distribution of the rates and errors. Figures 14-1 through 14-6 show these distributions for Mission 1026-1 and Figures 14-7 through 14-12 for Mission 1026-2.

The summary table below lists the maximum attitude errors and rates that were experienced during 90% of the FWD camera photographic operations, excluding the first six frames of each operation, and the total range of the errors and rates.

<u>Value</u>	<u>Mission 1026-1</u>		<u>Mission 1026-2</u>	
	<u>90%</u>	<u>Range</u>	<u>90%</u>	<u>Range</u>
Pitch Error (°)	0.65	-0.92 to +0.28	0.55	-0.88 to +0.14
Roll Error (°)	0.24	-0.40 to +0.60	0.56	-0.56 to +0.98
Yaw Error (°)	0.70	-0.56 to 1.45	0.87	-1.10 to +0.65
Pitch Rate (°/hr.)	37.90	-80 to +100	41.08	-85 to +85
Roll Rate (°/hr.)	33.15	-75 to +70	46.52	-95 to +95
Yaw Rate (°/hr.)	28.48	-58 to +54	30.75	-38 to +62

The performance of the attitude control system is comparable to the control systems used on recent missions. The panoramic photography was not degraded by the attitude control system.

-25% BUCKET FORWARD INSTRUMENT FRAMES 1-6 ON EACH OF OMITTED 90 PERCENT

Y PITCH ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)

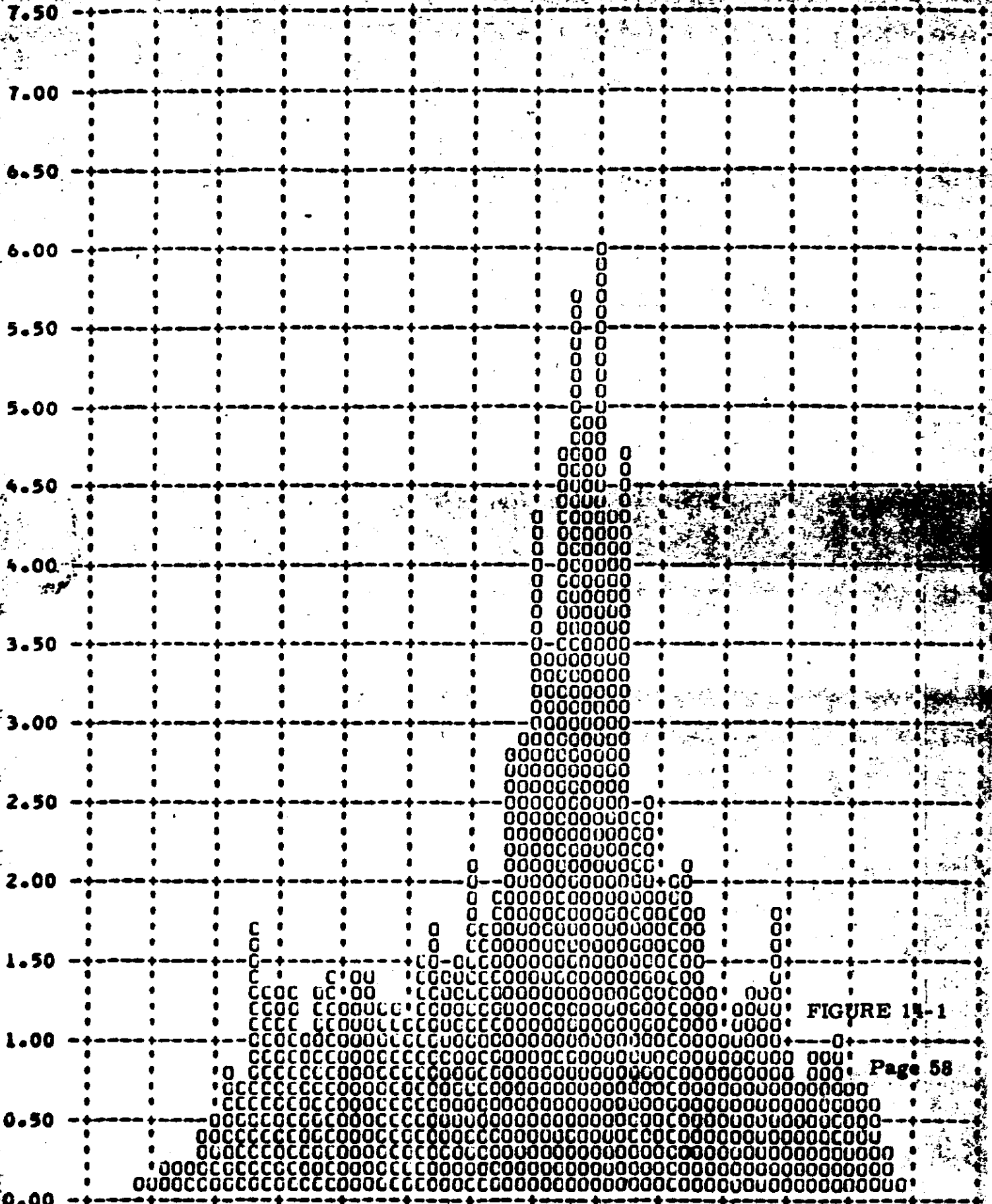


FIGURE 14-1

ROLL ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)

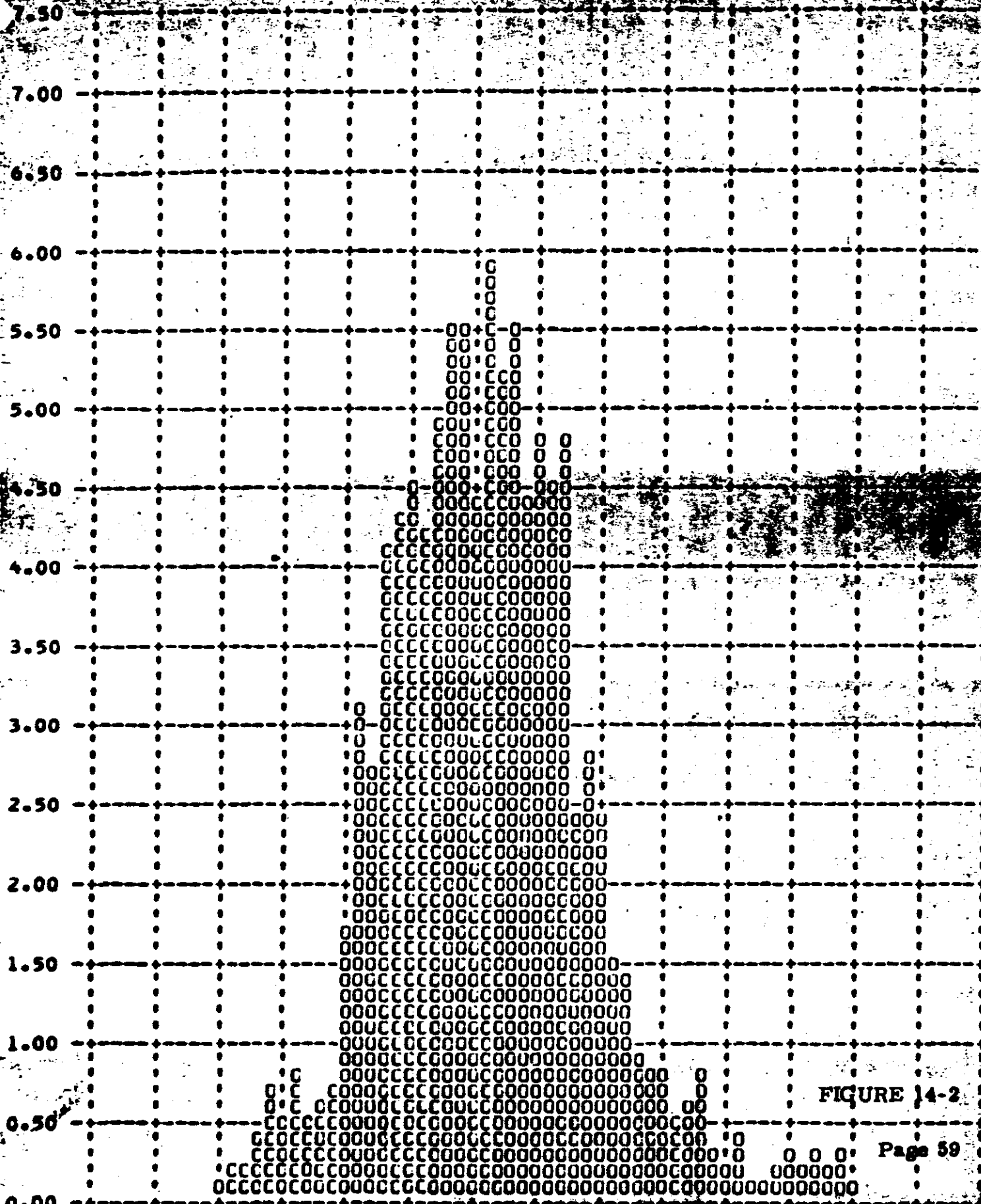


FIGURE 14-2

YAW ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)

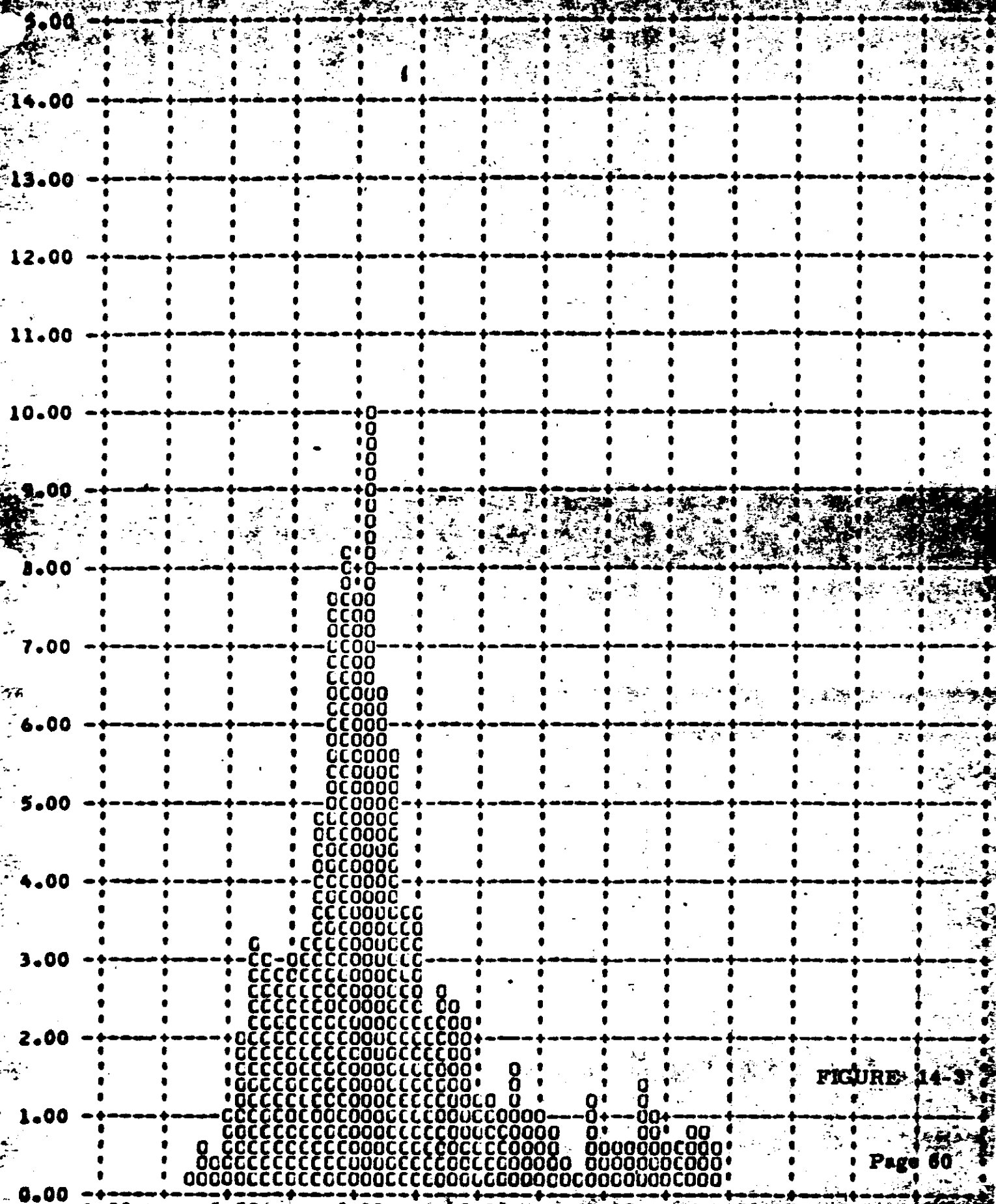


FIGURE 14-3

PITCH RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)

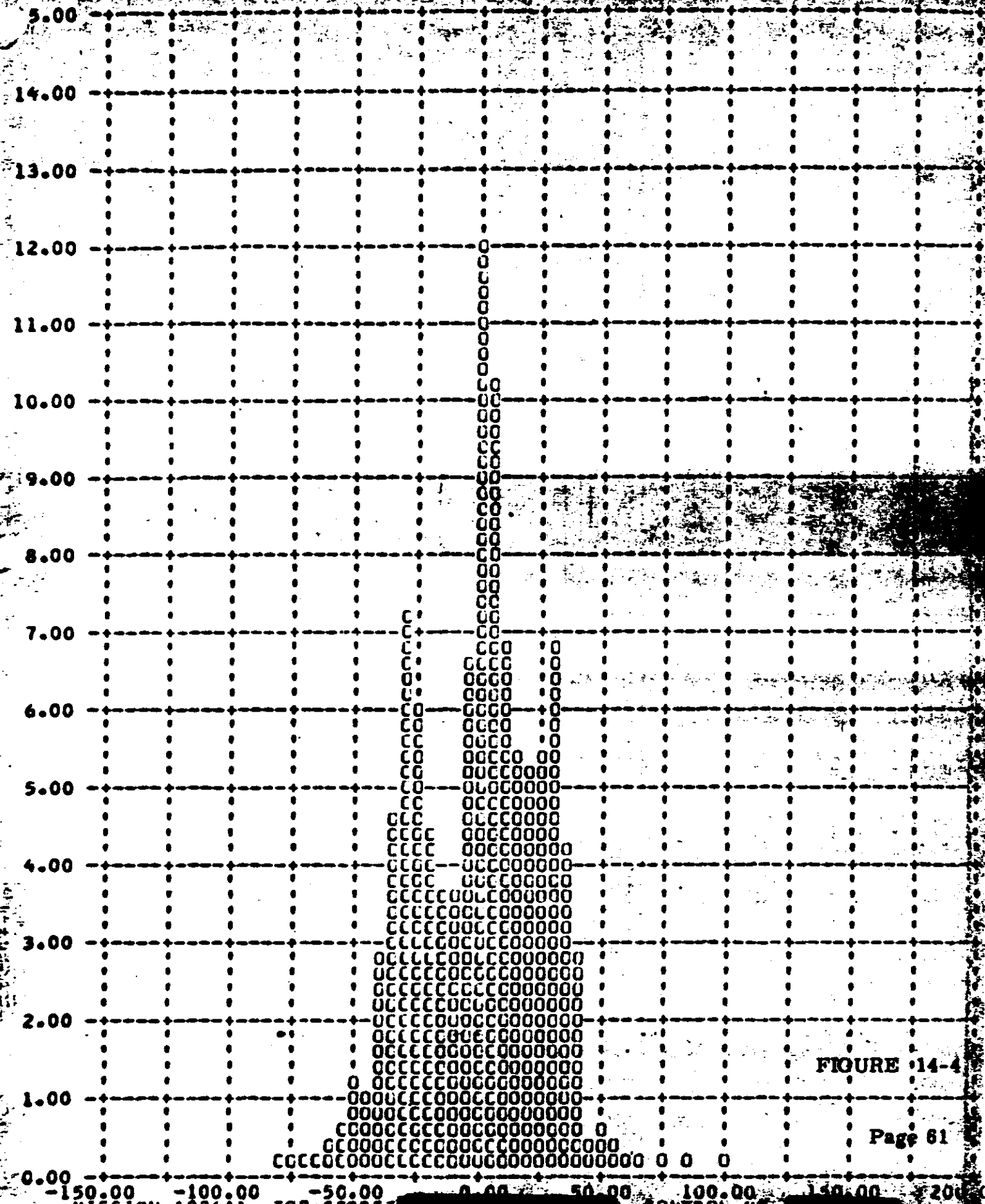


FIGURE 14-4

ROLL RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)

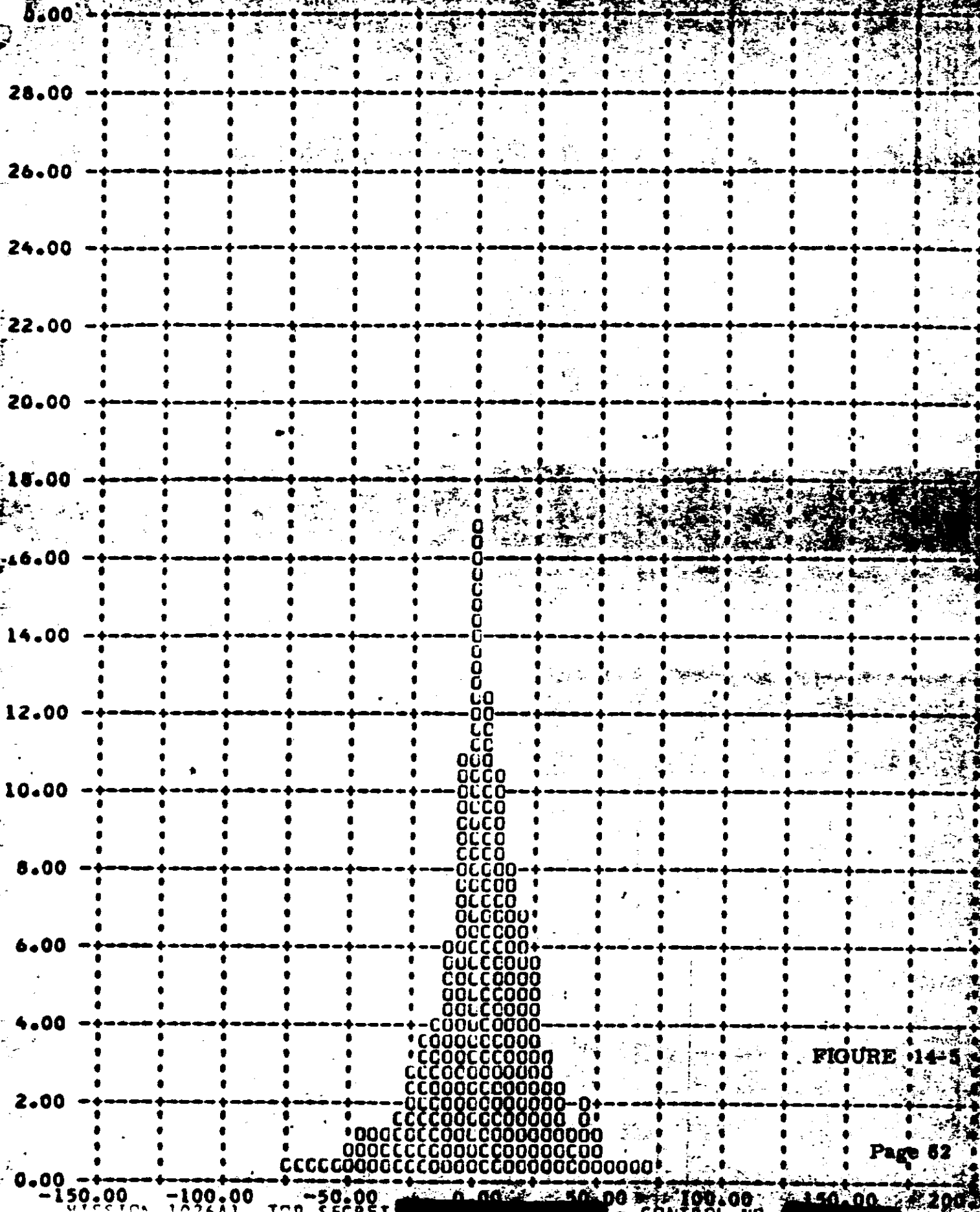


FIGURE 14-5

YAW RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)

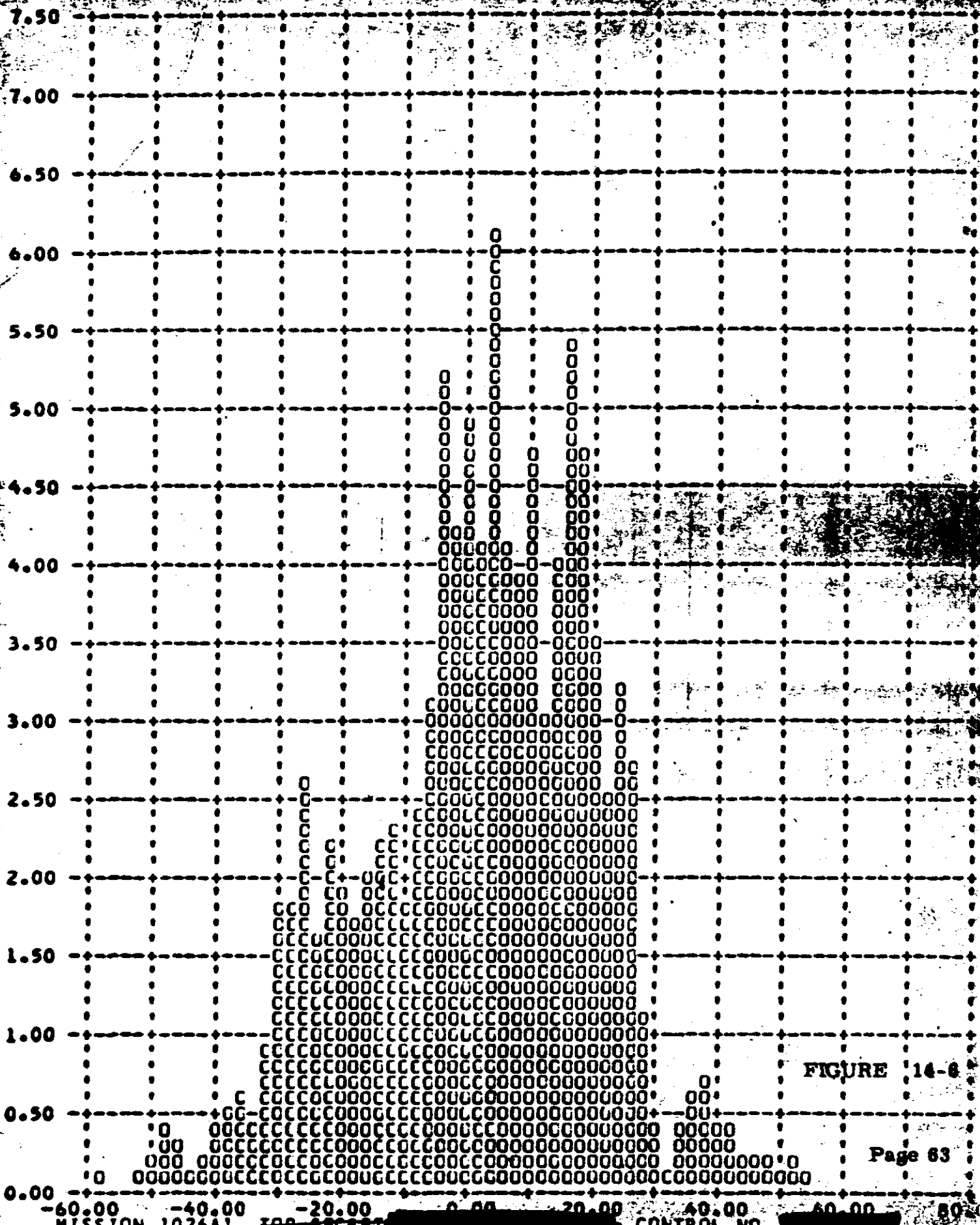


FIGURE 14-6

PITCH ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)

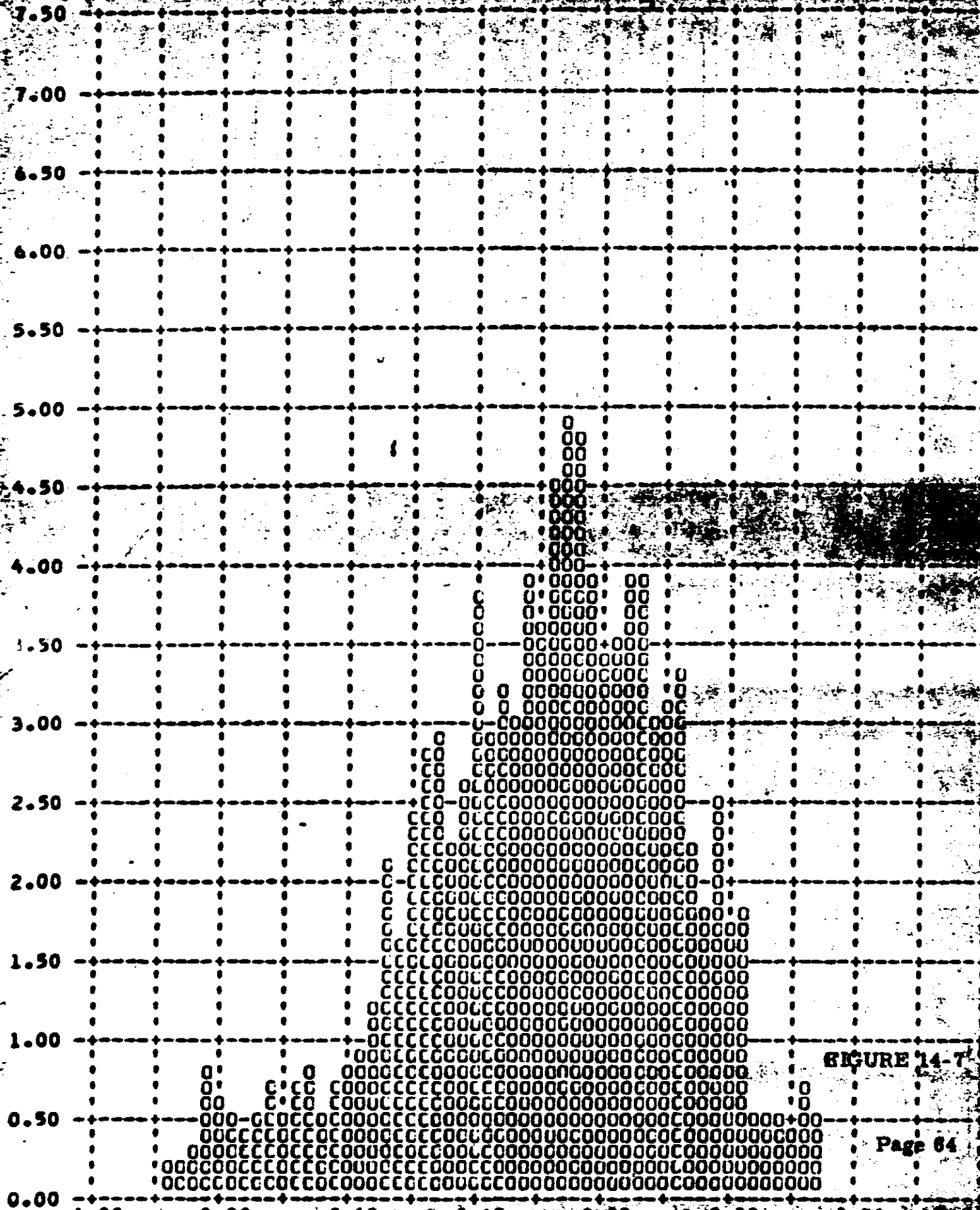


FIGURE 14-7

ROLL ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)

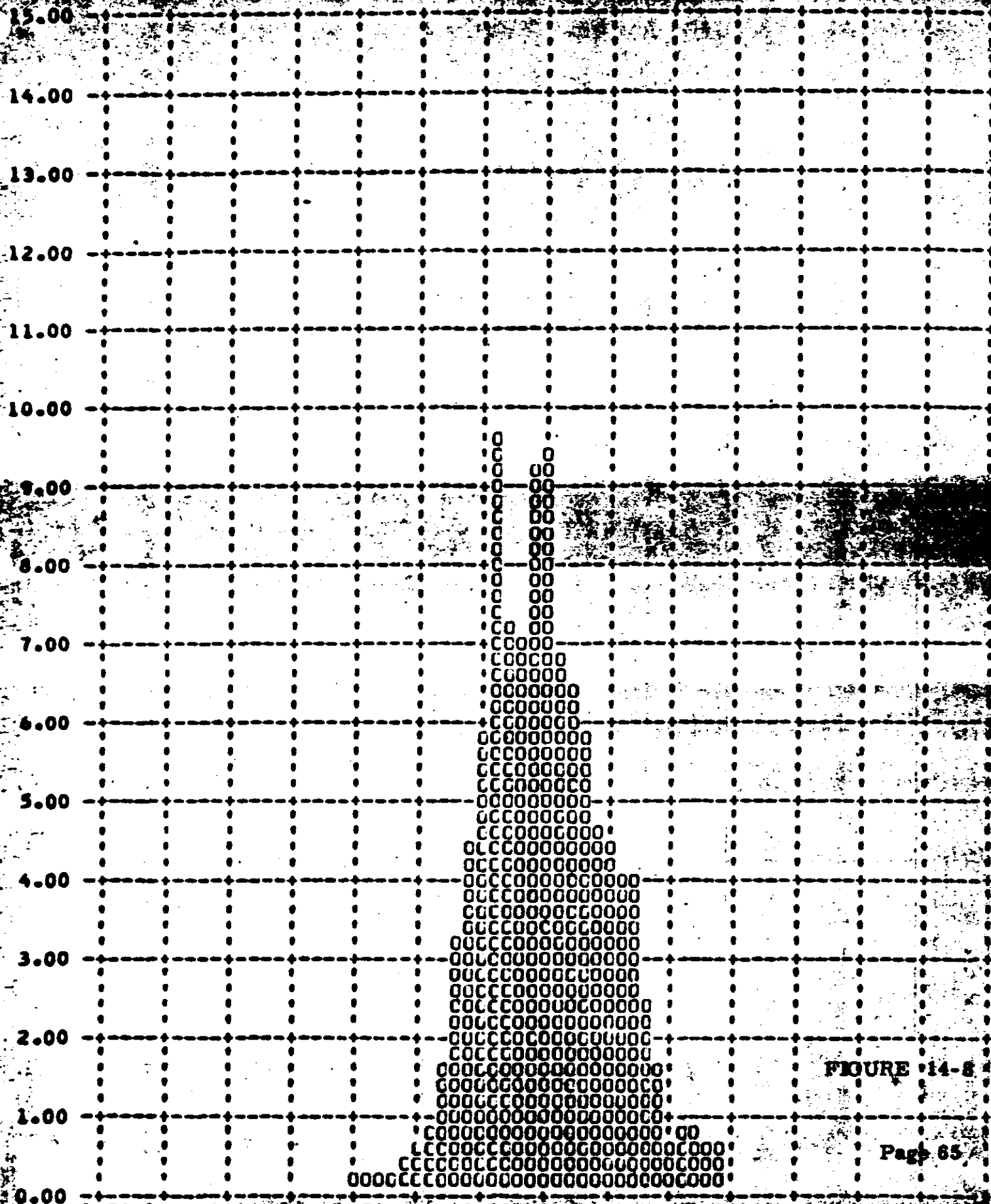


FIGURE 14-5

BUCKET FORWARD INSTRUMENT BEARING ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)

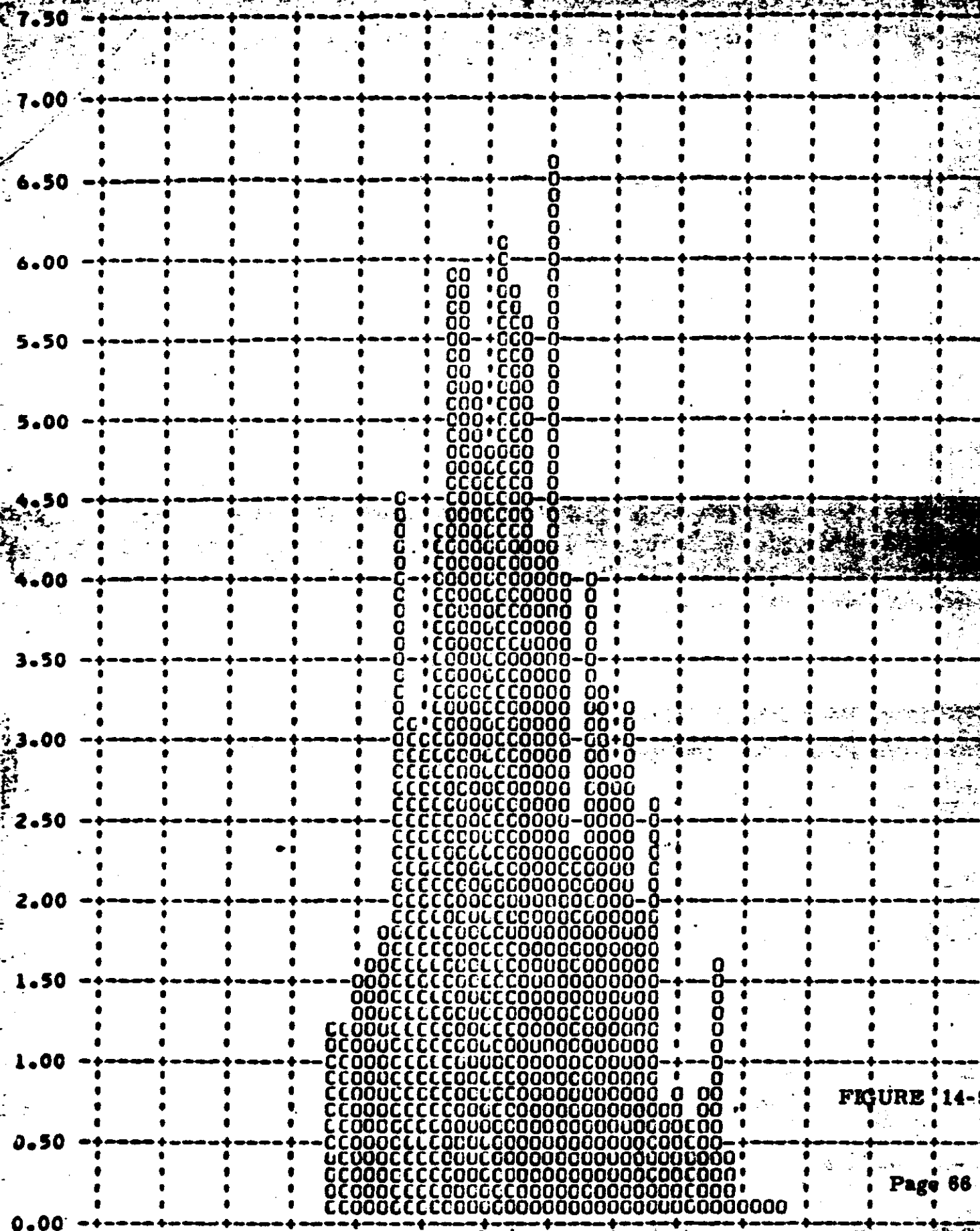


FIGURE 14-9

PITCH RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)

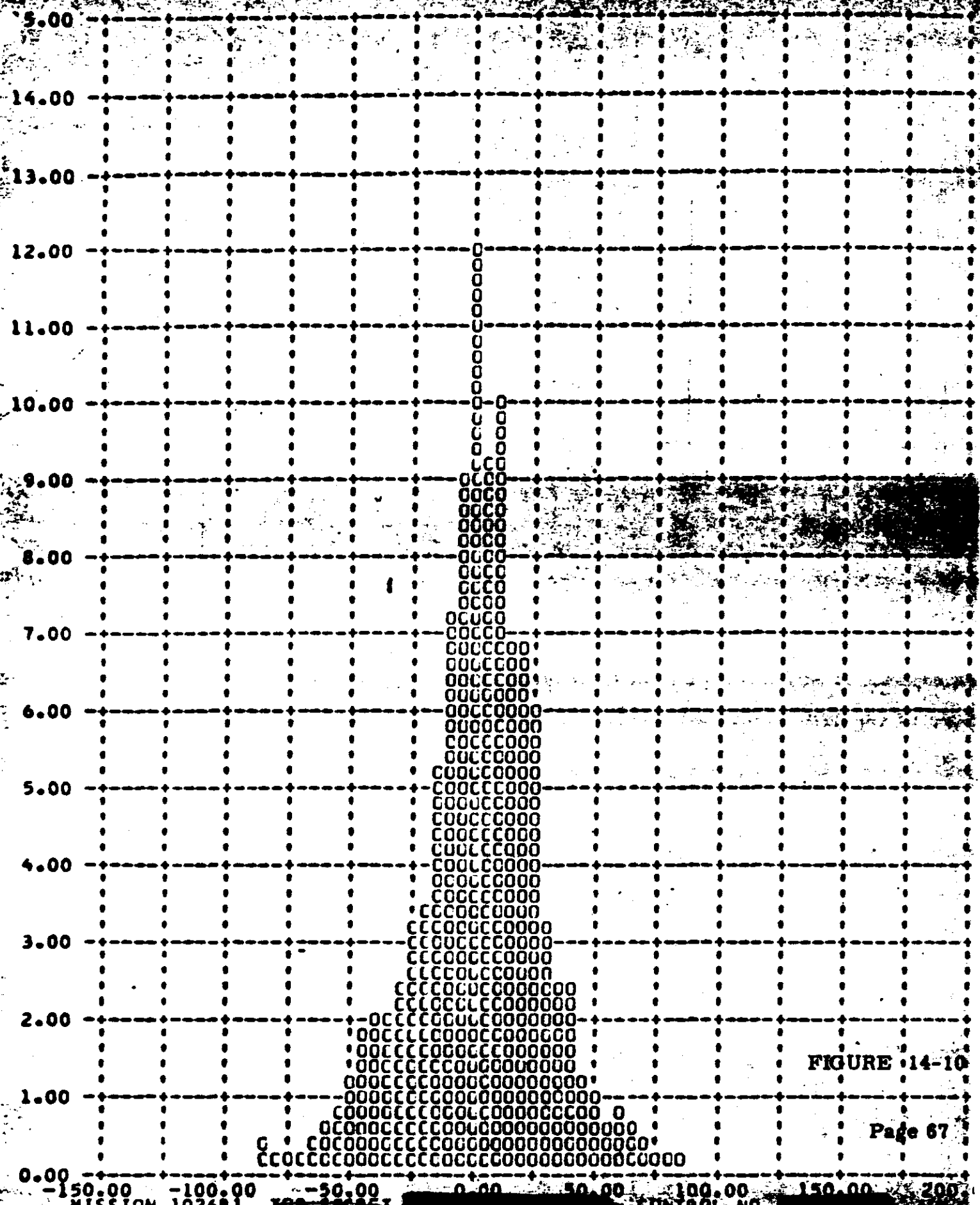


FIGURE 14-10

ROLL RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)

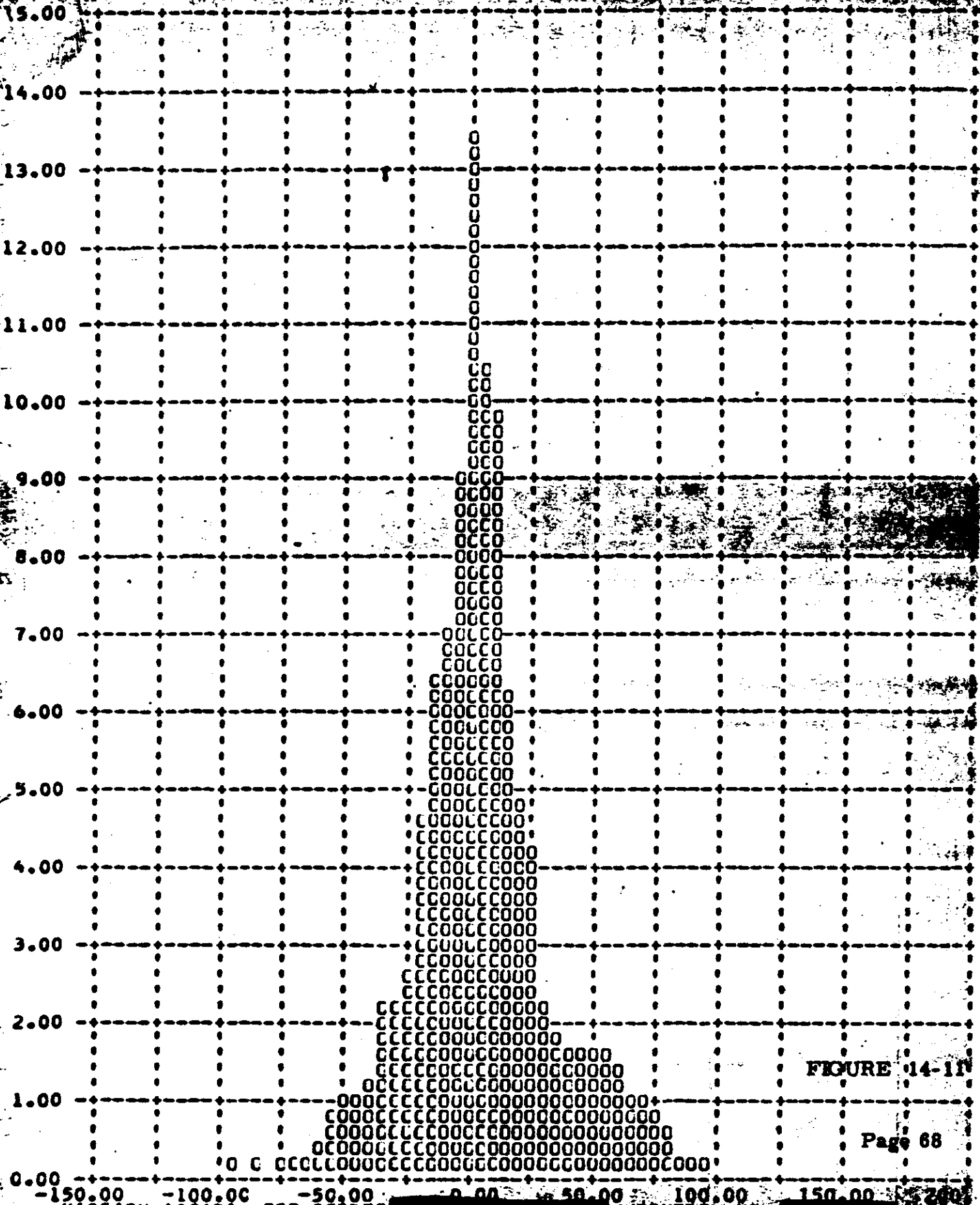


FIGURE 14-11

J-22 B-BUCKET FORWARD INSTRUMENT FRAMES 1-4-68

YAW RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)

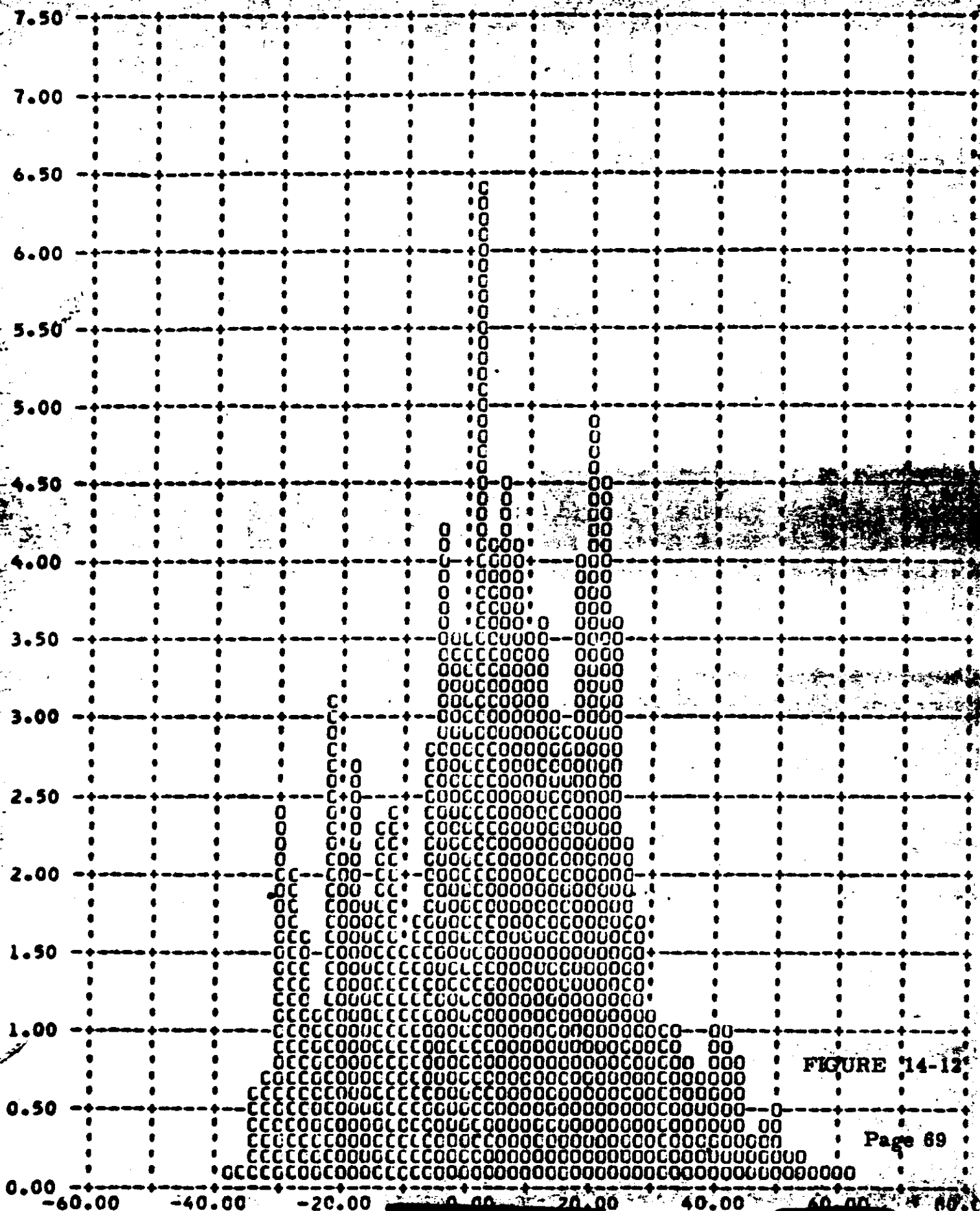


FIGURE 14-12

SECTION 15

IMAGE SMEAR ANALYSIS

The frame correlation tape supplied to A/P by NPIC contains the binary time word of each frame of photography. A computer program has been assembled at A/P which calculates the exposure time of each frame and compares the camera cycle rate with the ephemeris to calculate the V/h mismatch. This data is combined with the vehicle attitude error and rate values of each frame and the crab error caused by earth rotation at the latitude of each frame. The program outputs the total along track and cross track IMC error and the limit of ground resolution that can be acquired by a camera regardless of focal length and system capabilities.

The computer rejects the first six frames of all operations as the large V/h error induced by camera start-up is not representative of the overall system operations. The frequency distribution of the V/h errors and resolution limits are computer plotted and are shown in Figures 15-1 through 15-12.

The summary table 15-1 presents the maximum V/h ratio errors and resolution limits that existed during 90% of the photographic operations and the total range of values during all operations that were computed.

The high "Along Track Resolution Limit" on the A mission was due to a low perigee. From latitudes 230 to 205 the Pan Camera cycle rate limiter prevented appropriate FMC match. Some operations on the first day also encountered error rates higher than normal, previous to adequate orbit definition and ramp settings.

Passes 34M (Median) and 35M (Median) had along track resolution limits as high as 17.5 feet. This type of pass near orbit tangency at this time of year exceeds the systems capability of matching IMC and the required exposure time. These two passes involved 356 frames. The vehicle H-timer reset error on orbit 33 caused all events on these 2 orbits to occur ten seconds early thereby displacing operations northward.

~~TOP SECRET~~

No. [REDACTED]

MISSION 1026

V/h RATIO AND RESOLUTION LIMITS

VALUE	UNITS	CAMERA	MISSION 1026-1		MISSION 1026-2	
			90%	Range	90%	Range
V/h Ratio Error	%	FWD	6.13	-11.5 to +8.5	6.08	-8.8 to +2.2
		AFT	6.13	-16.5 to +9.0	6.67	-8.2 to +1.4
Along Track Resolution Limit	Feet	FWD	13.50	0.5 to 17.5	5.47	0.2 to 7.4
		AFT	9.08	0.2 to 13.8	3.28	0.2 to 4.6
Cross Track Resolution Limit	Feet	FWD	6.16	0.2 to 8.0	6.71	1.8 to 8.4
		AFT	4.11	0.2 to 5.4	4.47	1.4 to 5.2

TABLE 1

~~TOP SECRET~~

V/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY - PERCENT (Y)

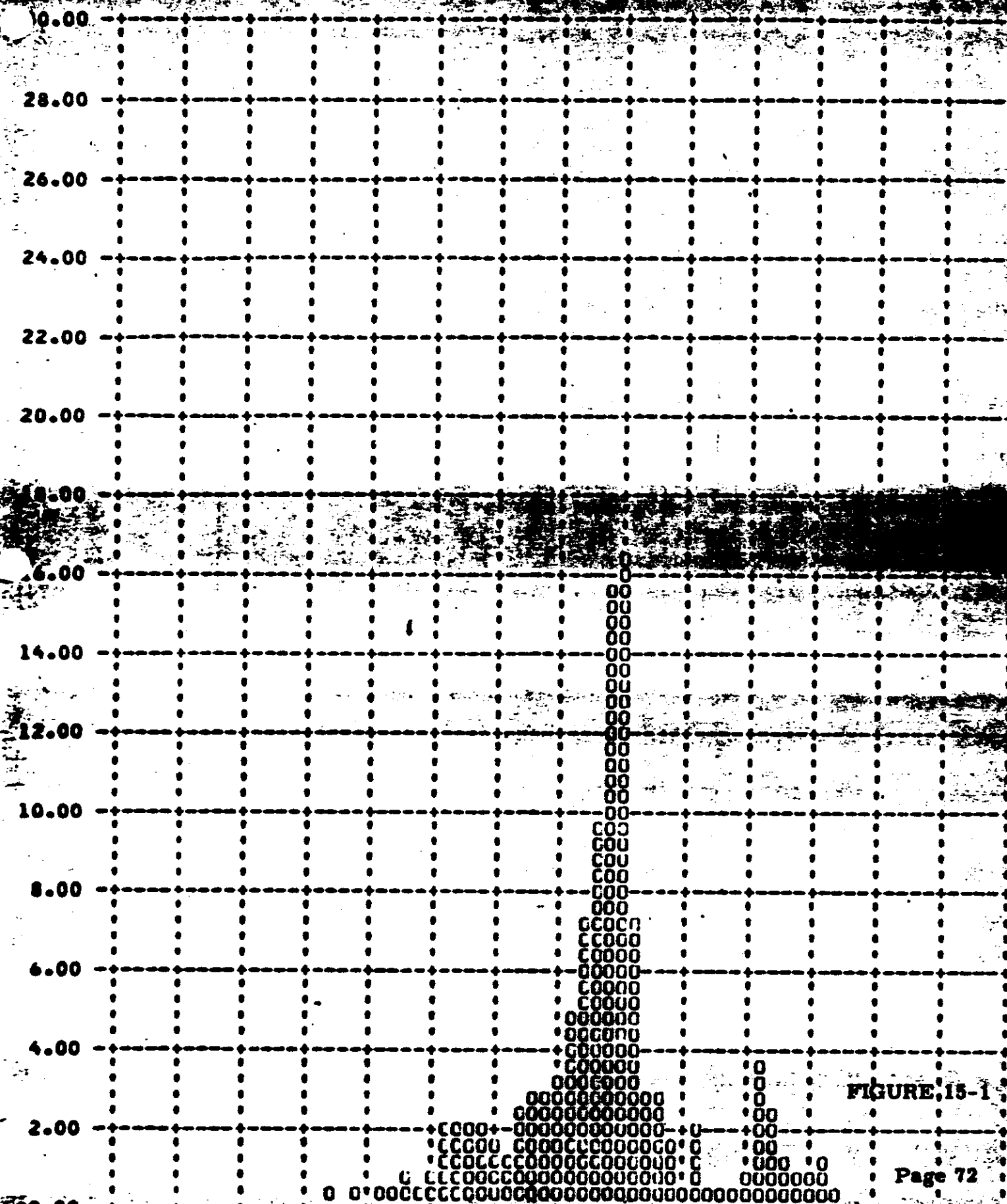


FIGURE 15-1

ALONG TRACK RESOLUTION (LINES) VERSUS FREQUENCY (PERCENT)

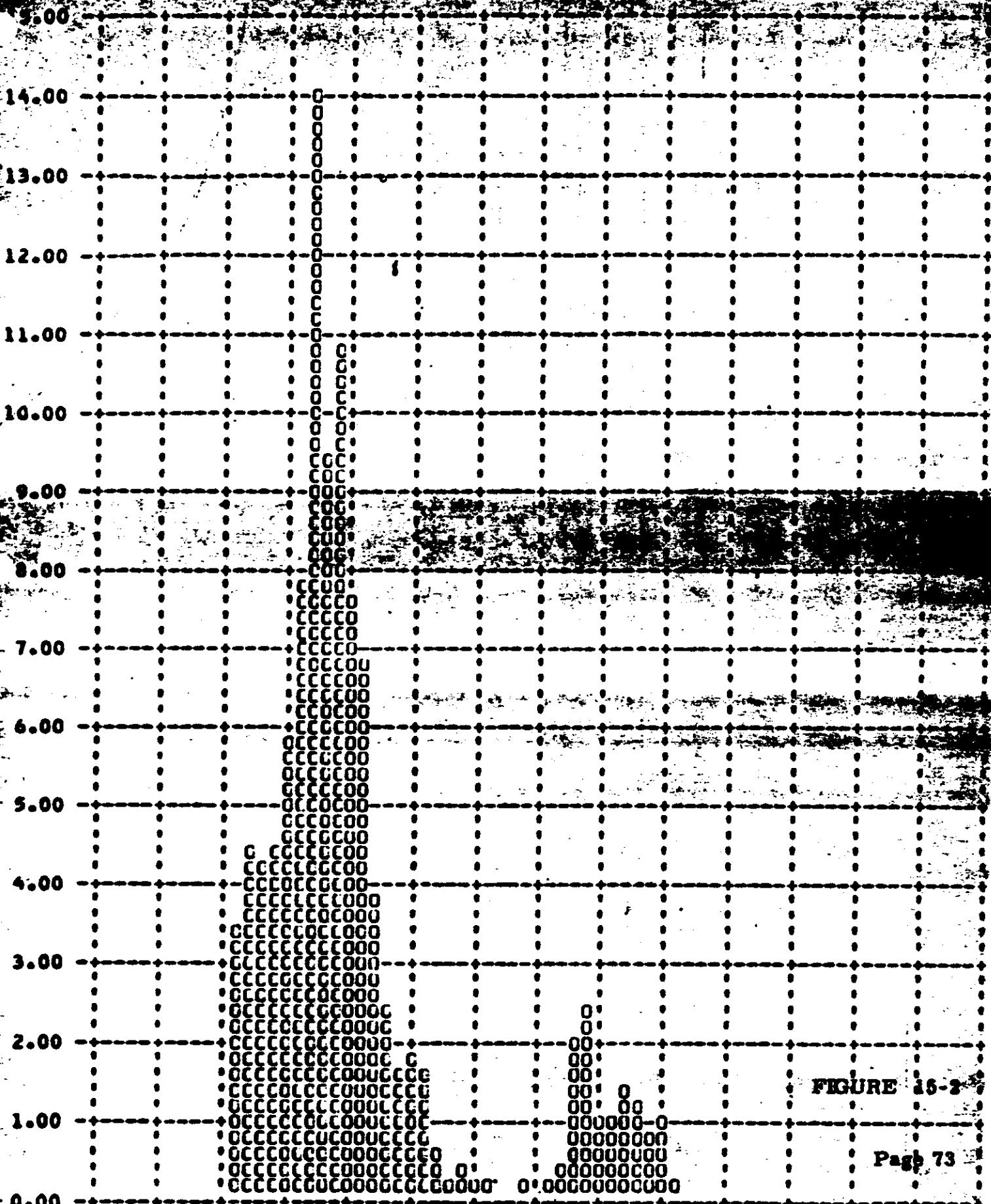


FIGURE 16-3

CROSS TRACK RESOLUTION LIMIT - FEET (%) VERSUS FREQUENCY - PERCENT

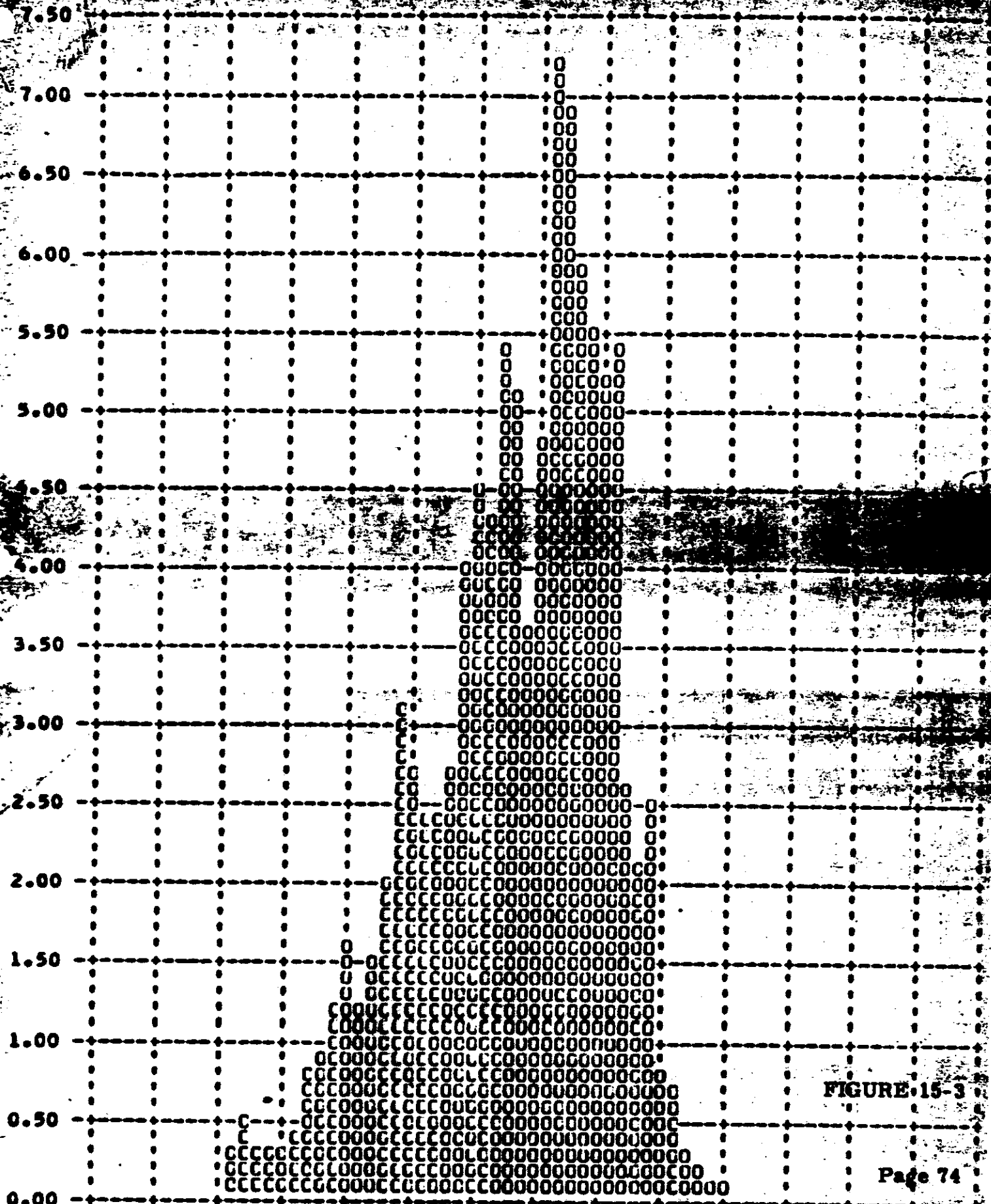


FIGURE 15-3

J-25 A-BUCKET AFT INSTRUMENT FRAMES 1-6 OF EACH OF OMITTED 90 PERCENT

Y V/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY - PERCENT (Y)

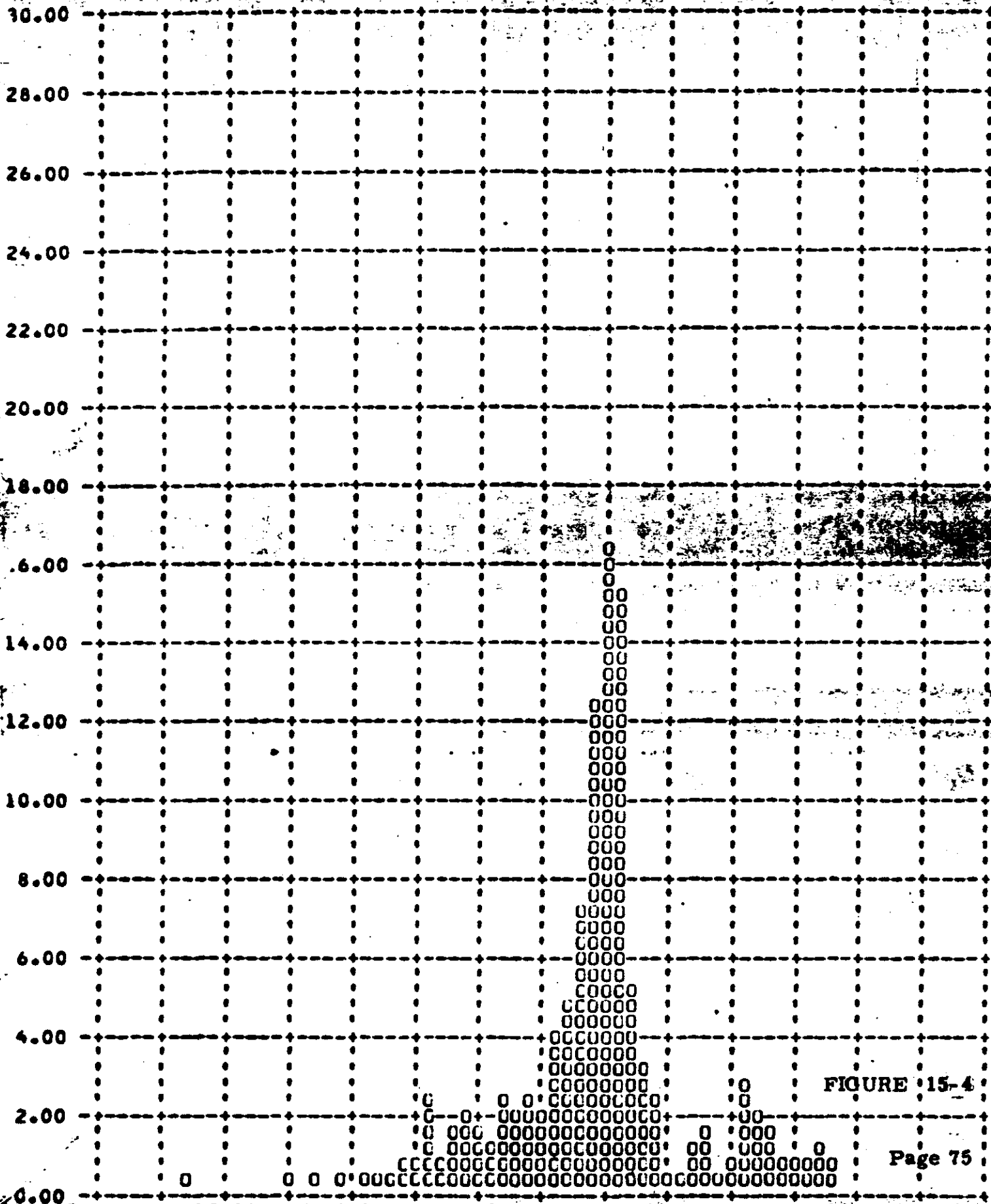


FIGURE 15-4

J-25 A-BUCKET AFT INSTRUMENT - FRAMES 1-6 OF EACH OF OMITTED 90 PERCENT

ALONG TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)

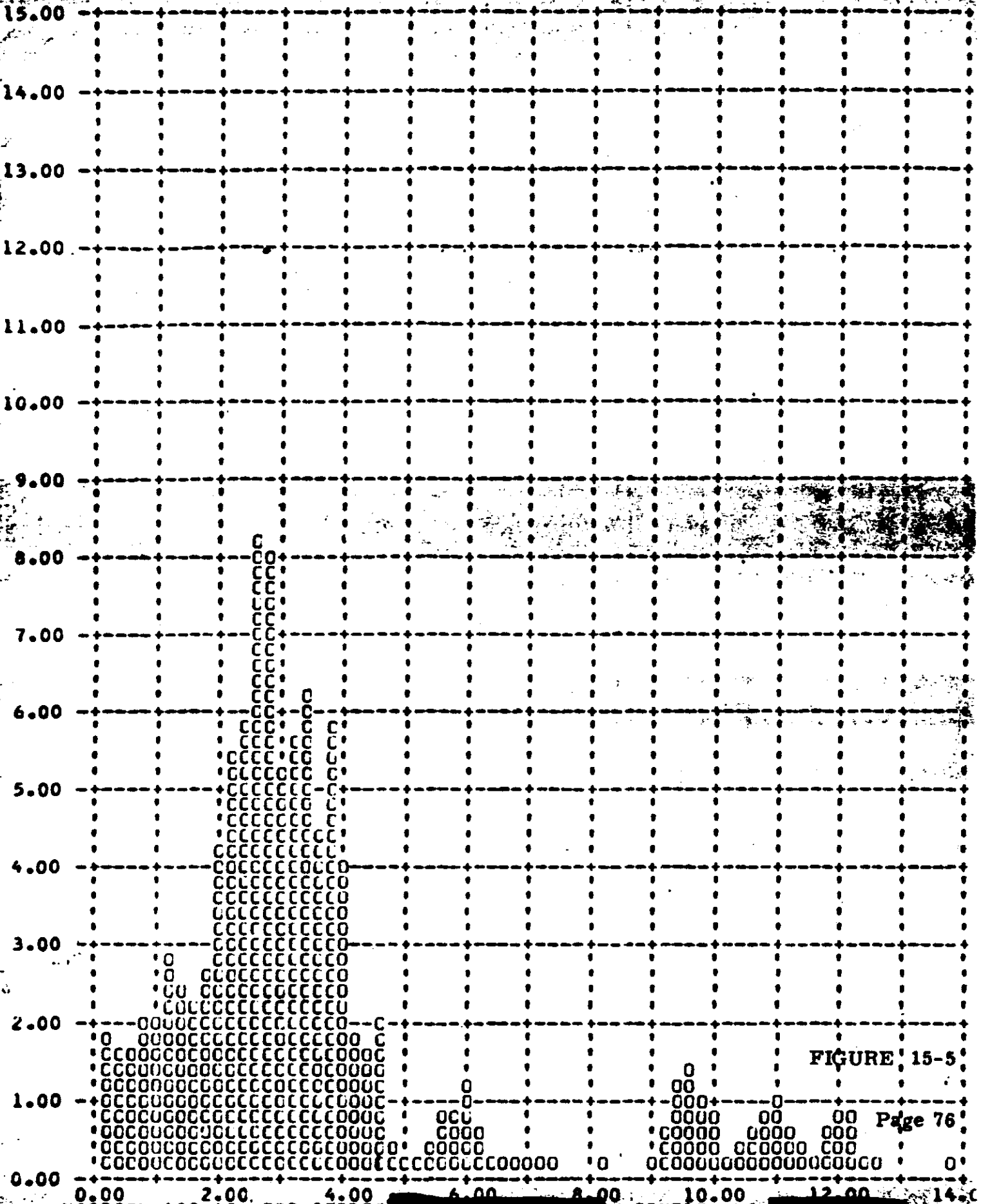


FIGURE 15-5

TICKET A AIRCRAFT ...

CROSS TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)

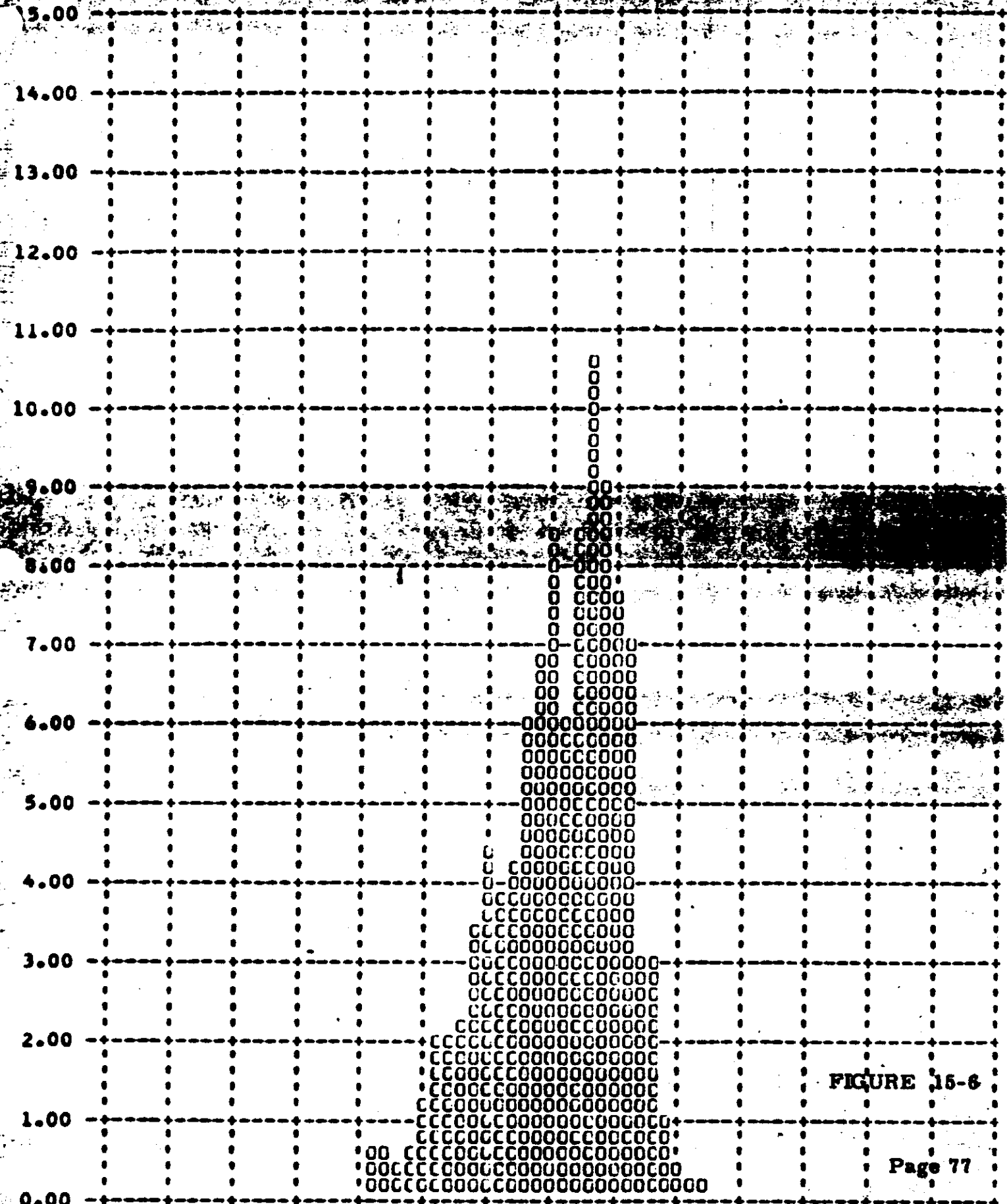


FIGURE 15-6

BUCKET FORWARD INSTRUMENTS 1-6 OF EACH OP. DATED 90 PERCENT
Y V/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY - PERCENT (Y)

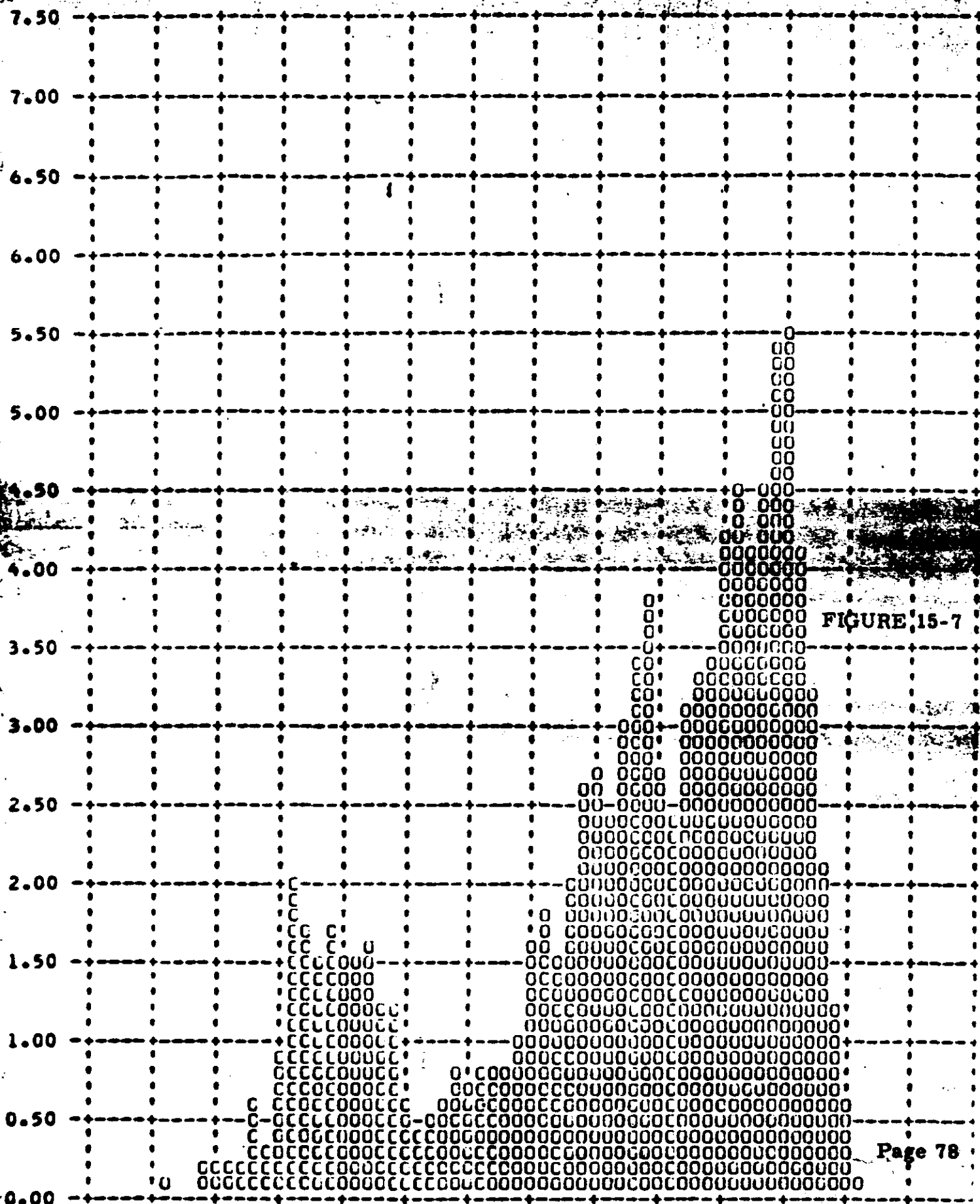


FIGURE 15-7

B-BUCKET FORWARD INSTRUMENTS PLANES 1-6 OF BATH OF DILTED 99 PERCENT

Y ALONG TRACK RESOLUTION LIMIT (PERCENT) VERSUS FREQUENCY (PERCENT)

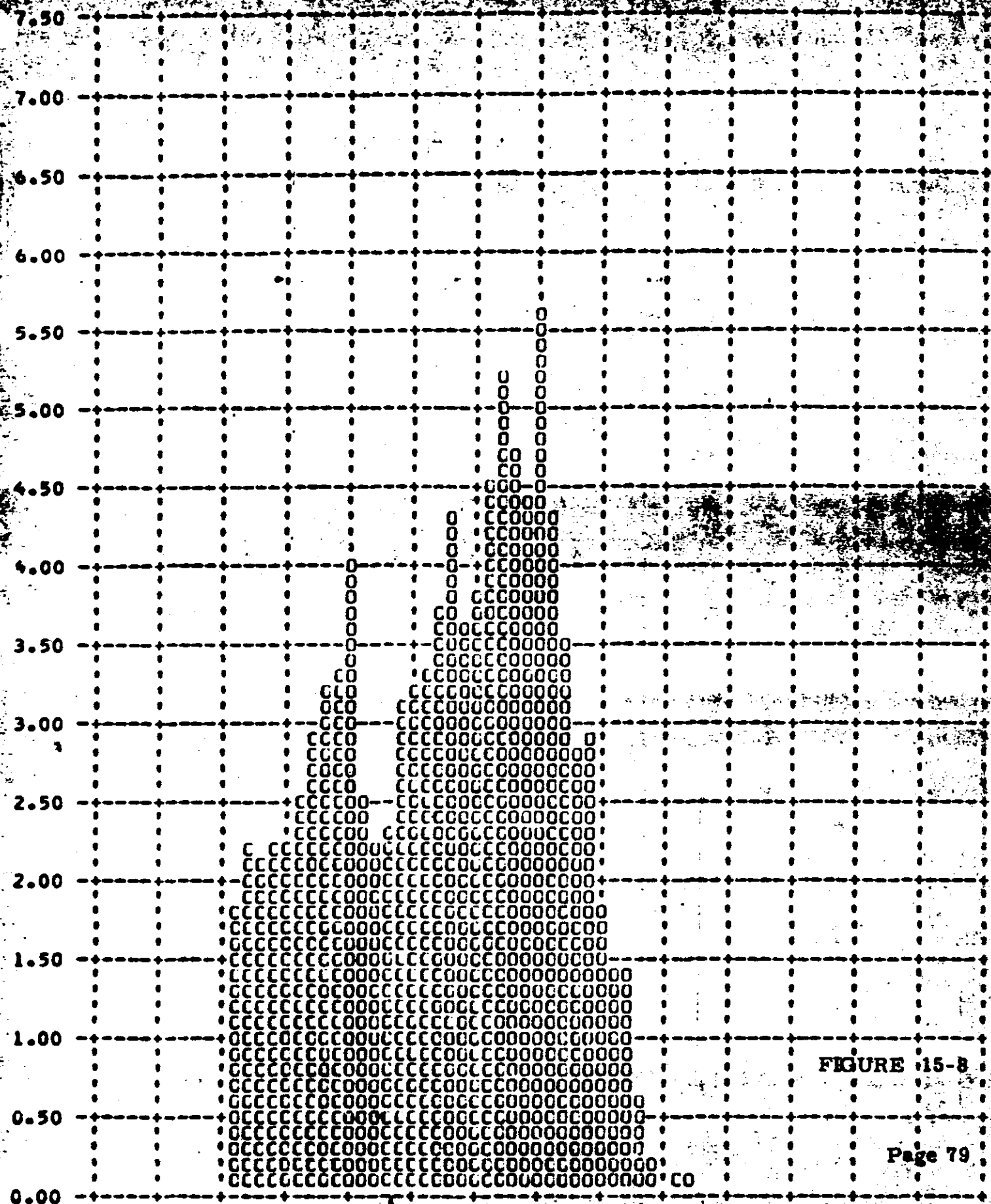


FIGURE 15-8

CROSS TRACK RESOLUTION LIMIT - FEET (Y) VERSUS FREQUENCY - PERCENT

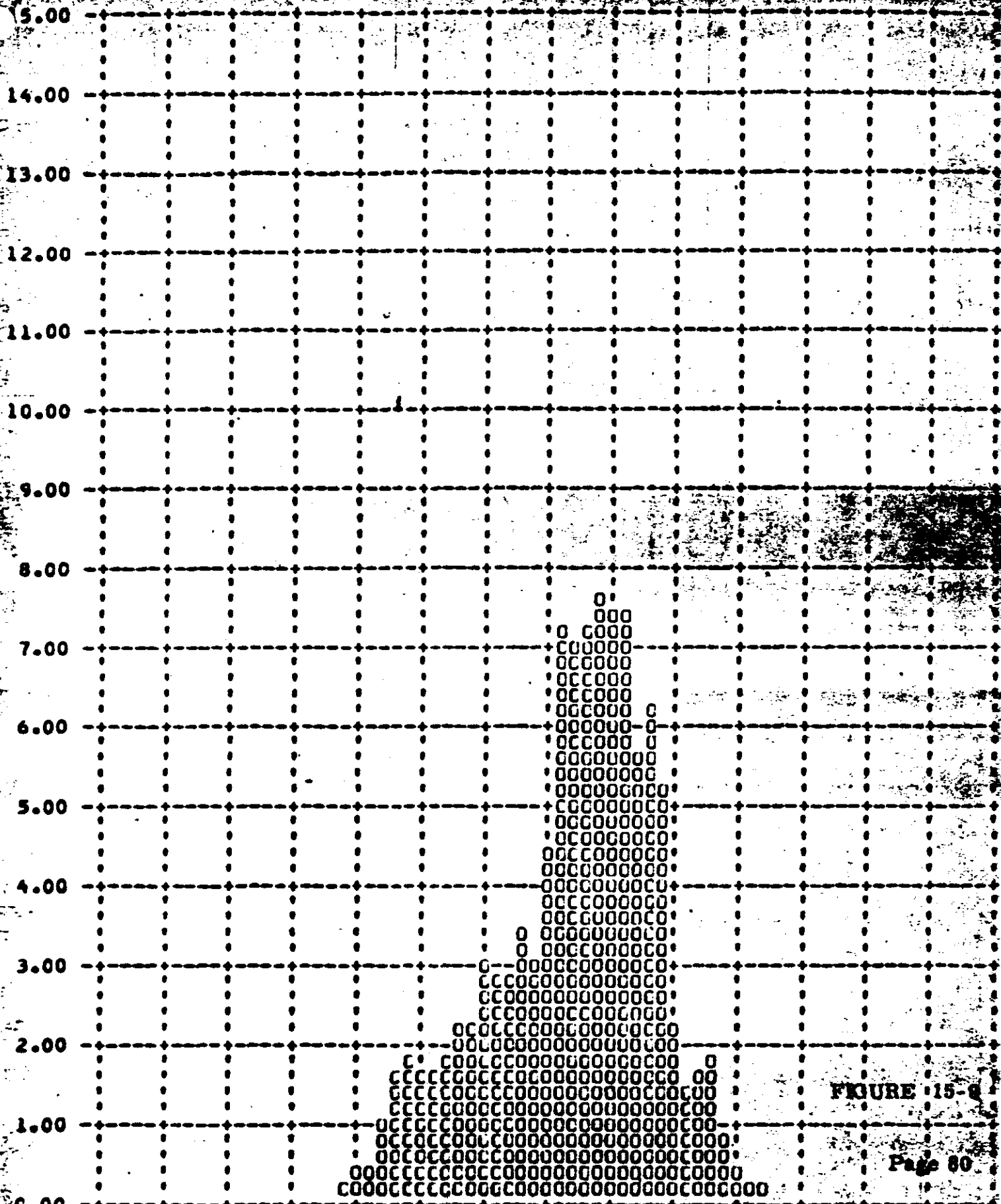


FIGURE 15-9

BUCKET AFT INSTRUMENT FRAME POSITION LIMITED 200 PERCENT

Y/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY - PERCENT (Y)

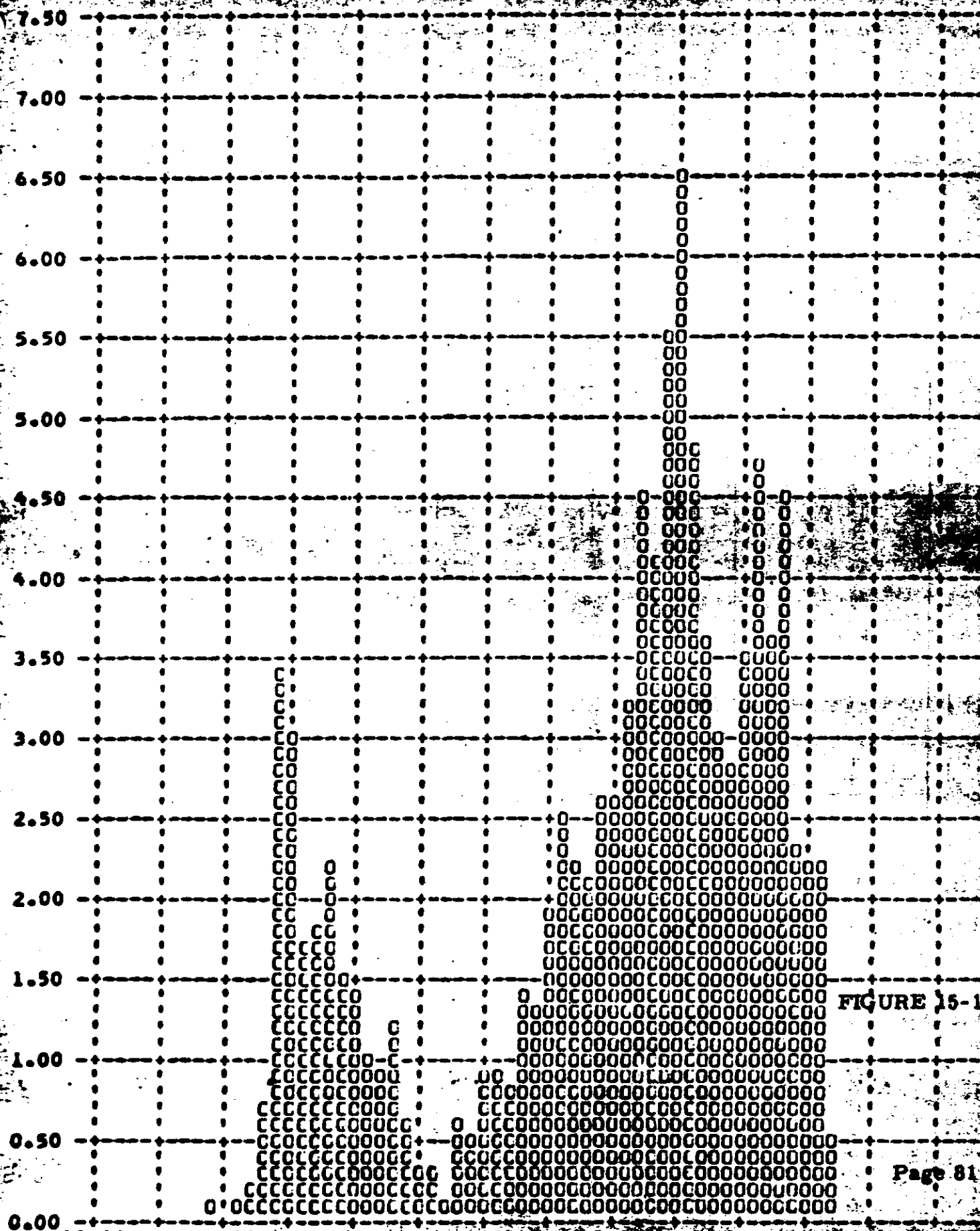


FIGURE 15-10

ALONG TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)

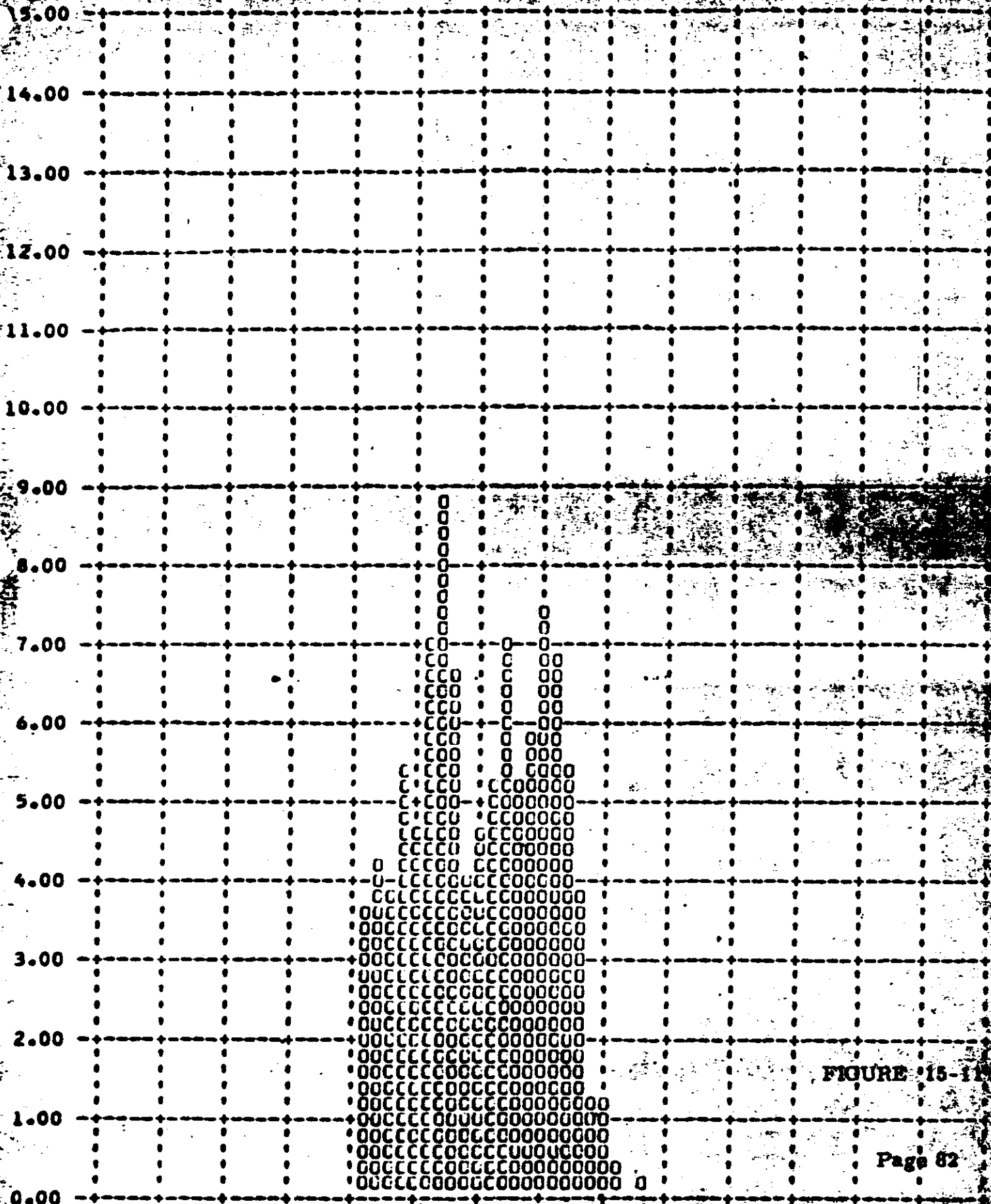


FIGURE 15-11

BUCKET A INSTRUMENT FRAMES 1 OF EACH OF LIMITED 90 PERCENT

CROSS TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)

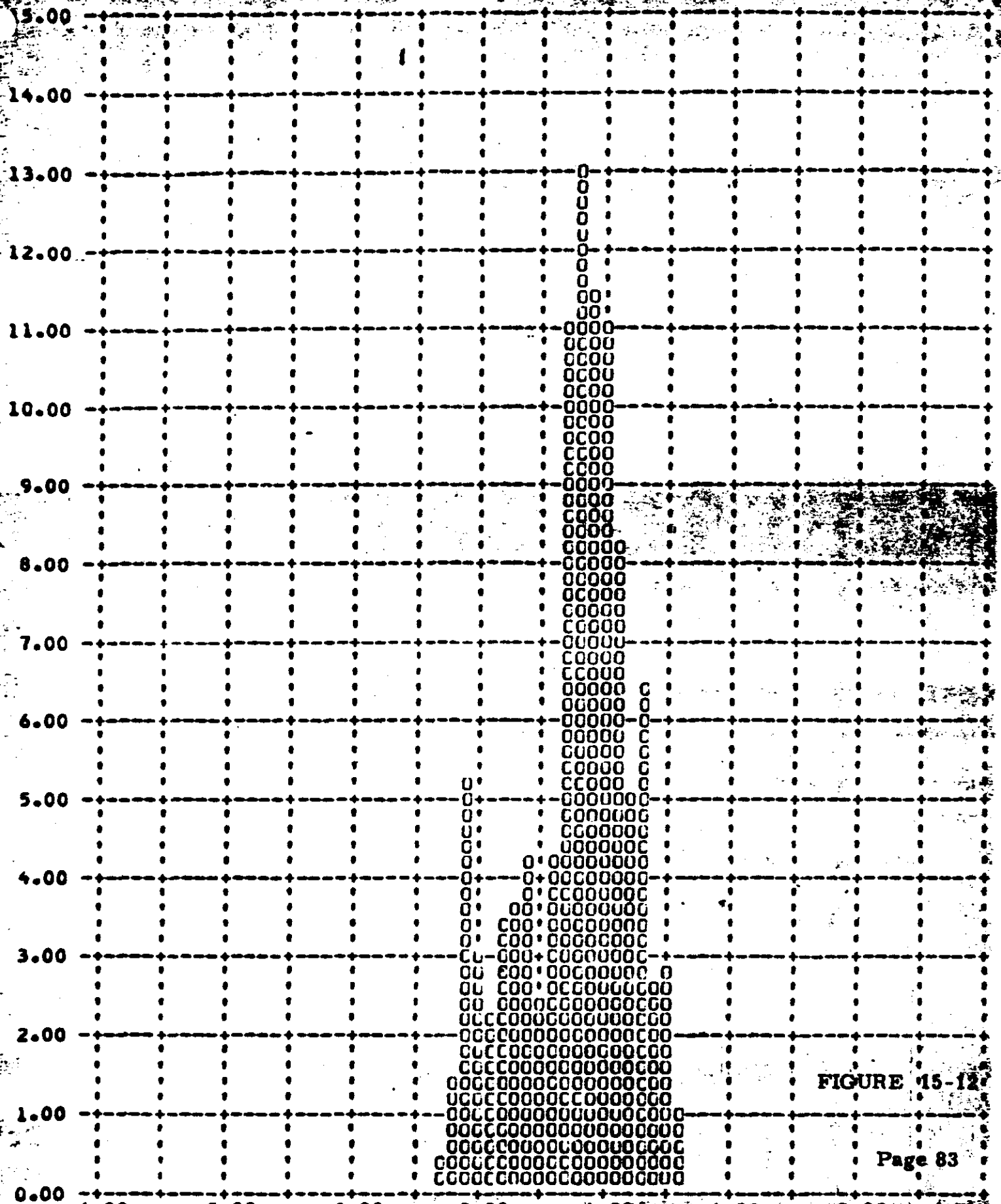


FIGURE 15-12

SECTION 16

RADIATION DOSAGE

Each recovery system flown on a Corona mission contains a sealed packet of Eastman Type 3401 and Royal X Pan emulsions to determine the total radiation received at the take-up cassette. Both film types have been irradiated by LMSC at various levels and the base plus fog densities recorded after controlled processing.

Following recovery the film dosimeter packets are removed at A/P and processed with a pre-flight sample of the same film type and sensitometric control film. The resulting base plus fog density measurement of the dosimeter strips is used to ascertain the total radiation level. The table below presents the base plus fog readings for the dosimeter strips and the radiation level equivalents.

<u>Emulsion</u>	<u>Mission 1026-1</u>		<u>Mission 1026-2</u>	
	<u>B + F Density</u>	<u>Radiation</u>	<u>B + F Density</u>	<u>Radiation</u>
Type 3401	0.15	0.3 R	0.20	0.7 R
Royal X Pan	0.22	0.3 R	0.30	0.6 R

The radiation level on mission -1 was one half of that experienced on mission -2 material. These levels are below that which will degrade the photography.

SECTION 17.**SYSTEM RELIABILITY**

Reliability calculations for the payload are based on a sample beginning with M-7. Hence both the major part of the Mural Program and the "J" Program are covered in the calculation. For certain auxiliaries, i. e., the stellar-index camera and the horizon cameras, the sample size is changed to recognize incorporation of modified equipment or new designs where reliability was one of the principal reasons for the modification. However, for primary mission function, the sample size is consistent with reliability reporting for the vehicle.

The reliability estimates of this section deal exclusively with the payload. Failures to achieve orbit or vehicle induced failures are thereby excluded. Recoveries before a complete mission has been completed are considered as full missions providing that early termination was caused by reasons not connected with payload operation. Film quality is not considered in the reliability estimate calculation. Hence, only electrical and mechanical functioning are considered.

The reliability estimate is also divided into primary and secondary functions. The primary functions are operation of the panoramic cameras, main camera door operation, operation of the payload clock, and recovery operations. The secondary mission functions are horizon camera operation excluding catastrophic open shutter failure mode, auxiliary data recording, and stellar-index camera operation. A summary of estimated reliability is shown in Tables 17-1.

Panoramic Camera Reliability

Sample Size - 126 opportunities to operate.

One failure - capping shutter on slave instrument on system M-7.

Assume - 3000 cycles per camera per mission.

Estimated Reliability = 98.7% at 50% confidence level.

Main Camera Door Reliability

Sample Size - 44 vehicles x 2 doors = 88 opportunities to operate

Estimated Reliability = 99.2% at 50% confidence level

Payload Command and Control

Sample Size - 6720 hours operation in sample

Two failures

Estimated Reliability = 96.3% at 50% confidence level

Payload Clock Reliability

Sample Size - 6720 hours operation in sample

No failures

Estimated Reliability = 99.0% at 50% confidence level

Estimated Reliability of Payload Functioning on orbit = 96.5% at 50% confidence level

Recovery System Reliability

53 opportunities to recover

1 failure - improper separation due to water seal/cutter failure

Estimated Reliability = 96.8% at 50% confidence level

Stellar-Index Camera Reliability

Sample begins with J5

Sample size = 14,740 cycles

Two failures

Estimated Reliability = 92.6 at 50% confidence level

Horizon Camera Reliability

Sample begins with J5 - 63,000 cycles

Estimated Reliability of Single Camera = 98.4% at 50% confidence level

Estimated Reliability of Four Horizon Cameras at a Parallel

Redundant System = 99.9% at 50% confidence level.

TOP SECRET

No. [REDACTED]

ESTIMATED RELIABILITY SUMMARY

(AT 50% CONFIDENCE LEVEL)

SESSION NUMBER	PRIMARY FUNCTIONS						SECONDARY FUNCTIONS			
	PROGRAMMING CAMERA DOORS	COMMAND & CONTROL SYSTEM	PAYLOAD CLOSE	ON - ORBIT FUNCTIONS	RECOVERY SYSTEM	STELLAR - INDEX CAMERAS	HORIZON CAMERAS	RECOVERY SYSTEM	STELLAR - INDEX CAMERAS	HORIZON CAMERAS
	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY
1008 TO 1009	82 97.3	3124 98.6	3124 98.0	3124 98.0	18 90.7	3400 93.1	18,000 91.7	18 90.7	3400 93.1	18,000 91.7
1009	84 97.4	3216 98.7	3216 98.0	3216 98.0	20 91.8	4290 92.3	18,000 90.4	20 91.8	4290 92.3	18,000 90.4
1010	84 97.0	3432 98.8	3432 98.1	3432 98.1	22 92.8	8100 73.7	18,000 94.4	22 92.8	8100 73.7	18,000 94.4
1011	86 97.7	3600 98.9	3600 98.1	3600 98.1	24 93.0	9325 94.7	21,000 96.8	24 93.0	9325 94.7	21,000 96.8
1012	86 97.6	3720 98.9	3720 98.2	3720 98.2	26 93.8	9625 94.7	24,000 98.8	26 93.8	9625 94.7	24,000 98.8
1013	82 97.8	3940 99.0	3940 98.9	3940 98.9	28 94.0	9890 98.1	23,800 98.4	28 94.0	9890 98.1	23,800 98.4
1014	84 97.9	4086 99.0	4086 98.9	4086 98.9	30 94.4	10375 99.8	25,500 98.4	30 94.4	10375 99.8	25,500 98.4
1015	84 98.0	4320 99.0	4320 98.9	4320 98.9	32 94.8	7225 99.8	31,800 98.4	32 94.8	7225 99.8	31,800 98.4
1016	86 98.1	4680 99.0	4680 98.9	4680 98.9	34 95.2	7680 99.8	34,800 98.7	34 95.2	7680 99.8	34,800 98.7
1017	84 98.3	4700 99.0	4700 98.7	4700 98.7	36 96.4	9925 98.3	37,800 97.3	36 96.4	9925 98.3	37,800 97.3
1018	84 98.3	4800 99.1	4800 98.6	4800 98.6	38 96.7	9980 98.3	40,800 97.3	38 96.7	9980 98.3	40,800 97.3
1019	84 98.4	5124 99.1	5124 98.9	5124 98.9	38 96.8	10775 98.3	43,800 97.3	38 96.8	10775 98.3	43,800 97.3

REVISION FOR CHANGED PREVIOUS FAILURE CHARACTERISTICS

TABLE 1-1

TOP SECRET

FORM 100-107-02-00000

ESTIMATED RELIABILITY SUMMARY

(AT 50% CONFIDENCE LEVEL)

MISSION NUMBER	PRIMARY FUNCTIONS				SECONDARY FUNCTIONS			
	PANORAMIC CAMERA	PARAVIEW CAMERA DOORS	COMMAND & CONTROL SYSTEM	PAYLOAD CLOCK	ON - ORBIT FUNCTIONS	RECOVERY SYSTEM	STELLAR - INDEX CAMERAS	HORIZON CAMERAS
	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY	RELIABILITY	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY	SAMPLE FAILURES RELIABILITY
1020	76 1 98.8	0 0 99.1	8344 1 97.1	8344 0 98.9	96.9	43 1 98.1	10,890 2 99.9	48,000 0 97.9
1021	76 1 98.8	0 0 99.1	8376 1 97.0	8376 0 98.8	96.9	41 1 98.0	9330 2 99.1	44,500 0 97.8
1022	80 1 98.8	0 0 99.2	8784 1 97.3	8784 0 98.9	96.9	45 1 98.3	11,860 2 90.7	51,000 0 98.0
1023	82 1 98.8	0 0 99.2	8000 2 98.8	8000 0 98.9	96.2	47 1 98.8	12,190 2 91.1	54,000 0 98.1
1024	84 1 98.8	0 0 99.2	8240 2 98.0	8240 0 98.9	96.3	49 1 98.8	13,040 2 91.6	57,000 0 98.2
1025	86 1 98.6	0 0 99.2	8480 2 96.1	8480 0 98.0	96.4	51 1 98.7	13,990 2 92.1	60,000 0 98.3
1026	86 1 98.7	0 0 99.2	8720 2 98.3	8720 0 98.0	96.8	53 1 98.8	14,740 2 92.6	63,000 0 98.3

~~TOP SECRET~~ [REDACTED]

No. [REDACTED]

SECTION 18

SUMMARY DATA

The comparison of the operating parameters and the performance achieved by previous missions has been difficult due to the large volume of data that results from each mission. Some of the pertinent characteristics from prior missions have been summarized in Tables 18-1 through 18-3.

The summary data was started with Mission 1004 as the J-05 camera system was the first to incorporate the major modifications of the titanium drum and scan arm, four roller scan head and Corona J capabilities. Only those missions that culminated in the recovery of some photography have been listed, therefore Missions 1003 and 1005 are deleted.

~~TOP SECRET~~ [REDACTED]

TOP SECRET

No.

MISSION SUMMARY

MISSION NUMBER	PAYLOAD NUMBER	VEHICLE NUMBER	LAUNCH DATE	L.A. INCH	ORBIT INCLINATION (°)	PERIGEE		RECOVERY PASS	MASTER CAMERA		SLAVE CAMERA		STELLAR CAMERA No. 1 & 2			
						ALTITUDE (NM)	LOCATION (°N)		CAMERA NUMBER	FILTER TYPE	CAMERA NUMBER	FILTER TYPE				
1004	J-08	1174	5/18/64	211 E	74.9	99.9	29.0	49	112	124	0.250	W-21	189	0.250	W-21	048/48/48
1006	J-09	1176	6/4/64	2239 E	79.9	64.0	63.2	66	128	148	0.200	W-21	149	0.200	W-21	048/47/48
1007	J-07	1008	6/18/64	2318 E	88.0	99.2	41.5	68	128	144	0.250	W-25	149	0.200	W-21	043/43/43
1008	J-10	1177	7/10/64	2314 E	86.0	99.4	40.8	49	112	130	0.200	W-21	181	0.200	W-21	048/48/48
1009	J-12	1008	8/9/64	2316 E	80.1	99.6	39.9	49	128	154	0.200	W-21	198	0.200	W-21	056/54/56
1010	J-11	1178	9/14/64	2264 E	64.9	97.4	42.5	68	144	192	0.175	W-21	193	0.175	W-21	041/41/41
1011	J-3E	1179	10/9/64	2150 E	79.9	99.3	20.9	68	—	160	0.175	W-21	181	0.175	W-21	030/30/30
1012	J-13	1179	10/17/64	2202 E	78.0	96.2	32.4	49	81	156	0.200	W-21	187	0.200	W-21	031/31/47
1013	J-15	1178	11/2/64	2130 E	80.0	100.0	29.0	68	81	188	0.225	W-21	189	0.225	W-21	052/49/56
1014	J-16	1180	11/8/64	2036 E	70.0	103.2	65.6	81	148	162	0.250	W-25	139	0.175	W-21	053/59/49
1015	J-17	1007	12/8/64	2110 E	74.9	96.7	21.9	81	178	138	0.250	W-25	141	0.175	W-21	061/61/61
1016	J-18	1008	1/18/65	2101 E	74.9	99.4	30.2	81	189	132	0.250	W-25	133	0.175	W-21	055/55/55
1017	J-14	1011	2/25/65	2144 E	79.0	97.2	28.9	81	148	140	0.250	W-25	168	0.175	W-21	081/81/81
1018	J-19	1012	3/23/65	2111 E	96.0	100.2	40.3	88	99	152	0.250	W-25	123	0.175	W-21	029/29/29
1019	J-04	1014	4/29/65	2144 E	86.0	99.1	27.1	88	—	116	0.250	W-25	119	0.175	W-21	039/39/39
1020	J-20	1013	6/9/65	2158 E	79.1	97.1	40.6	97	115	136	0.250	W-25	137	0.175	W-21	067/67/67
1021	J-21	1016	5/18/65	1803 E	79.0	109.2	24.3	81	201	166	0.175	W-21	167	0.200	W-25	043/43/43
1022	J-22	1017	7/19/65	2201 E	86.0	99.7	30.3	88	144	168	0.250	W-25	169	0.175	W-21	063/63/63
1023	J-23	1016	8/17/65	2100 E	70.0	97.8	29.0	81	144	170	0.225	W-25	171	0.150	W-21	017/17/17
1024	J-24	1019	9/22/65	2131 E	80.0	98.9	18.4	81	161	172	0.225	W-25	173	0.150	W-21	066/66/66
1025	J-25	1016	10/8/65	1746 E	79.0	118.9	40.3	81	167	142	0.175	W-21	187	0.175	W-21	071/71/71
1026	J-26	1020	10/28/65	2117 E	79.0	99.0	17.0	81	165	174	0.225	W-25	179	0.100	W-21	076/76/76

TOP SECRET

TABL

TOP SECRET

No. [REDACTED]

PERFORMANCE SUMMARY

MISSION NUMBER	CAMERA	SERIAL NUMBER	M I P VALUE	VISUAL RES	AT SPL		M I F / A I M		S I C T Y	AVERAGE		30% ATTITUDE ERROR (")		30% ATTITUDE RATES (YAW) / MIN		90% V/N ERROR (D)	90% RESOLUTION LIMIT (FT/IN) ALONG TRACK
					S I C T Y (M)	AVERAGE (M)	S I C T Y (M)	AVERAGE (M)		P I T C H	Y A W	P I T C H	Y A W				
1004-1	FWD AFT	124	85	78	97	109	115	127	124	0.45	0.42	1.08	25.0	21.0	8.1	7.7	
1004-2	FWD AFT	125	85	73	83	113	82	90	85	0.74	0.80	0.91	30.0	29.0	4.9	6.8	
1004-1	FWD AFT	148	90	74	68	88	84	92	88	0.41	0.42	1.14	28.5	27.6	16.4	15.8	
1004-2	FWD AFT	149	90	83	72	80	84	90	87	0.49	0.40	1.08	27.9	30.0	11.6	10.1	
1007-1	FWD AFT	144	85	80	60	87	82	91	82	0.88	0.46	1.43	23.9	29.9	3.6	3.1	
1007-2	FWD AFT	145	85	81	77	83	68	110	74	0.64	0.47	—	—	—	4.6	2.1	
1008-1	FWD AFT	180	85	78	80	95	81	89	81	0.89	0.38	0.94	23.9	29.6	2.9	4.9	
1008-2	FWD AFT	181	85	82	84	94	82	95	85	0.63	0.36	0.71	24.0	32.5	2.8	4.2	
1009-1	FWD AFT	184	85	82	80	—	75	88	88	0.60	0.65	0.71	22.7	27.6	3.3	8.3	
1009-2	FWD AFT	185	85	87	87	—	76	84	72	0.48	0.69	0.59	23.9	27.2	2.6	4.9	
1010-1	FWD AFT	182	85	80	90	86	82	93	87	0.93	0.20	0.87	23.6	30.6	4.9	2.3	
1010-2	FWD AFT	183	85	80	82	85	87	98	85	0.59	0.70	1.21	23.6	30.7	4.6	7.8	
1011-1	FWD AFT	160	90	84	77	86	78	87	83	0.77	0.39	0.97	28.9	31.1	2.3	8.3	
1012-1	FWD AFT	186	85	91	—	91	84	98	89	0.45	0.81	—	38.2	—	1.5	4.8	
1012-2	FWD AFT	187	85	89	—	89	84	91	85	0.97	0.77	0.81	30.7	20.4	8.9	3.3	
1013-1	FWD AFT	188	85	89	—	94	81	103	81	0.84	0.32	1.34	29.0	38.8	2.7	7.8	
1014-1	FWD AFT	142	80	87	—	78	74	86	74	0.62	0.41	1.48	38.0	38.5	2.2	8.8	
1014-2	FWD AFT	139	80	83	—	78	70	77	70	1.08	0.61	1.44	34.8	38.3	2.3	8.8	
1018-1	FWD AFT	138	85	87	—	76	80	86	80	1.06	0.89	—	38.1	—	1.4	8.4	
1018-2	FWD AFT	141	85	83	—	73	80	87	80	0.68	0.38	0.83	29.4	36.2	8.0	8.8	
1018-1	FWD AFT	132	85	85	—	84	81	90	81	0.72	0.83	0.53	29.2	36.2	8.0	8.8	
1018-2	FWD AFT	133	85	85	—	61	54	61	54	0.72	0.83	2.01	30.2	40.4	2.8	8.8	
1017-1	FWD AFT	140	85	72	—	87	78	84	78	0.48	0.76	2.50	32.2	39.5	2.3	8.8	
1017-2	FWD AFT	163	85	85	—	70	80	84	80	0.48	0.78	2.49	32.0	36.5	2.3	8.8	
1018-1	FWD AFT	122	85	79	—	70	82	88	82	0.81	0.48	—	36.7	—	3.4	8.8	
1018-2	FWD AFT	123	85	84	—	74	77	89	77	0.81	0.48	—	36.2	—	3.7	8.8	

DATA NOT PRESENTLY AVAILABLE - TOP SECRET

TABULAR

PERFORMANCE SUMMARY

MISSION NUMBER	CAMERA	SERIAL NUMBER	M I P VALUE	VISUAL RES.	SLIT AVERAGE (μ)	APSPPE MTR/AIM		SLIT AVERAGE (μ)	SLIT AVERAGE (μ)	ALL	HIGH	90% ATTITUDE ERROR (°)			90% ATTITUDE RATES (°/HR)			90% V/M ERROR (°)	90% RESOLUTION (LINE PAIRS)
						SLIT (μ)	AVERAGE (μ)					PITCH	ROLL	YAW	PITCH	ROLL	YAW		
1019-1	FWD APT	118 / 119	88	88	73	80	80	80	80	83	104	0.43	0.37	0.87	31.8	34.7	33.0	3.2	8.3
1020-1	FWD APT	126	88	88	88	80	80	80	80	78	80	0.44	0.38	0.78	37.4	31.8	28.7	3.4	8.9
1020-2	FWD APT	137	88	88	88	80	80	80	80	84	108	0.46	0.38	0.78	37.4	31.8	28.7	3.4	8.9
1021-1	FWD APT	166	88	88	77	80	80	80	80	88	99	0.48	0.37	0.81	34.8	32.6	28.2	2.7	8.8
1021-2	FWD APT	167	88	88	74	80	80	80	80	88	112	0.55	0.38	0.81	34.8	32.6	28.2	2.7	8.8
1022-1	FWD APT	168	88	88	84	80	80	80	80	78	91	0.47	0.31	0.89	28.3	27.1	23.8	3.9	9.8
1022-2	FWD APT	169	88	88	88	80	80	80	80	101	111	0.47	0.31	0.90	27.9	26.6	23.8	3.0	6.2
1023-1	FWD APT	170	88	88	88	80	80	80	80	74	84	0.40	0.31	0.90	29.4	27.3	31.0	2.6	8.0
1023-2	FWD APT	171	88	88	88	80	80	80	80	99	110	0.40	0.31	0.90	29.4	27.3	31.0	1.8	4.9
1024-1	FWD APT	172	88	88	88	80	80	80	80	87	110	0.48	0.33	0.80	33.0	28.7	23.8	3.4	4.9
1024-2	FWD APT	173	88	88	88	80	80	80	80	83	101	0.48	0.33	0.80	32.9	28.7	23.8	3.5	2.7
1025-1	FWD APT	148	88	88	79	80	80	80	80	78	87	0.48	0.37	0.83	29.8	21.3	28.6	2.8	3.9
1025-2	FWD APT	149	88	88	88	80	80	80	80	88	76	0.42	0.35	0.82	32.2	24.9	30.8	2.6	8.9
1026-1	FWD APT	174	88	88	88	80	80	80	80	94	105	0.42	0.35	0.82	32.2	24.9	30.4	2.1	3.8
1026-2	FWD APT	175	88	88	88	80	80	80	80	88	101	0.34	0.31	0.83	30.4	24.8	34.4	3.5	4.7
1027-1	FWD APT	176	88	88	88	80	80	80	80	100	114	0.36	0.31	0.83	30.6	23.8	34.4	3.1	3.7
1027-2	FWD APT	177	88	88	88	80	80	80	80	80	97	0.50	0.41	0.85	28.1	28.7	23.9	2.0	3.9
1028-1	FWD APT	178	88	88	88	80	80	80	80	101	114	0.51	0.42	0.85	28.6	29.7	23.7	2.8	2.8
1028-2	FWD APT	179	88	88	88	80	80	80	80	88	107	0.46	0.34	0.85	37.9	33.2	28.8	6.1	13.8
1029-1	FWD APT	180	88	88	88	80	80	80	80	92	92	0.46	0.34	0.70	37.9	33.2	28.8	6.1	13.8
1029-2	FWD APT	181	88	88	88	80	80	80	80	92	104	0.46	0.34	0.87	41.1	48.8	30.8	6.1	13.8
1030-1	FWD APT	182	88	88	88	80	80	80	80	90	103	0.59	0.55	0.86	43.3	50.0	27.7	6.7	13.8
1030-2	FWD APT	183	88	88	88	80	80	80	80	90	103	0.59	0.55	0.86	43.3	50.0	27.7	6.7	13.8

DATA NOT PRESENTLY AVAILABLE

TOP SECRET

TOP SECRET

No. XXXXXXXXXX

EXPOSURE - PROCESSING SUMMARY

MISSION NUMBER	CAMERA	SOLAR ELEVATION RANGE (°)		SOLAR AZIMUTH RANGE (°)		PREDICTED PROCESSING			REPORTED PROCESSING			COMPUTED PROCESSING			TERRAIN D-MIN			TERRAIN D-MAX			CLOUD D-MAX			UNDER PROCESSED EXP'S	NOMINAL PROCESSED EXP'S	OVER PROCESSED	OVER EXPOSED	CLOUD COVER (%)		
		LOW	HIGH	LOW	HIGH	P	V	F	P	V	F	P	V	F	LOW	HIGH	MEAN	LOW	HIGH	MEAN	LOW	HIGH	MEAN							
1004-1	PWD	5	25	124	7	75	19	4	79	17	0	78	21	0	28	1.89	0.83	0.78	0.43	2.43	1.97	2.02	1.00	2.43	2.04	2	60	31	5	35
1004-1	AFT	-3	81	124	8	74	21	4	79	17	0	80	20	0	28	1.89	0.83	0.78	0.43	2.43	1.97	2.02	1.00	2.43	2.04	2	60	31	5	35
1004-2	PWD	-3	81	124	7	74	21	4	79	17	0	80	20	0	28	1.89	0.83	0.78	0.43	2.43	1.97	2.02	1.00	2.43	2.04	2	60	31	5	35
1004-2	AFT	-4	88	10	131	7	76	17	37	50	13	4	77	19	0	0.73	0.81	0.73	0.38	2.30	1.89	1.93	0.43	2.46	1.99	0	67	20	9	38
1004-1	PWD	38	86	140	1	99	0	1	51	48	0	91	49	0	23	1.81	0.71	0.88	0.80	2.31	1.88	1.92	1.31	2.40	2.24	0	72	21	1	68
1006-2	PWD	38	86	140	1	99	0	1	51	48	0	91	49	0	23	1.81	0.71	0.88	0.80	2.31	1.88	1.92	1.31	2.40	2.24	0	72	21	1	68
1006-2	AFT	38	86	147	2	98	0	30	41	29	11	89	30	0	11	1.14	0.53	0.50	0.38	2.28	1.49	1.50	1.30	2.33	2.11	2	72	4	0	68
1007-1	PWD	18	49	80	103	0	95	1	20	79	0	85	73	0	25	0.26	0.82	0.58	0.63	2.19	1.48	1.47	1.47	2.90	2.12	0	77	9	3	59
1007-2	PWD	11	49	48	102	0	100	0	10	42	48	6	77	17	0	0.26	0.76	0.55	0.78	2.31	1.52	1.52	1.54	2.39	2.20	1	60	8	1	68
1008-1	PWD	30	51	80	102	0	100	0	4	27	68	0	34	66	0	0.32	0.86	0.62	0.78	2.24	1.58	1.58	1.48	2.39	2.21	2	66	8	1	68
1008-2	PWD	29	56	42	105	0	100	0	3	31	66	0	27	73	0	0.14	0.71	0.72	0.87	2.10	1.57	1.58	1.09	2.40	2.20	1	73	23	1	68
1009-1	PWD	12	49	42	132	0	100	0	1	26	73	0	34	66	0	0.32	0.86	0.62	0.78	2.24	1.58	1.58	1.48	2.39	2.21	2	66	8	1	68
1009-2	PWD	23	58	35	138	2	98	0	4	47	49	0	40	60	0	0.29	0.85	0.64	0.84	2.37	1.53	1.53	1.08	2.50	2.30	4	74	17	0	68
1010-1	PWD	19	47	45	93	0	100	0	13	87	0	91	62	0	0.28	0.82	0.64	0.92	2.26	1.58	1.58	1.11	2.42	2.16	2	78	4	0	68	
1010-2	PWD	18	47	45	93	0	100	0	13	87	0	91	62	0	0.28	0.82	0.64	0.92	2.26	1.58	1.58	1.11	2.42	2.16	2	78	4	0	68	
1011-1	PWD	2	85	33	66	0	67	33	2	47	50	0	37	75	0	0.18	0.99	0.48	0.96	2.35	1.58	1.59	1.21	2.41	2.03	7	76	18	0	68
1012-1	PWD	0	45	38	71	0	64	36	7	56	37	0	65	35	0	0.25	0.93	0.53	0.84	2.30	1.40	1.42	0.90	2.39	2.00	6	68	10	9	68
1012-2	PWD	0	45	38	71	0	64	36	7	56	37	0	65	35	0	0.25	0.93	0.53	0.84	2.30	1.40	1.42	0.90	2.39	2.00	6	68	10	9	68
1013-1	PWD	0	86	28	82	0	84	36	2	7	91	0	33	67	0	0.24	1.48	0.68	0.84	2.26	1.89	1.89	1.10	2.38	1.97	5	74	16	0	68
1014-1	PWD	0	89	13	71	0	21	79	1	38	61	0	63	37	0	0.17	0.99	0.40	0.86	2.36	1.40	1.42	1.01	2.38	1.94	27	39	1	0	68
1014-2	PWD	0	89	14	69	0	31	69	0	13	87	0	36	64	0	0.16	1.26	0.31	0.68	2.36	1.62	1.62	0.42	2.43	1.91	19	42	8	0	68
1016-1	PWD	0	79	-2	71	0	10	90	0	10	90	0	11	89	0	0.22	1.00	0.50	0.46	2.30	1.49	1.49	0.34	2.36	1.72	31	40	2	0	68
1016-2	PWD	0	79	-2	71	0	10	90	0	10	90	0	11	89	0	0.22	1.00	0.50	0.46	2.30	1.49	1.49	0.34	2.36	1.72	31	40	2	0	68
1016-1	PWD	0	69	13	76	0	7	93	1	93	1	91	0	91	0	0.26	1.21	0.58	0.52	2.22	1.37	1.38	0.38	2.40	1.74	17	70	12	0	68
1016-2	PWD	0	69	12	76	0	27	73	0	26	74	0	42	58	0	0.13	0.55	0.31	0.45	2.04	1.67	1.68	0.85	2.44	1.91	17	66	8	1	68
1017-1	PWD	0	84	-4	76	0	19	81	1	27	78	0	40	60	0	0.20	1.65	0.48	0.61	2.35	1.78	1.78	0.60	2.32	2.00	1	77	13	1	68
1017-2	PWD	0	84	-4	76	0	19	81	1	27	78	0	40	60	0	0.20	1.65	0.48	0.61	2.35	1.78	1.78	0.60	2.32	2.00	1	77	13	1	68
1018-1	PWD	6	77	13	134	0	100	0	9	83	28	1	83	16	0	0.19	1.46	0.56	0.58	2.32	1.68	1.68	1.00	2.32	1.98	2	19	7	0	68
1018-2	PWD	6	77	14	134	0	100	0	9	83	28	1	83	16	0	0.19	1.46	0.56	0.58	2.32	1.68	1.68	1.00	2.32	1.98	2	19	7	0	68

TOP SECRET

TAB. 1

TOP SECRET

No.

EXPOSURE - PROCESSING SUMMARY

MISSION NUMBER	CAMERA	SOLAR ELEVATION RANGE (°)		SOLAR AZIMUTH RANGE (°)		PREDICTED PROCESSING			REPORTED PROCESSING			COMPUTO PROCESSING			TERRAIN D-MIN			TERRAIN D-MAX			CLOUD RANGE			D-MAX MEAN	D-MAX MEDIAN	UNDER EXPOSED (CU)	UNDER PROCESSED (CU)	NOMINAL EXP. & PROC. (CU)	OVER PROCESSED (CU)	OVER EXPOSED (CU)	GLASS COVER (CU)
		Low	High	Low	High	P	F	T	P	F	T	Low	High	Mean	Low	High	Mean	Low	High	Mean	Low	High	Mean								
10104	P/W A/P	24 23	70 70	24 21	192 182	0 0	21 26	22 19	32 26	46 19	40 10	46 10	40 10	0.61 0.61	0.26 0.13	1.92 1.70	0.71 0.66	0.80 0.80	2.18 2.06	1.45 1.43	1.90 1.43	0.84 0.80	2.26 2.30	1.94 1.95	2.00 2.02	4	7	64	17	7	45
10204	P/W A/P	20 20	78 78	19 17	186 186	0 0	19 18	13 18	49 36	39 29	41 26	41 26	0.85 0.55	0.23 0.23	1.30 1.20	0.85 0.55	0.80 0.70	2.28 2.20	1.87 1.44	1.90 1.44	1.40 1.22	2.38 2.29	2.10 2.04	2.16 2.10	1	18	76	4	0	102	
10304	P/W A/P	47 48	69 68	18 17	35 33	0 0	64 33	34 17	56 23	29 17	26 17	26 17	0.55 0.33	0.83 0.83	1.20 1.20	0.55 0.33	0.80 0.70	2.20 2.20	1.47 1.44	1.44 1.44	1.44 1.44	1.22 1.22	2.29 2.04	2.10 2.10	0	18	76	5	0	102	
INSUFFICIENT DATA																															
10201-1	P/W A/P	18 14	66 66	14 14	108 108	0 0	99 99	14 14	39 39	47 47	152 43	152 43	0.84 0.84	0.23 0.17	1.90 1.70	0.84 0.84	0.80 0.80	2.18 2.18	1.45 1.45	1.90 1.90	0.97 0.85	2.26 2.30	1.92 1.90	2.00 2.00	8	9	72	11	2	26	
10201-2	P/W A/P	13 13	82 82	13 13	133 133	0 0	100 100	0 0	83 83	22 22	80 80	80 80	0.78 0.78	0.33 0.33	1.38 1.38	0.78 0.78	0.80 0.80	2.28 2.28	1.43 1.43	1.90 1.90	1.04 1.04	2.23 2.23	1.82 1.82	1.85 1.85	14	13	72	6	0	26	
10202-1	P/W A/P	28 27	67 67	26 26	180 180	0 0	89 89	11 11	42 42	81 81	42 42	42 42	0.45 0.37	0.18 0.24	1.48 1.48	0.45 0.37	0.84 0.82	2.42 2.30	1.87 1.83	1.87 1.83	1.32 1.30	2.33 2.24	2.24 2.23	2.29 2.23	30	19	47	3	0	36	
10202-2	P/W A/P	28 28	74 74	21 21	182 182	0 0	92 92	1 1	37 37	62 62	43 43	43 43	0.39 0.39	0.20 0.20	0.99 0.99	0.39 0.39	0.82 0.82	2.45 2.45	1.45 1.45	1.45 1.45	1.16 1.16	2.43 2.43	2.23 2.23	2.28 2.28	35	28	35	1	0	48	
10203-1	P/W A/P	22 20	82 81	8 6	184 163	0 0	93 93	0 0	19 19	27 27	72 42	72 42	0.38 0.38	0.18 0.18	1.28 1.28	0.38 0.38	0.43 0.43	2.41 2.41	1.22 1.22	1.22 1.22	0.87 0.87	2.41 2.41	2.08 2.11	2.11 2.11	20	44	34	2	0	36	
10203-2	P/W A/P	29 28	81 80	13 13	177 178	0 0	17 17	93 93	0 0	19 19	82 72	82 72	0.48 0.48	0.22 0.22	1.38 1.38	0.48 0.48	0.41 0.41	2.03 2.03	1.18 1.18	1.18 1.18	0.90 0.90	2.41 2.41	2.03 2.11	2.11 2.11	13	35	60	2	0	36	
10204-1	P/W A/P	10 8	61 61	24 21	137 136	0 0	100 100	0 0	28 28	72 72	72 72	72 72	0.35 0.35	0.17 0.20	1.74 1.74	0.35 0.35	0.40 0.40	2.25 2.25	1.82 1.82	1.82 1.82	0.38 0.38	2.34 2.34	1.97 2.03	2.03 2.03	27	48	23	0	0	36	
10204-2	P/W A/P	9 9	79 79	11 11	181 181	0 0	100 100	12 12	19 19	69 69	78 78	78 78	0.46 0.46	0.24 0.24	1.17 1.17	0.46 0.46	0.48 0.48	2.40 2.40	1.30 1.30	1.30 1.30	1.01 1.01	2.45 2.45	1.91 1.91	1.99 1.99	13	46	39	2	0	36	
10205-1	P/W A/P	1 0	70 70	-23 -19	151 151	0 0	68 72	32 26	10 8	49 43	44 39	44 39	0.43 0.43	0.18 0.18	1.42 1.42	0.43 0.43	0.37 0.37	2.36 2.36	1.37 1.37	1.37 1.37	0.42 0.42	2.35 2.35	1.81 1.81	1.82 1.82	33	25	38	4	1	36	
10205-2	P/W A/P	1 0	70 70	-21 -18	151 151	0 0	71 71	29 29	3 3	42 35	42 35	42 35	0.45 0.45	0.18 0.18	1.22 1.22	0.45 0.45	0.36 0.36	2.34 2.34	1.32 1.32	1.32 1.32	0.63 0.63	2.29 2.29	1.78 1.78	1.89 1.89	29	21	48	4	0	36	
10206-1	P/W A/P	0 0	87 87	23 21	135 135	0 0	4 4	96 96	0 0	21 21	79 79	79 79	0.38 0.38	0.20 0.20	1.26 1.26	0.38 0.38	0.31 0.31	2.27 2.27	1.22 1.22	1.22 1.22	0.40 0.40	2.28 2.28	1.77 1.87	1.87 1.87	97	13	28	2	0	48	
10206-2	P/W A/P	1 0	72 72	8 8	184 184	0 0	100 100	0 0	5 5	94 94	30 30	30 30	0.36 0.36	0.19 0.19	1.32 1.32	0.36 0.36	0.29 0.29	2.27 2.27	1.08 1.08	1.08 1.08	0.82 0.82	2.44 2.44	1.63 1.63	1.70 1.70	78	27	33	1	0	48	
10206-3	P/W A/P	0 0	87 87	13 13	178 178	0 0	0 0	0 0	2 2	93 93	18 18	18 18	0.32 0.32	0.21 0.21	1.35 1.35	0.32 0.32	0.27 0.27	2.28 2.28	1.08 1.08	1.08 1.08	0.85 0.85	2.28 2.28	1.61 1.61	1.70 1.70	60	18	23	3	0	48	

* DATA NOT PRESENTLY AVAILABLE

~~TOP SECRET~~ [REDACTED]

No. [REDACTED]

SECTION A

APPENDIX

~~TOP SECRET~~ [REDACTED]

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS																				
	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN																		
00	0	0	0	0	0	0	0	0	0	0	0	0																		
01	0	0	0	0	0	0	0	0	0	0	0	0																		
02	0	0	0	0	0	0	0	0	0	0	0	0																		
03	0	0	0	0	0	0	0	0	0	0	0	0																		
04	0	0	0	0	0	0	0	0	0	0	0	0																		
05	0	0	0	0	0	0	0	0	0	0	0	0																		
06	0	0	0	0	0	0	0	0	0	0	0	0																		
07	0	0	0	0	0	0	0	0	0	0	0	0																		
08	0	0	0	0	0	0	0	0	0	0	0	0																		
09	0	0	0	0	0	0	0	0	0	0	0	0																		
10	0	0	0	0	0	0	0	0	0	0	0	0																		
11	0	0	0	0	0	0	0	0	0	0	0	0																		
12	0	0	0	0	0	0	0	0	0	0	0	0																		
13	0	0	0	0	0	0	0	0	0	0	0	0																		
14	0	0	0	0	0	0	0	0	0	0	0	0																		
15	0	0	0	0	0	0	0	0	0	0	0	0																		
16	0	0	0	0	0	0	0	0	0	0	0	0																		
17	0	0	0	0	0	0	0	0	0	0	0	0																		
18	0	0	0	0	0	0	0	0	0	0	0	0																		
19	0	0	0	0	0	0	0	0	0	0	0	0																		
20	0	0	0	0	0	0	0	0	0	0	0	0																		
21	0	0	0	0	0	0	0	0	0	0	0	0																		
22	0	0	0	0	0	0	0	0	0	0	0	0																		
23	0	0	0	0	0	0	0	0	0	0	0	0																		
24	0	0	0	0	0	0	0	0	0	0	0	0																		
25	0	0	0	0	0	0	0	0	0	0	0	0																		
26	0	0	0	0	0	0	0	0	0	0	0	0																		
27	0	0	0	0	0	0	0	0	0	0	0	0																		
28	0	0	0	0	0	0	0	0	0	0	0	0																		
29	0	0	0	0	0	0	0	0	0	0	0	0																		
30	0	0	0	0	0	0	0	0	0	0	0	0																		
31	0	0	0	0	0	0	0	0	0	0	0	0																		
32	0	0	0	0	0	0	0	0	0	0	0	0																		
33	0	0	0	0	0	0	0	0	0	0	0	0																		
34	0	0	0	0	0	0	0	0	0	0	0	0																		
35	0	0	0	0	0	0	0	0	0	0	0	0																		
36	0	0	0	0	0	0	0	0	0	0	0	0																		
37	0	0	0	0	0	0	0	0	0	0	0	0																		
38	0	0	0	0	0	0	0	0	0	0	0	0																		
39	0	0	0	0	0	0	0	0	0	0	0	0																		
40	0	0	0	0	0	0	0	0	0	0	0	0																		
41	0	0	0	0	0	0	0	0	0	0	0	0																		
42	0	0	0	0	0	0	0	0	0	0	0	0																		
43	0	0	0	0	0	0	0	0	0	0	0	0																		
44	0	0	0	0	0	0	0	0	0	0	0	0																		
45	0	0	0	0	0	0	0	0	0	0	0	0																		
46	0	0	0	0	0	0	0	0	0	0	0	0																		
47	0	0	0	0	0	0	0	0	0	0	0	0																		
48	0	0	0	0	0	0	0	0	0	0	0	0																		
49	0	0	0	0	0	0	0	0	0	0	0	0																		
50	0	0	0	0	0	0	0	0	0	0	0	0																		
SUBTOTAL				47	0	0	4	0	0	0	0	0	167	0	0	10	0	0	0	0	0	21	0	0	14	0	0	0	0	0

TOP SECRET

- CONTROL NO.

TABLE A-1

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN
0.51	0	0	0	0	0	0	0	0	0	0	0	0
0.52	0	0	0	0	0	0	0	0	0	0	0	0
0.53	0	0	0	0	0	0	0	0	0	0	0	0
0.54	0	0	0	0	0	0	0	0	0	0	0	0
0.55	0	0	0	0	0	0	0	0	0	0	0	0
0.56	0	0	0	0	0	0	0	0	0	0	0	0
0.57	0	0	0	0	0	0	0	0	0	0	0	0
0.58	0	0	0	0	0	0	0	0	0	0	0	0
0.59	0	0	0	0	0	0	0	0	0	0	0	0
0.60	0	0	0	0	0	0	0	0	0	0	0	0
0.61	0	0	0	0	0	0	0	0	0	0	0	0
0.62	0	0	0	0	0	0	0	0	0	0	0	0
0.63	0	0	0	0	0	0	0	0	0	0	0	0
0.64	0	0	0	0	0	0	0	0	0	0	0	0
0.65	0	0	0	0	0	0	0	0	0	0	0	0
0.66	0	0	0	0	0	0	0	0	0	0	0	0
0.67	0	0	0	0	0	0	0	0	0	0	0	0
0.68	0	0	0	0	0	0	0	0	0	0	0	0
0.69	0	0	0	0	0	0	0	0	0	0	0	0
0.70	0	0	0	0	0	0	0	0	0	0	0	0
0.71	0	0	0	0	0	0	0	0	0	0	0	0
0.72	0	0	0	0	0	0	0	0	0	0	0	0
0.73	0	0	0	0	0	0	0	0	0	0	0	0
0.74	0	0	0	0	0	0	0	0	0	0	0	0
0.75	0	0	0	0	0	0	0	0	0	0	0	0
0.76	0	0	0	0	0	0	0	0	0	0	0	0
0.77	0	0	0	0	0	0	0	0	0	0	0	0
0.78	0	0	0	0	0	0	0	0	0	0	0	0
0.79	0	0	0	0	0	0	0	0	0	0	0	0
0.80	0	0	0	0	0	0	0	0	0	0	0	0
0.81	0	0	0	0	0	0	0	0	0	0	0	0
0.82	0	0	0	0	0	0	0	0	0	0	0	0
0.83	0	0	0	0	0	0	0	0	0	0	0	0
0.84	0	0	0	0	0	0	0	0	0	0	0	0
0.85	0	0	0	0	0	0	0	0	0	0	0	0
0.86	0	0	0	0	0	0	0	0	0	0	0	0
0.87	0	0	0	0	0	0	0	0	0	0	0	0
0.88	0	0	0	0	0	0	0	0	0	0	0	0
0.89	0	0	0	0	0	0	0	0	0	0	0	0
0.90	0	0	0	0	0	0	0	0	0	0	0	0
0.91	0	0	0	0	0	0	0	0	0	0	0	0
0.92	0	0	0	0	0	0	0	0	0	0	0	0
0.93	0	0	0	0	0	0	0	0	0	0	0	0
0.94	0	0	0	0	0	0	0	0	0	0	0	0
0.95	0	0	0	0	0	0	0	0	0	0	0	0
0.96	0	0	0	0	0	0	0	0	0	0	0	0
0.97	0	0	0	0	0	0	0	0	0	0	0	0
0.98	0	0	0	0	0	0	0	0	0	0	0	0
0.99	0	0	0	0	0	0	0	0	0	0	0	0
1.00	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	0	0	0	0	0	0	0	0

TOP SECRET



- CONTROL NO.



TABLE A-1

DENSITY VALUE PRIMARY MIN MAX LIM INTERMEDIATE MIN MAX LIM FULL MIN MAX LIM ALL LEVELS MIN MAX LIM

SUB	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
01	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
02	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
03	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
04	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
05	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
06	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
07	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
08	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
09	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
TOTAL	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000

TOP SECRET [REDACTED] - CONTROL NO. [REDACTED]

TABLE A-1

DENSITY VALUE PRIMARY MIN MAX LIN INTERMEDIATE MIN MAX LIN FULL MIN MAX LIN ALL LEVELS MIN MAX LIN

Table with columns for Density Value, Primary, Intermediate, Full, and All Levels. Rows include numerical data points and a SUBTOTAL row.

TOP SECRET [REDACTED] - CONTROL NO. [REDACTED]

TABLE A-1

DENSITY VALUE PRIMARY MIN MAX LIN INTERMEDIATE MIN MAX LIN FULL MIN MAX LIN ALL LEVELS MIN MAX LIN

DENSITY VALUE	PRIMARY MIN	PRIMARY MAX	PRIMARY LIN	INTERMEDIATE MIN	INTERMEDIATE MAX	INTERMEDIATE LIN	FULL MIN	FULL MAX	FULL LIN	ALL LEVELS MIN	ALL LEVELS MAX	ALL LEVELS LIN
01	0	0	0	0	0	0	0	0	0	0	0	0
02	0	0	0	0	0	0	0	0	0	0	0	0
03	0	0	0	0	0	0	0	0	0	0	0	0
04	0	0	0	0	0	0	0	0	0	0	0	0
05	0	0	0	0	0	0	0	0	0	0	0	0
06	0	0	0	0	0	0	0	0	0	0	0	0
07	0	0	0	0	0	0	0	0	0	0	0	0
08	0	0	0	0	0	0	0	0	0	0	0	0
09	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0
45	0	0	0	0	0	0	0	0	0	0	0	0
46	0	0	0	0	0	0	0	0	0	0	0	0
47	0	0	0	0	0	0	0	0	0	0	0	0
48	0	0	0	0	0	0	0	0	0	0	0	0
49	0	0	0	0	0	0	0	0	0	0	0	0
50	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	0	0	0	0	0	0	0	0
TOTAL	0	0	0	0	0	0	0	0	0	0	0	0

TOP SECRET

- CONTROL NO.

TABLE A-1

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN
2.51	0	0	0	0	0	0	0	0	0	0	0	0
2.52	0	0	0	0	0	0	0	0	0	0	0	0
2.53	0	0	0	0	0	0	0	0	0	0	0	0
2.54	0	0	0	0	0	0	0	0	0	0	0	0
2.55	0	0	0	0	0	0	0	0	0	0	0	0
2.56	0	0	0	0	0	0	0	0	0	0	0	0
2.57	0	0	0	0	0	0	0	0	0	0	0	0
2.58	0	0	0	0	0	0	0	0	0	0	0	0
2.59	0	0	0	0	0	0	0	0	0	0	0	0
2.60	0	0	0	0	0	0	0	0	0	0	0	0
2.61	0	0	0	0	0	0	0	0	0	0	0	0
2.62	0	0	0	0	0	0	0	0	0	0	0	0
2.63	0	0	0	0	0	0	0	0	0	0	0	0
2.64	0	0	0	0	0	0	0	0	0	0	0	0
2.65	0	0	0	0	0	0	0	0	0	0	0	0
2.66	0	0	0	0	0	0	0	0	0	0	0	0
2.67	0	0	0	0	0	0	0	0	0	0	0	0
2.68	0	0	0	0	0	0	0	0	0	0	0	0
2.69	0	0	0	0	0	0	0	0	0	0	0	0
2.70	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	0	0	0	0	0	0	0	0
TOTAL	0	0	0	59	59	57	184	184	171	243	243	228

MISSION 1026-1		INSTR - FRWD		12/28/65		PROCESSING AND EXPOSURE ANALYSIS					
PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC
INTERMEDIATE	59	3 PC	53 PC	41 PC	3 PC	0 PC	3 PC	0 PC	41 PC	3 PC	0 PC
FULL	184	74 PC	0 PC	24 PC	0 PC	0 PC	0 PC	0 PC	24 PC	0 PC	0 PC
ALL LEVELS	243	57 PC	13 PC	28 PC	2 PC	0 PC	2 PC	0 PC	28 PC	2 PC	0 PC
PROCESS LEVEL	BASE + FOG	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0.01-0.09	0.01-0.13	0.14-0.39	0.40-0.90	-----	0.91 AND UP	0.01-0.13	0.14-0.39	0.40-0.90	-----	0.91 AND UP
INTERMED	0.10-0.17	0.01-0.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35 AND UP	0.01-0.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35 AND UP
FULL	0.18 AND UP	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70 AND UP	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70 AND UP

~~TOP SECRET~~ [REDACTED] CONTROL NO. [REDACTED]

TABLE A-1

TOP SECRET

CONFIDENTIAL NO.

MISSION • 1026-1 • INSTR • FRWD • 12/28/65 PLOT OF 0 MIN • TERRAIN • PROCESSING • INTERMEDIATE
ARITH MEAN • 0.40 • MEDIAN • 0.33 • STD DEV • 0.18 • RANGE • 0.20 TO 0.95 WITH 59 SAMPLES

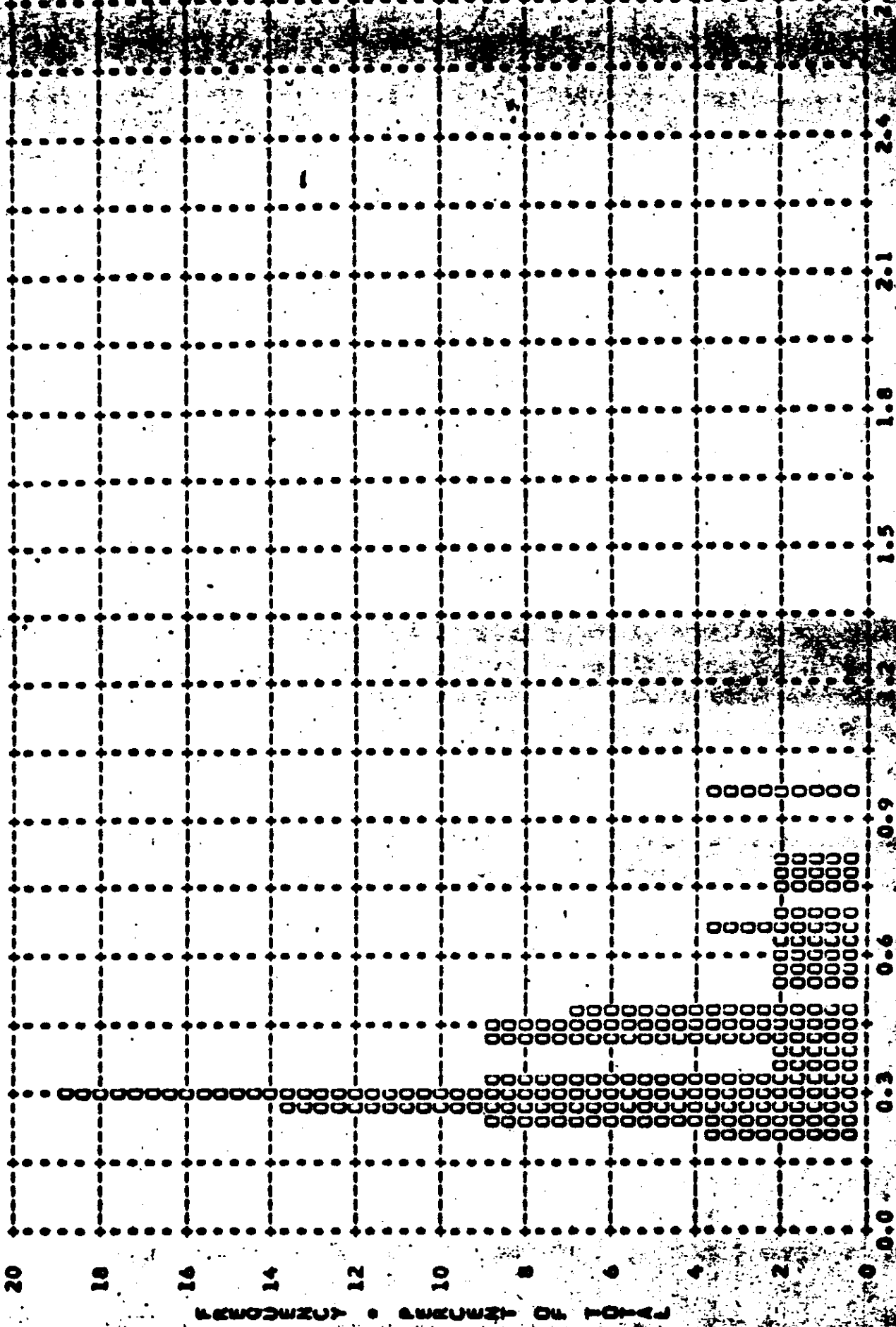


FIGURE A-1

TOP SECRET

CONTROL NO.

MISSION • 1026-1 • INSTR • FRWD • 12/28/65 PLOT OF 0 MAX • TERRAIN • PROCESSING • INTERMEDIATE
ARITH MEAN • 1.31 • MEDIAN • 1.28 • STD DEV • 0.43 • RANGE • 0.43 TO 2.08 WITH 59 SAMPLES

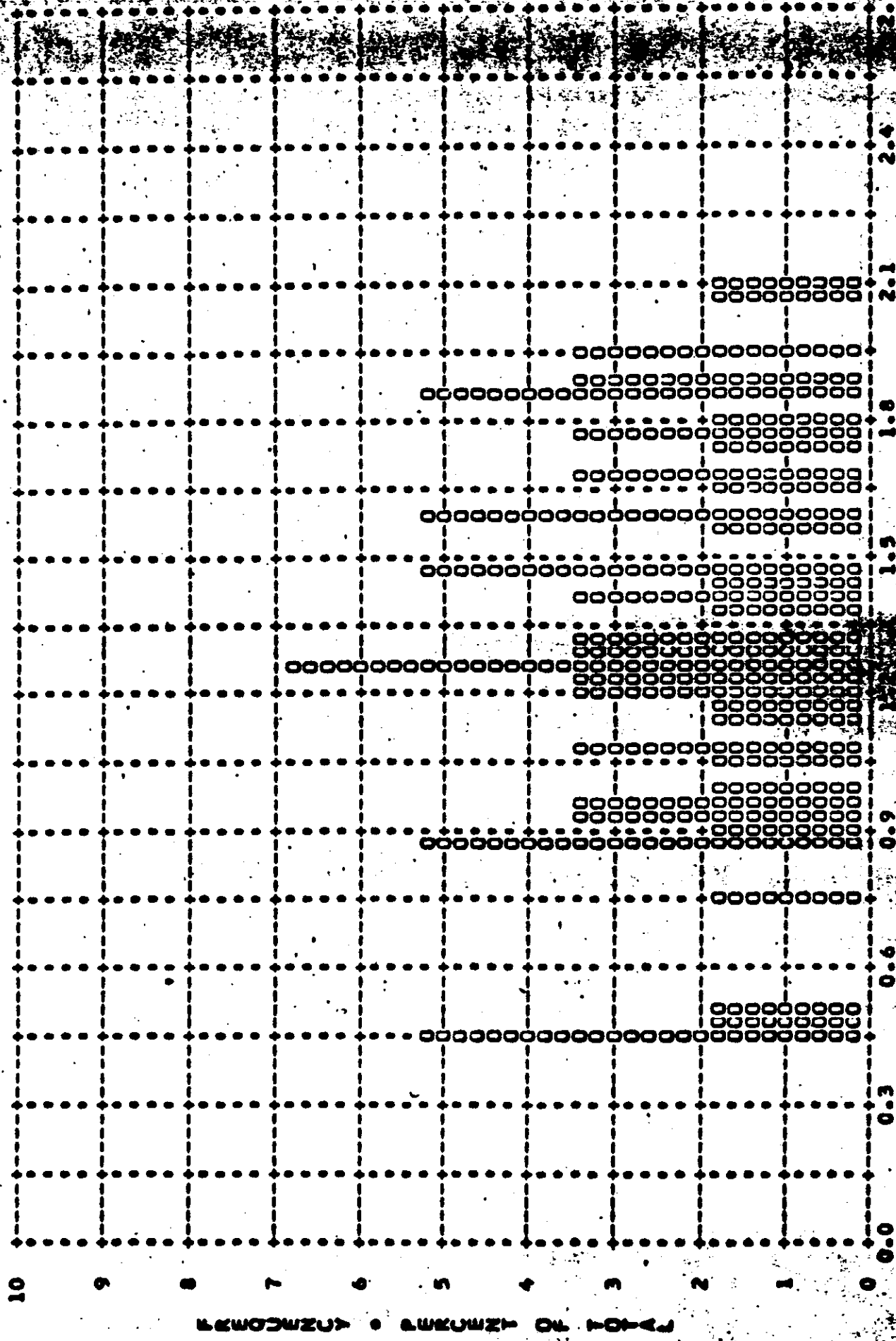
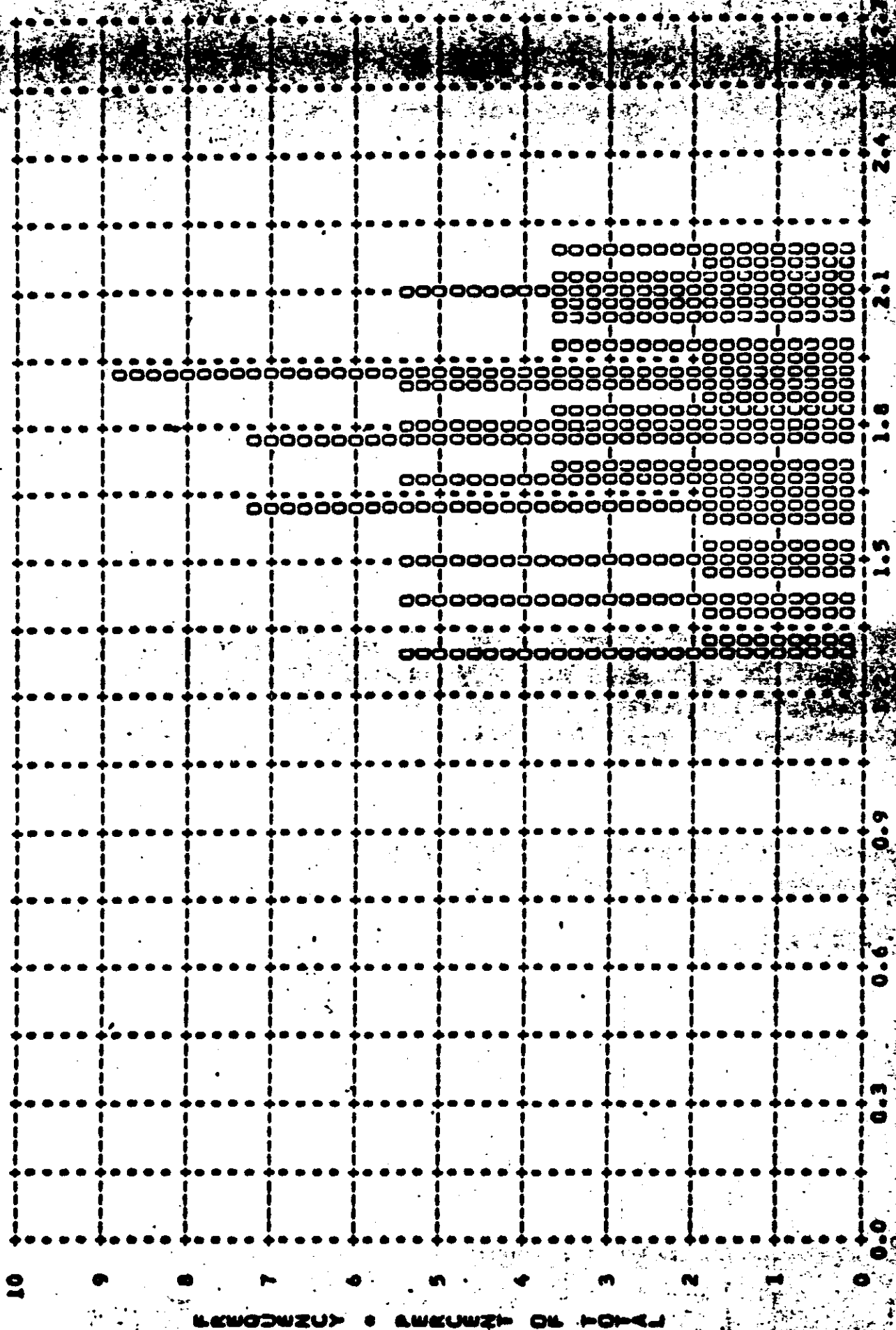


FIGURE A-2

~~TOP SECRET~~

CONTROL NO.

MISSION • 1026-1 • INSTR • FRWD • 12/28/65 PLOT OF D MAX • CLOUD • PROCESSING • INTERMEDIATE
ARITH MEAN • 1.76 • MEDIAN • 1.78 • STD DEV • 0.26 • RANGE • 1.27 TO 2.18 WITH 57 SAMPLES



TOP SECRET

CO. ROL NO.

MISSION • 1026-1 • INSTR • FRWD • 12/28/65 PLOT OF D MIN • TERRAIN • PROCESSING • FULL
ARITH MEAN • 0.37 • MEDIAN • 0.33 • STD DEV • 0.14 • RANGE • 0.22 TO 1.26 WITH 184 SAMPLES

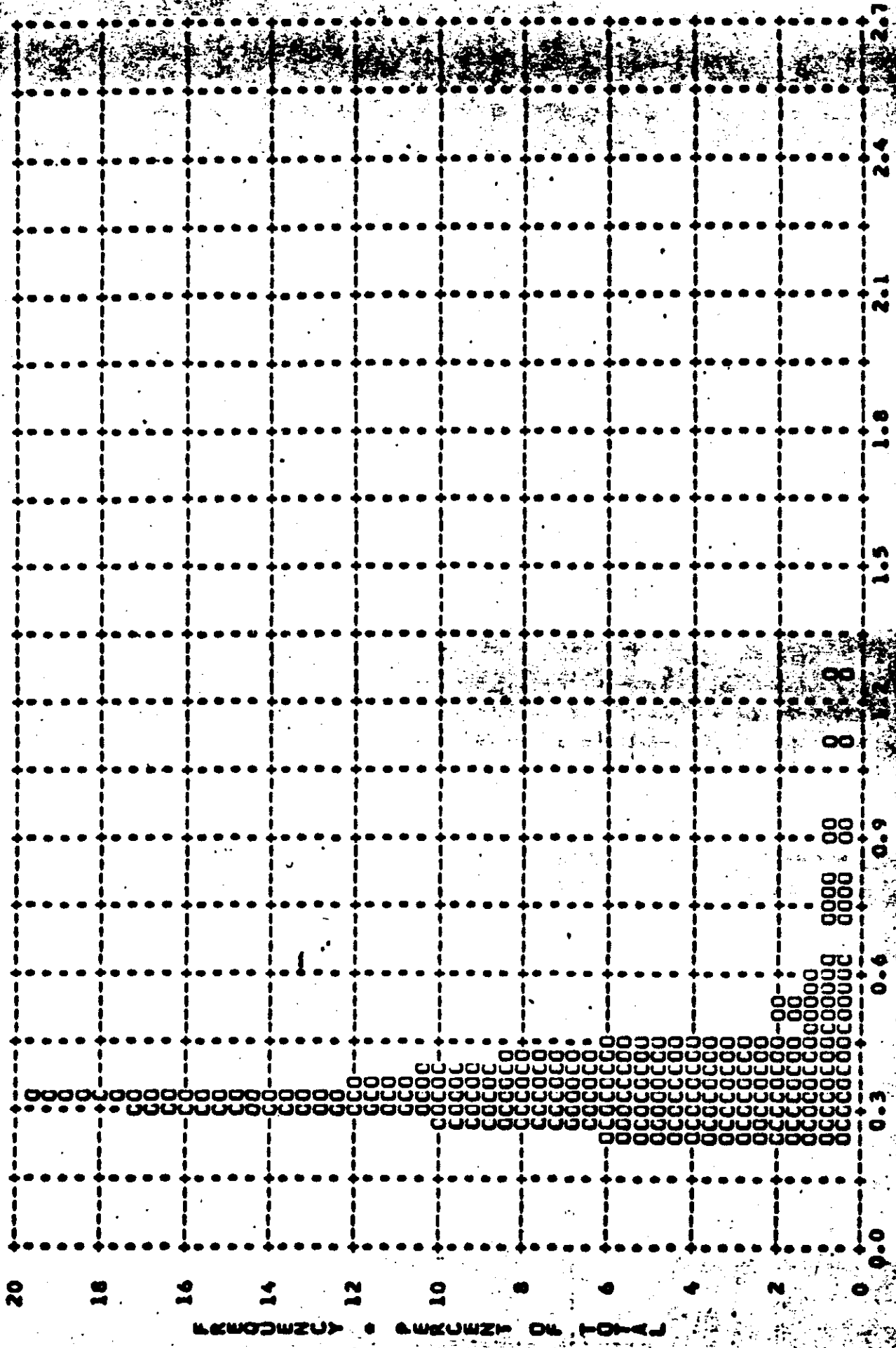


FIGURE A-4

SECURITY

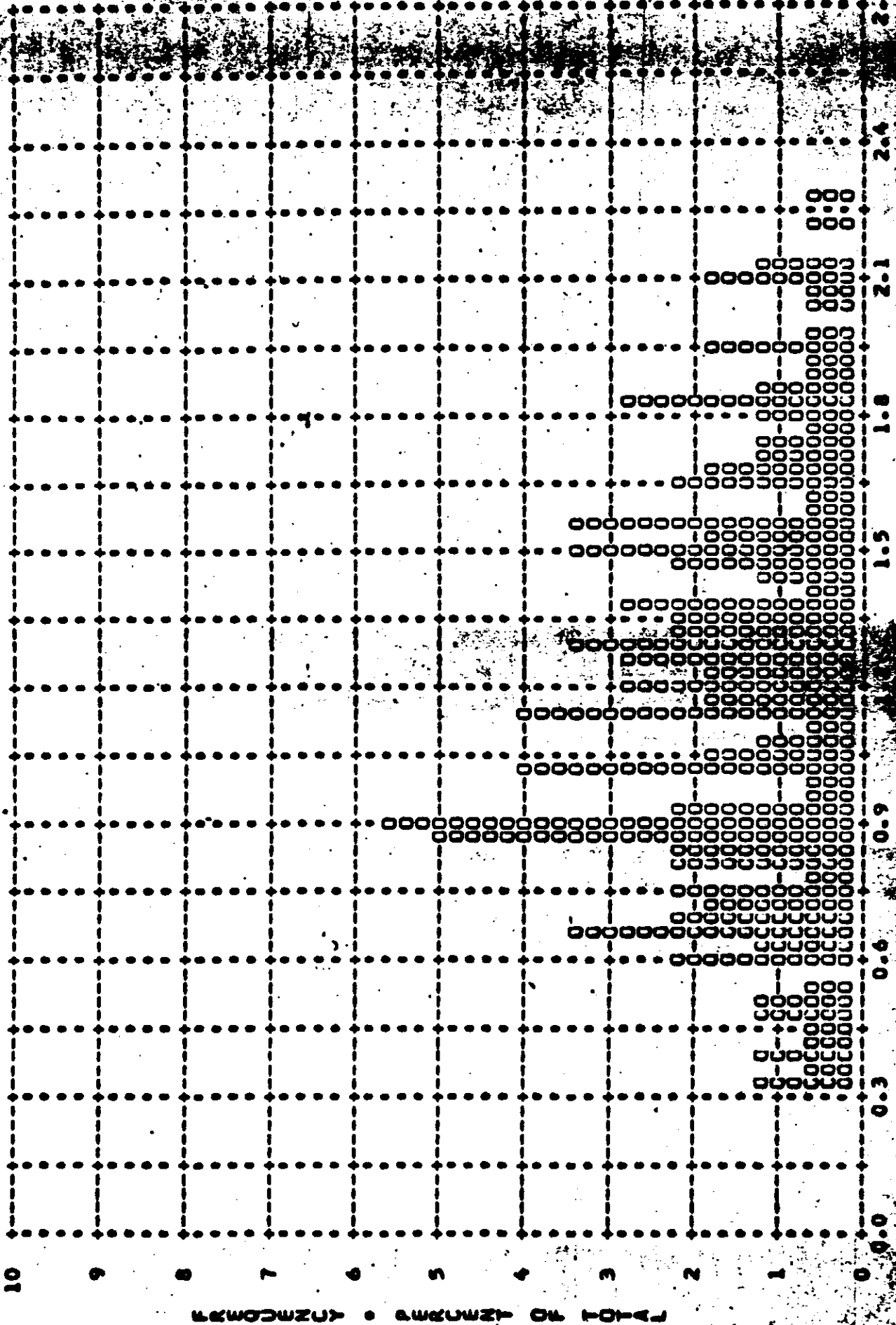
CONFIDENTIAL

TOP SECRET

TOP SECRET

CONTROL NO.

MISSION • 1026-1 • INSTR • FRWD • 12/28/65 PLOT OF D MAX • TERRAIN • PROCESSING • FULL
ARITH MEAN • 1.19 • MECIAN • 1.18 • STD DEV • 0.46 • RANGE • 0.31 TO 2.27 WITH 184 SAMPLES



FREQUENCY • PERCENT OF TOTAL

FIGURE A-5

TOP SECRET

CONTROL NO.

TOP SECRET

PROL NO.

MISSION • 1026-1 • INSTR • FRWD • 12/28/65 PLOT OF D MAX • CLOUD • PROCESSING • FULL
ARITH MEAN • 1.77 • MEDIAN • 1.90 • STD DEV • 0.38 • RANGE • 0.40 TO 2.28 WITH 171 SAMPLES

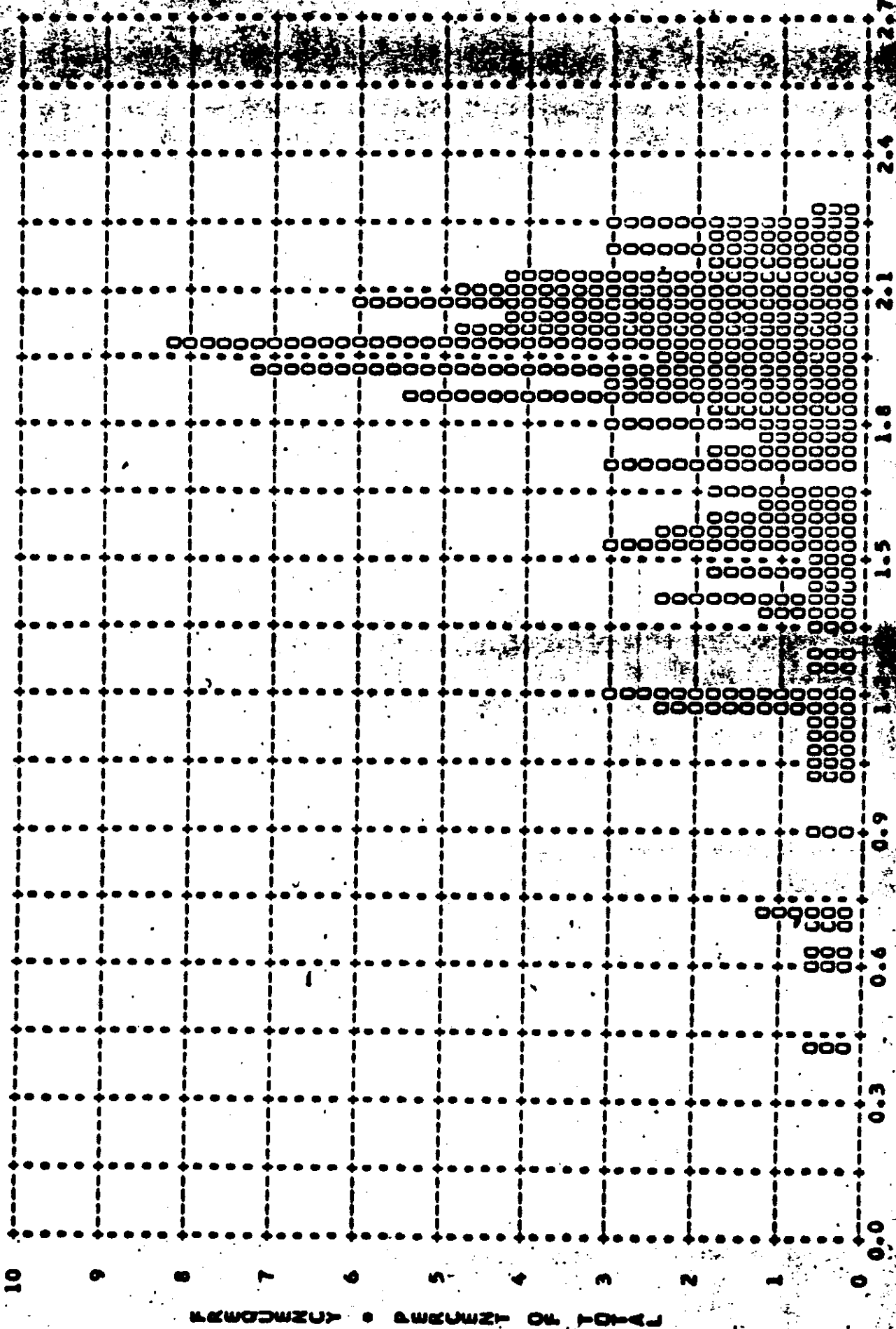


FIGURE A-6

DENSITY •

CONSTANT NO.

TOP SECRET

TOP SECRET

CL. NO. 100

MISSION • 1026-1 • INSTR • FRWD • 12/28/65 PLOT OF D MIN • TERRAIN • PROCESSING • ALL LEVELS
ARITH MEAN • 0.38 • MEDIAN • 0.33 • STD DEV • 0.15 • RANGE • 0.20 TO 1.26 WITH 243 SAMPLES

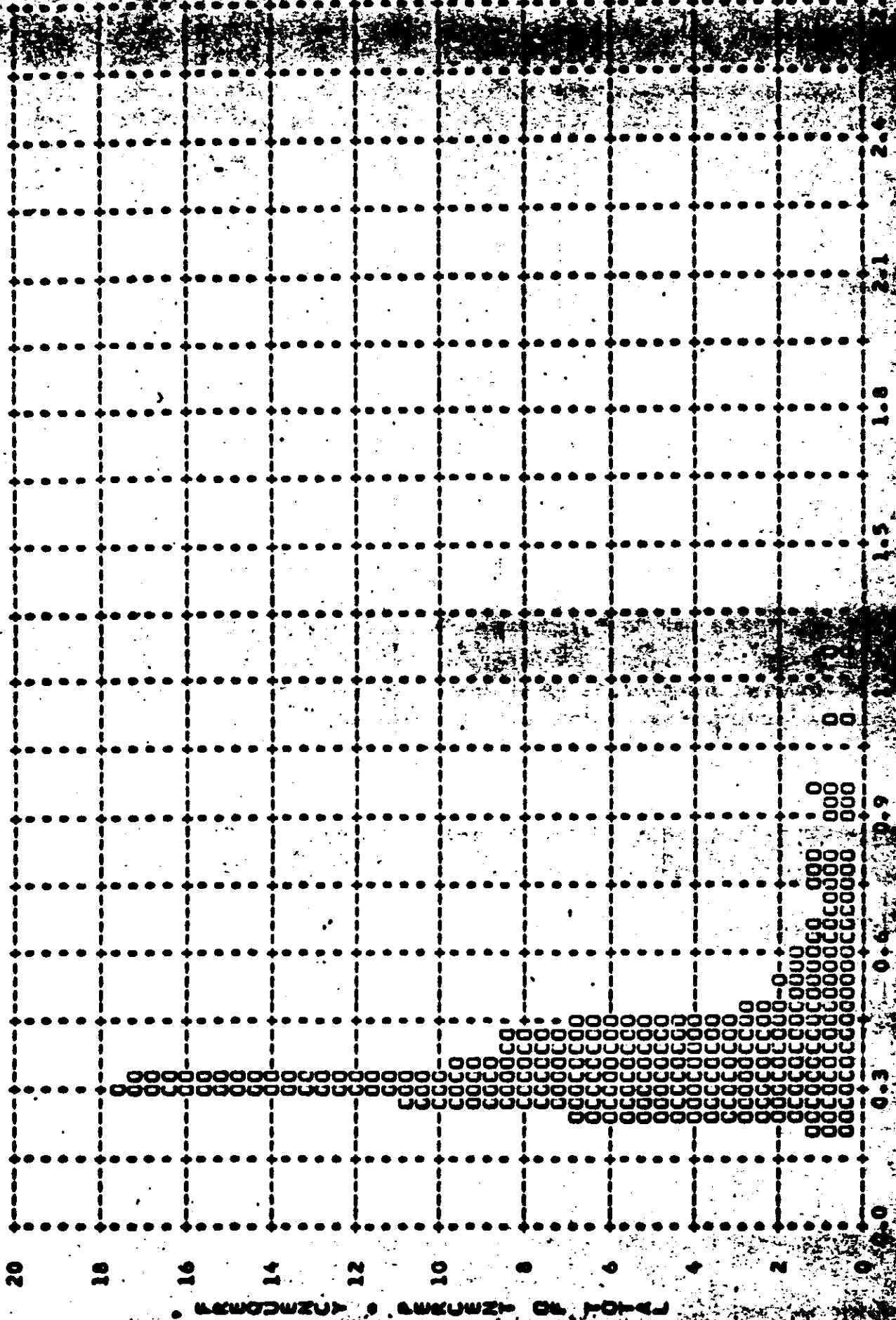
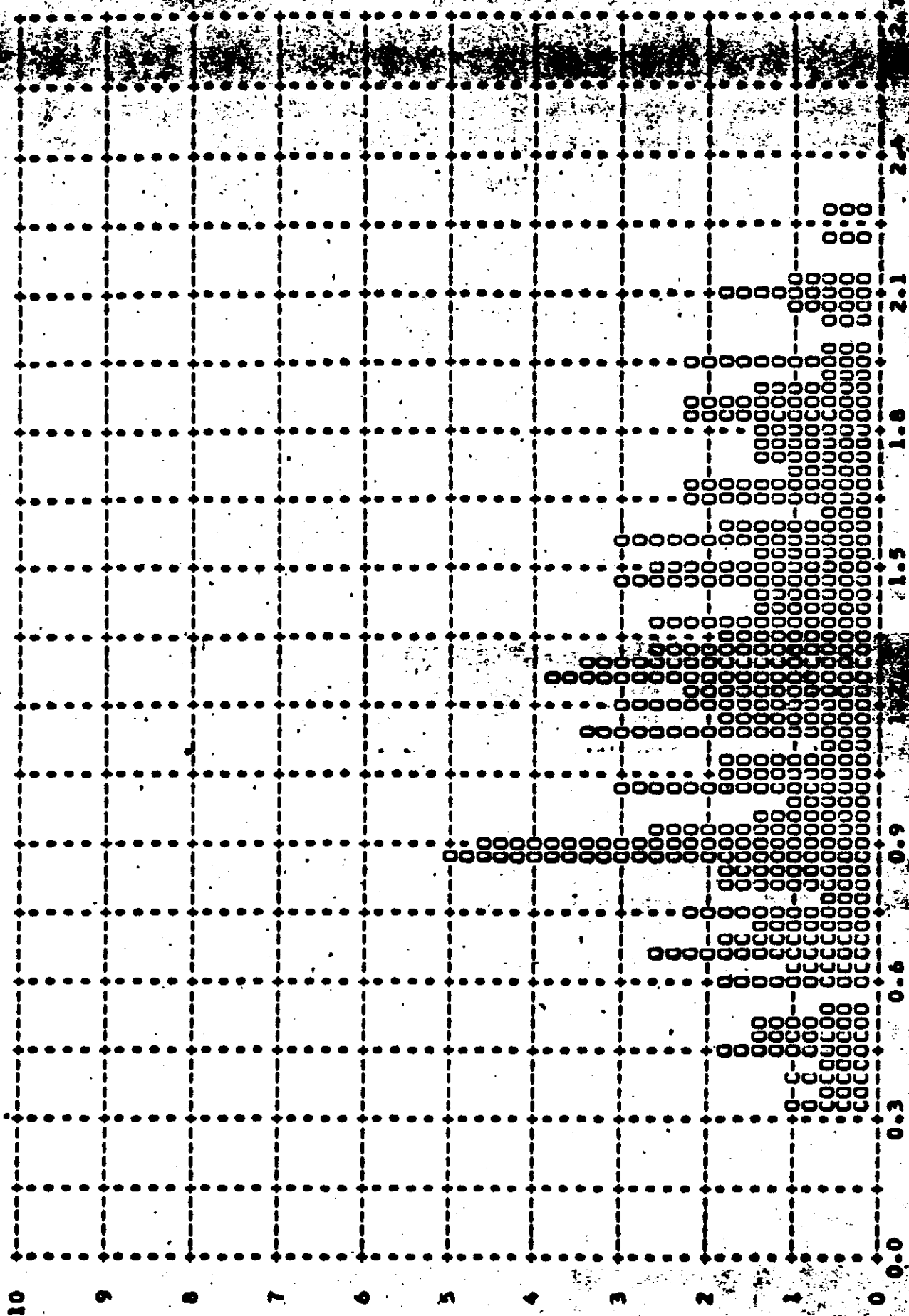


FIGURE A-7

TOP SECRET

CONTROL NO.

MISSION • 1026-1 • INSTR • FRWD • 12/28/65 PLOT OF D MAX • TERRAIN • PROCESSING • ALL LEVELS
ARITH MEAN • 1.22 • MEDIAN • 1.22 • STD DEV • 0.45 • RANGE • 0.31 TO 2.27 WITH 243 SAMPLES



PL-10 FORM 10-65

FIGURE A-8

SECURITY

TOP SECRET

CONTROL NO.

~~TOP SECRET~~

██████████ - CONTROL NO. ██████████

MISSION • 1026-1 • INSTR • FRWD • 12/28/65 PLOT OF D MAX • CLOUD • PROCESSING • ALL LEVELS
ARITH MEAN • 1.77 • MEDIAN • 1.87 • STD DEV • 0.36 • RANGE • 0.40 TO 2.28 WITH 228 SAMPLES

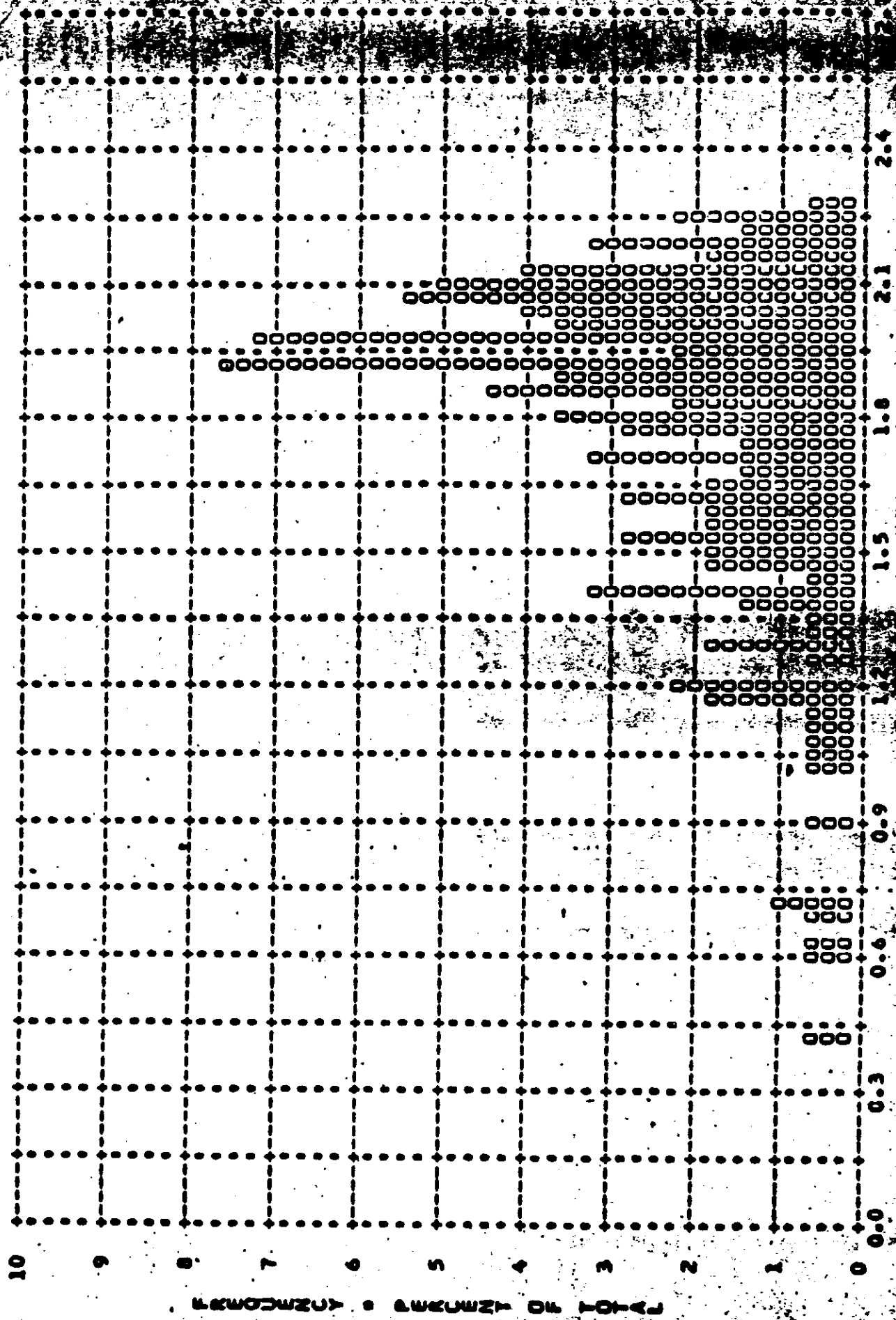


FIGURE A-9

██████████ - CONTROL NO. ██████████

~~TOP SECRET~~

DENSITY VALUE	PRIMARY			INTERMEDIATE			ALL LEVELS		
	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN
00	0	0	0	0	0	0	0	0	0
01	0	0	0	0	0	0	0	0	0
02	0	0	0	0	0	0	0	0	0
03	0	0	0	0	0	0	0	0	0
04	0	0	0	0	0	0	0	0	0
05	0	0	0	0	0	0	0	0	0
06	0	0	0	0	0	0	0	0	0
07	0	0	0	0	0	0	0	0	0
08	0	0	0	0	0	0	0	0	0
09	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0
45	0	0	0	0	0	0	0	0	0
46	0	0	0	0	0	0	0	0	0
47	0	0	0	0	0	0	0	0	0
48	0	0	0	0	0	0	0	0	0
49	0	0	0	0	0	0	0	0	0
50	0	0	0	0	0	0	0	0	0
51	0	0	0	0	0	0	0	0	0
52	0	0	0	0	0	0	0	0	0
53	0	0	0	0	0	0	0	0	0
54	0	0	0	0	0	0	0	0	0
55	0	0	0	0	0	0	0	0	0
56	0	0	0	0	0	0	0	0	0
57	0	0	0	0	0	0	0	0	0
58	0	0	0	0	0	0	0	0	0
59	0	0	0	0	0	0	0	0	0
60	0	0	0	0	0	0	0	0	0
61	0	0	0	0	0	0	0	0	0
62	0	0	0	0	0	0	0	0	0
63	0	0	0	0	0	0	0	0	0
64	0	0	0	0	0	0	0	0	0
65	0	0	0	0	0	0	0	0	0
66	0	0	0	0	0	0	0	0	0
67	0	0	0	0	0	0	0	0	0
68	0	0	0	0	0	0	0	0	0
69	0	0	0	0	0	0	0	0	0
70	0	0	0	0	0	0	0	0	0
71	0	0	0	0	0	0	0	0	0
72	0	0	0	0	0	0	0	0	0
73	0	0	0	0	0	0	0	0	0
74	0	0	0	0	0	0	0	0	0
75	0	0	0	0	0	0	0	0	0
76	0	0	0	0	0	0	0	0	0
77	0	0	0	0	0	0	0	0	0
78	0	0	0	0	0	0	0	0	0
79	0	0	0	0	0	0	0	0	0
80	0	0	0	0	0	0	0	0	0
81	0	0	0	0	0	0	0	0	0
82	0	0	0	0	0	0	0	0	0
83	0	0	0	0	0	0	0	0	0
84	0	0	0	0	0	0	0	0	0
85	0	0	0	0	0	0	0	0	0
86	0	0	0	0	0	0	0	0	0
87	0	0	0	0	0	0	0	0	0
88	0	0	0	0	0	0	0	0	0
89	0	0	0	0	0	0	0	0	0
90	0	0	0	0	0	0	0	0	0
91	0	0	0	0	0	0	0	0	0
92	0	0	0	0	0	0	0	0	0
93	0	0	0	0	0	0	0	0	0
94	0	0	0	0	0	0	0	0	0
95	0	0	0	0	0	0	0	0	0
96	0	0	0	0	0	0	0	0	0
97	0	0	0	0	0	0	0	0	0
98	0	0	0	0	0	0	0	0	0
99	0	0	0	0	0	0	0	0	0
100	0	0	0	0	0	0	0	0	0
SUBTOTAL									

TOP SECRET

CONTROL NO.

TABLE A-2

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN
.51	0	0	0	0	0	0	0	0	0	0	0	0
.52	0	0	0	0	0	0	0	0	0	0	0	0
.53	0	0	0	0	0	0	0	0	0	0	0	0
.54	0	0	0	0	0	0	0	0	0	0	0	0
.55	0	0	0	0	0	0	0	0	0	0	0	0
.56	0	0	0	0	0	0	0	0	0	0	0	0
.57	0	0	0	0	0	0	0	0	0	0	0	0
.58	0	0	0	0	0	0	0	0	0	0	0	0
.59	0	0	0	0	0	0	0	0	0	0	0	0
.60	0	0	0	0	0	0	0	0	0	0	0	0
.61	0	0	0	0	0	0	0	0	0	0	0	0
.62	0	0	0	0	0	0	0	0	0	0	0	0
.63	0	0	0	0	0	0	0	0	0	0	0	0
.64	0	0	0	0	0	0	0	0	0	0	0	0
.65	0	0	0	0	0	0	0	0	0	0	0	0
.66	0	0	0	0	0	0	0	0	0	0	0	0
.67	0	0	0	0	0	0	0	0	0	0	0	0
.68	0	0	0	0	0	0	0	0	0	0	0	0
.69	0	0	0	0	0	0	0	0	0	0	0	0
.70	0	0	0	0	0	0	0	0	0	0	0	0
.71	0	0	0	0	0	0	0	0	0	0	0	0
.72	0	0	0	0	0	0	0	0	0	0	0	0
.73	0	0	0	0	0	0	0	0	0	0	0	0
.74	0	0	0	0	0	0	0	0	0	0	0	0
.75	0	0	0	0	0	0	0	0	0	0	0	0
.76	0	0	0	0	0	0	0	0	0	0	0	0
.77	0	0	0	0	0	0	0	0	0	0	0	0
.78	0	0	0	0	0	0	0	0	0	0	0	0
.79	0	0	0	0	0	0	0	0	0	0	0	0
.80	0	0	0	0	0	0	0	0	0	0	0	0
.81	0	0	0	0	0	0	0	0	0	0	0	0
.82	0	0	0	0	0	0	0	0	0	0	0	0
.83	0	0	0	0	0	0	0	0	0	0	0	0
.84	0	0	0	0	0	0	0	0	0	0	0	0
.85	0	0	0	0	0	0	0	0	0	0	0	0
.86	0	0	0	0	0	0	0	0	0	0	0	0
.87	0	0	0	0	0	0	0	0	0	0	0	0
.88	0	0	0	0	0	0	0	0	0	0	0	0
.89	0	0	0	0	0	0	0	0	0	0	0	0
.90	0	0	0	0	0	0	0	0	0	0	0	0
.91	0	0	0	0	0	0	0	0	0	0	0	0
.92	0	0	0	0	0	0	0	0	0	0	0	0
.93	0	0	0	0	0	0	0	0	0	0	0	0
.94	0	0	0	0	0	0	0	0	0	0	0	0
.95	0	0	0	0	0	0	0	0	0	0	0	0
.96	0	0	0	0	0	0	0	0	0	0	0	0
.97	0	0	0	0	0	0	0	0	0	0	0	0
.98	0	0	0	0	0	0	0	0	0	0	0	0
.99	0	0	0	0	0	0	0	0	0	0	0	0
.00	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	10	27	5	3	29	7	4	5	1

TOP SECRET

CONTROL NO. [REDACTED]

TABLE A-2

DENSITY VALUE	PRIMARY			INTERMEDIATE			ADULT			ALL LEVELS		
	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN
01	0	0	0	0	0	0	0	0	0	0	0	0
02	0	0	0	0	0	0	0	0	0	0	0	0
03	0	0	0	0	0	0	0	0	0	0	0	0
04	0	0	0	0	0	0	0	0	0	0	0	0
05	0	0	0	0	0	0	0	0	0	0	0	0
06	0	0	0	0	0	0	0	0	0	0	0	0
07	0	0	0	0	0	0	0	0	0	0	0	0
08	0	0	0	0	0	0	0	0	0	0	0	0
09	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0
45	0	0	0	0	0	0	0	0	0	0	0	0
46	0	0	0	0	0	0	0	0	0	0	0	0
47	0	0	0	0	0	0	0	0	0	0	0	0
48	0	0	0	0	0	0	0	0	0	0	0	0
49	0	0	0	0	0	0	0	0	0	0	0	0
50	0	0	0	0	0	0	0	0	0	0	0	0
SUB TOTAL	0	0	0	0	0	0	0	0	0	0	0	0

~~TOP SECRET~~

CONTROL NO. [REDACTED]

TABLE A-2

TOP SECRET

CONTROL NO.

MISSION # 1026-1 • INSTRUMENT # AFI 12/28/63 DENSITY FREQ DLSTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN
51	0	0	0	0	0	0	0	0	0	0	0	0
52	0	0	0	0	0	0	0	0	0	0	0	0
53	0	0	0	0	0	0	0	0	0	0	0	0
54	0	0	0	0	0	0	0	0	0	0	0	0
55	0	0	0	0	0	0	0	0	0	0	0	0
56	0	0	0	0	0	0	0	0	0	0	0	0
57	0	0	0	0	0	0	0	0	0	0	0	0
58	0	0	0	0	0	0	0	0	0	0	0	0
59	0	0	0	0	0	0	0	0	0	0	0	0
60	0	0	0	0	0	0	0	0	0	0	0	0
61	0	0	0	0	0	0	0	0	0	0	0	0
62	0	0	0	0	0	0	0	0	0	0	0	0
63	0	0	0	0	0	0	0	0	0	0	0	0
64	0	0	0	0	0	0	0	0	0	0	0	0
65	0	0	0	0	0	0	0	0	0	0	0	0
66	0	0	0	0	0	0	0	0	0	0	0	0
67	0	0	0	0	0	0	0	0	0	0	0	0
68	0	0	0	0	0	0	0	0	0	0	0	0
69	0	0	0	0	0	0	0	0	0	0	0	0
70	0	0	0	0	0	0	0	0	0	0	0	0
71	0	0	0	0	0	0	0	0	0	0	0	0
72	0	0	0	0	0	0	0	0	0	0	0	0
73	0	0	0	0	0	0	0	0	0	0	0	0
74	0	0	0	0	0	0	0	0	0	0	0	0
75	0	0	0	0	0	0	0	0	0	0	0	0
76	0	0	0	0	0	0	0	0	0	0	0	0
77	0	0	0	0	0	0	0	0	0	0	0	0
78	0	0	0	0	0	0	0	0	0	0	0	0
79	0	0	0	0	0	0	0	0	0	0	0	0
80	0	0	0	0	0	0	0	0	0	0	0	0
81	0	0	0	0	0	0	0	0	0	0	0	0
82	0	0	0	0	0	0	0	0	0	0	0	0
83	0	0	0	0	0	0	0	0	0	0	0	0
84	0	0	0	0	0	0	0	0	0	0	0	0
85	0	0	0	0	0	0	0	0	0	0	0	0
86	0	0	0	0	0	0	0	0	0	0	0	0
87	0	0	0	0	0	0	0	0	0	0	0	0
88	0	0	0	0	0	0	0	0	0	0	0	0
89	0	0	0	0	0	0	0	0	0	0	0	0
90	0	0	0	0	0	0	0	0	0	0	0	0
91	0	0	0	0	0	0	0	0	0	0	0	0
92	0	0	0	0	0	0	0	0	0	0	0	0
93	0	0	0	0	0	0	0	0	0	0	0	0
94	0	0	0	0	0	0	0	0	0	0	0	0
95	0	0	0	0	0	0	0	0	0	0	0	0
96	0	0	0	0	0	0	0	0	0	0	0	0
97	0	0	0	0	0	0	0	0	0	0	0	0
98	0	0	0	0	0	0	0	0	0	0	0	0
99	0	0	0	0	0	0	0	0	0	0	0	0
00	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	0	0	0	0	0	0	0	0

TOP SECRET



CONTROL NO.



TABLE A-2

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS					
	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN			
01	00	00	00	00	00	00	00	00	00	00	00	00			
02	00	00	00	00	00	00	00	00	00	00	00	00			
03	00	00	00	00	00	00	00	00	00	00	00	00			
04	00	00	00	00	00	00	00	00	00	00	00	00			
05	00	00	00	00	00	00	00	00	00	00	00	00			
06	00	00	00	00	00	00	00	00	00	00	00	00			
07	00	00	00	00	00	00	00	00	00	00	00	00			
08	00	00	00	00	00	00	00	00	00	00	00	00			
09	00	00	00	00	00	00	00	00	00	00	00	00			
10	00	00	00	00	00	00	00	00	00	00	00	00			
11	00	00	00	00	00	00	00	00	00	00	00	00			
12	00	00	00	00	00	00	00	00	00	00	00	00			
13	00	00	00	00	00	00	00	00	00	00	00	00			
14	00	00	00	00	00	00	00	00	00	00	00	00			
15	00	00	00	00	00	00	00	00	00	00	00	00			
16	00	00	00	00	00	00	00	00	00	00	00	00			
17	00	00	00	00	00	00	00	00	00	00	00	00			
18	00	00	00	00	00	00	00	00	00	00	00	00			
19	00	00	00	00	00	00	00	00	00	00	00	00			
20	00	00	00	00	00	00	00	00	00	00	00	00			
21	00	00	00	00	00	00	00	00	00	00	00	00			
22	00	00	00	00	00	00	00	00	00	00	00	00			
23	00	00	00	00	00	00	00	00	00	00	00	00			
24	00	00	00	00	00	00	00	00	00	00	00	00			
25	00	00	00	00	00	00	00	00	00	00	00	00			
26	00	00	00	00	00	00	00	00	00	00	00	00			
27	00	00	00	00	00	00	00	00	00	00	00	00			
28	00	00	00	00	00	00	00	00	00	00	00	00			
29	00	00	00	00	00	00	00	00	00	00	00	00			
30	00	00	00	00	00	00	00	00	00	00	00	00			
31	00	00	00	00	00	00	00	00	00	00	00	00			
32	00	00	00	00	00	00	00	00	00	00	00	00			
33	00	00	00	00	00	00	00	00	00	00	00	00			
34	00	00	00	00	00	00	00	00	00	00	00	00			
35	00	00	00	00	00	00	00	00	00	00	00	00			
36	00	00	00	00	00	00	00	00	00	00	00	00			
37	00	00	00	00	00	00	00	00	00	00	00	00			
38	00	00	00	00	00	00	00	00	00	00	00	00			
39	00	00	00	00	00	00	00	00	00	00	00	00			
40	00	00	00	00	00	00	00	00	00	00	00	00			
41	00	00	00	00	00	00	00	00	00	00	00	00			
42	00	00	00	00	00	00	00	00	00	00	00	00			
43	00	00	00	00	00	00	00	00	00	00	00	00			
44	00	00	00	00	00	00	00	00	00	00	00	00			
45	00	00	00	00	00	00	00	00	00	00	00	00			
46	00	00	00	00	00	00	00	00	00	00	00	00			
47	00	00	00	00	00	00	00	00	00	00	00	00			
48	00	00	00	00	00	00	00	00	00	00	00	00			
49	00	00	00	00	00	00	00	00	00	00	00	00			
50	00	00	00	00	00	00	00	00	00	00	00	00			
SUBTOTAL	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00

TOP SECRET [REDACTED] - CONTROL NO. [REDACTED]

TABLE A-2

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN
.51	0	0	0	0	0	0	0	0	0	0	0	0
.52	0	0	0	0	0	0	0	0	0	0	0	0
.53	0	0	0	0	0	0	0	0	0	0	0	0
.54	0	0	0	0	0	0	0	0	0	0	0	0
.55	0	0	0	0	0	0	0	0	0	0	0	0
.56	0	0	0	0	0	0	0	0	0	0	0	0
.57	0	0	0	0	0	0	0	0	0	0	0	0
.58	0	0	0	0	0	0	0	0	0	0	0	0
.59	0	0	0	0	0	0	0	0	0	0	0	0
.60	0	0	0	0	0	0	0	0	0	0	0	0
.61	0	0	0	0	0	0	0	0	0	0	0	0
.62	0	0	0	0	0	0	0	0	0	0	0	0
.63	0	0	0	0	0	0	0	0	0	0	0	0
.64	0	0	0	0	0	0	0	0	0	0	0	0
.65	0	0	0	0	0	0	0	0	0	0	0	0
.66	0	0	0	0	0	0	0	0	0	0	0	0
.67	0	0	0	0	0	0	0	0	0	0	0	0
.68	0	0	0	0	0	0	0	0	0	0	0	0
.69	0	0	0	0	0	0	0	0	0	0	0	0
.70	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	0	0	0	0	0	0	0	0
TOTAL	0	0	0	90	90	95	150	150	130	240	240	225

MISSION 1026-1 INSTR - AFT 12/28/65 PROCESSING AND EXPOSURE ANALYSIS

PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0	0 PC	0 PC	0 PC	0 PC	0 PC
INTERMEDIATE	90	0 PC	71 PC	27 PC	2 PC	0 PC
FULL	150	63 PC	0 PC	57 PC	1 PC	0 PC
ALL LEVELS	240	39 PC	27 PC	33 PC	1 PC	0 PC

PROCESS LEVEL	BASE + FOG	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0.01-0.09	0.01-0.13	0.14-0.39	0.40-0.90	-----	0.91 AND U
INTERMED	0.10-0.17	0.01-0.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35 AND U
FULL	0.18 AND UP	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70 AND U

~~TOP SECRET~~

CONTROL NO. [REDACTED]

TABLE A-2

TOP SECRET

CONTROL NO.

MISSION • 1026-1 • INSTR • AFT • 12/28/65 PLOT OF 0 MIN • TERRAIN • PROCESSING • INTERMEDIATE
ARITH MEAN • 0.37 • MEDIAN • 0.33 • STD DEV • 0.16 • RANGE • 0.21 TO 1.11 WITH 90 SAMPLES

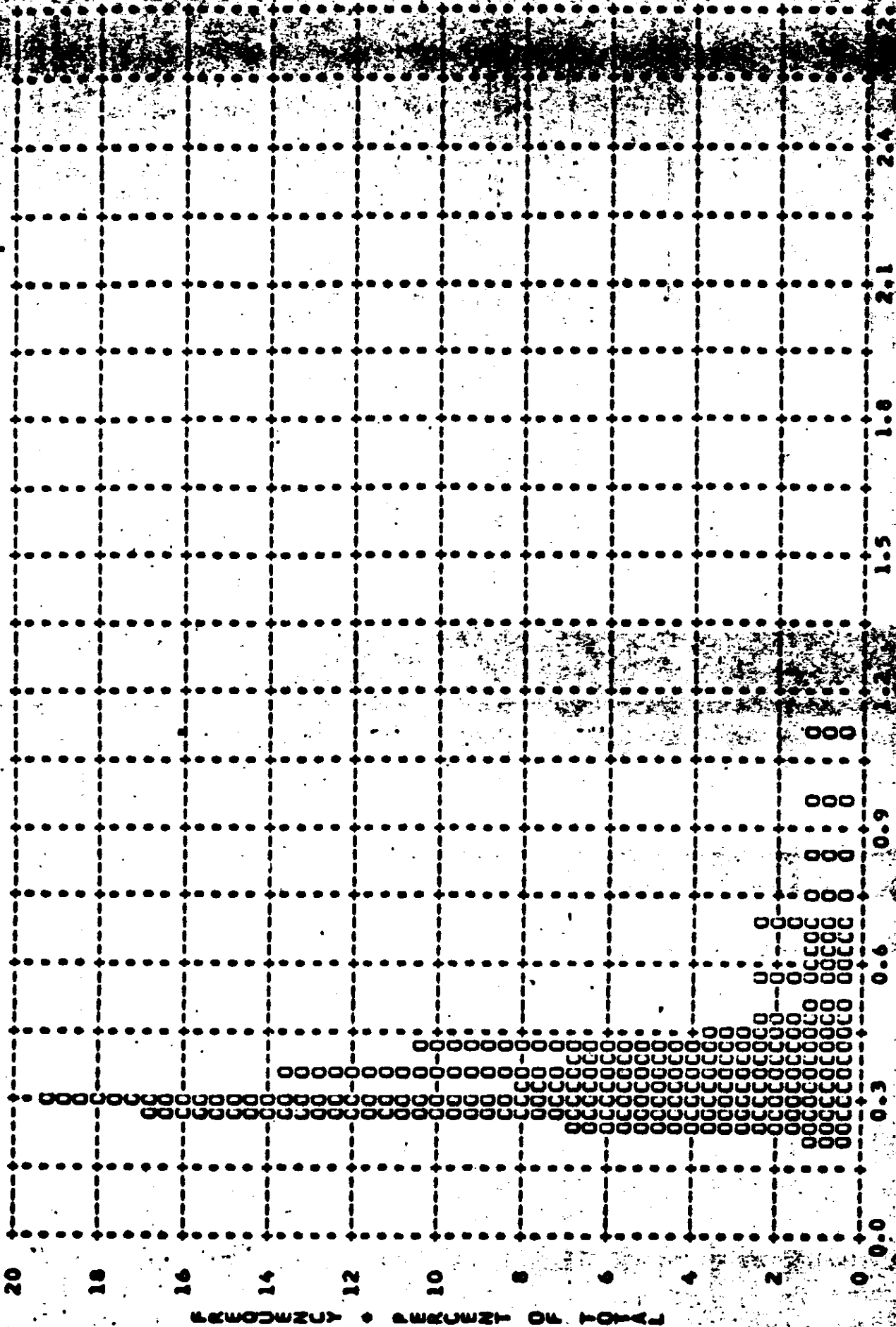


FIGURE A-10

DENSITY

TOP SECRET

CONTROL NO.

TOP SECRET

CONTROL NO.

MISSION • 1026-1 • INSTR • AFT • 12/28/65 PLOT OF D MAX • TERRAIN • PROCESSING • INTERMEDIATE
ARITH MEAN • 1.22 • MEDIAN • 1.27 • STD DEV • 0.48 • RANGE • 0.35 TO 2.31 WITH 90 SAMPLES

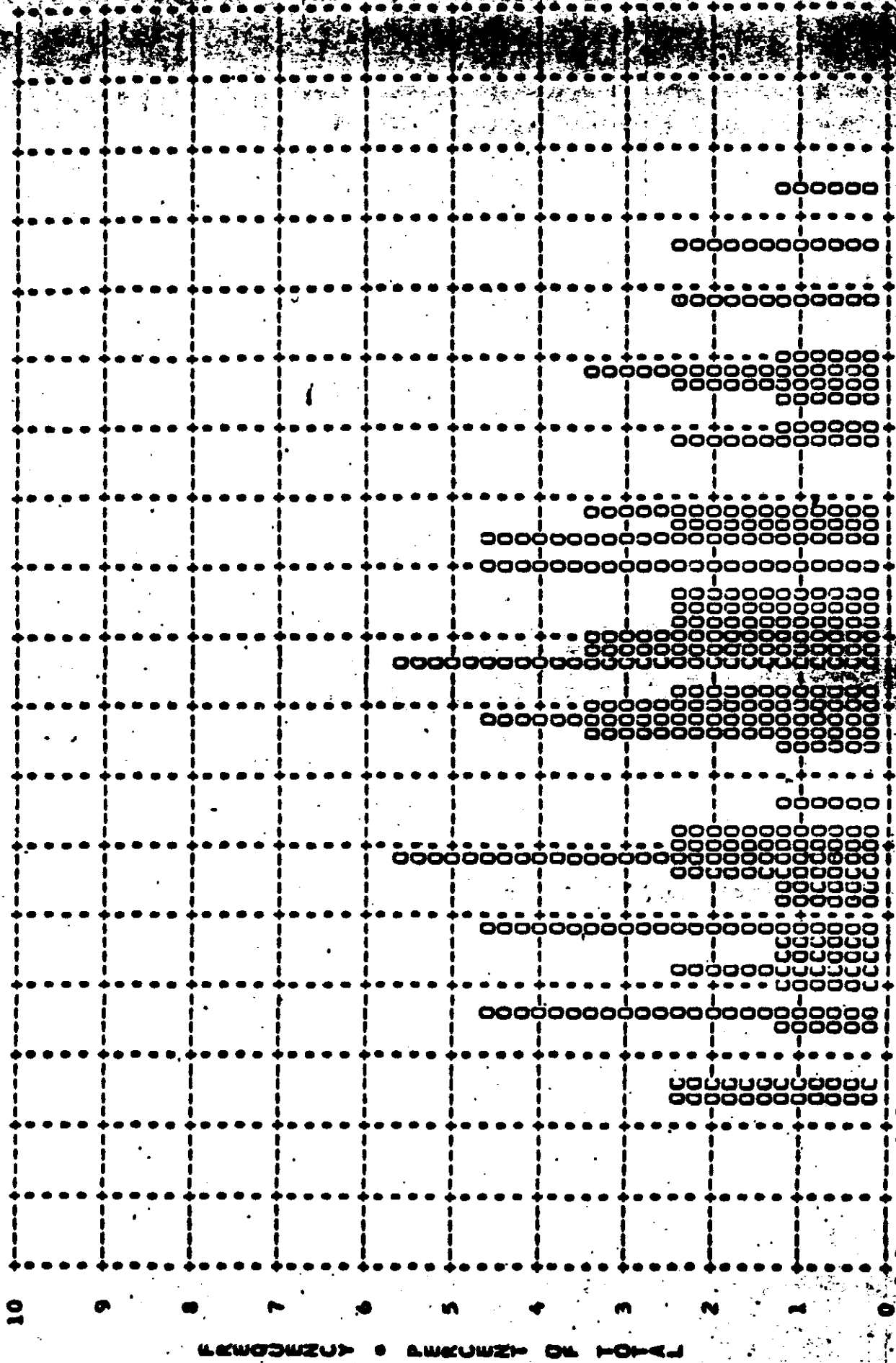


FIGURE A-11

TOP SECRET

CONTROL NO.

MISSION • 1026-1 • INSTR • AFT • 12/28/65 PLOT OF 0 MAX • CLOUD • PROCESSING • INTERMEDIATE
ARITH MEAN • 1.74 • MEDIAN • 1.82 • STD DEV • 0.37 • RANGE • 0.37 TO 2.32 WITH 95 SAMPLES

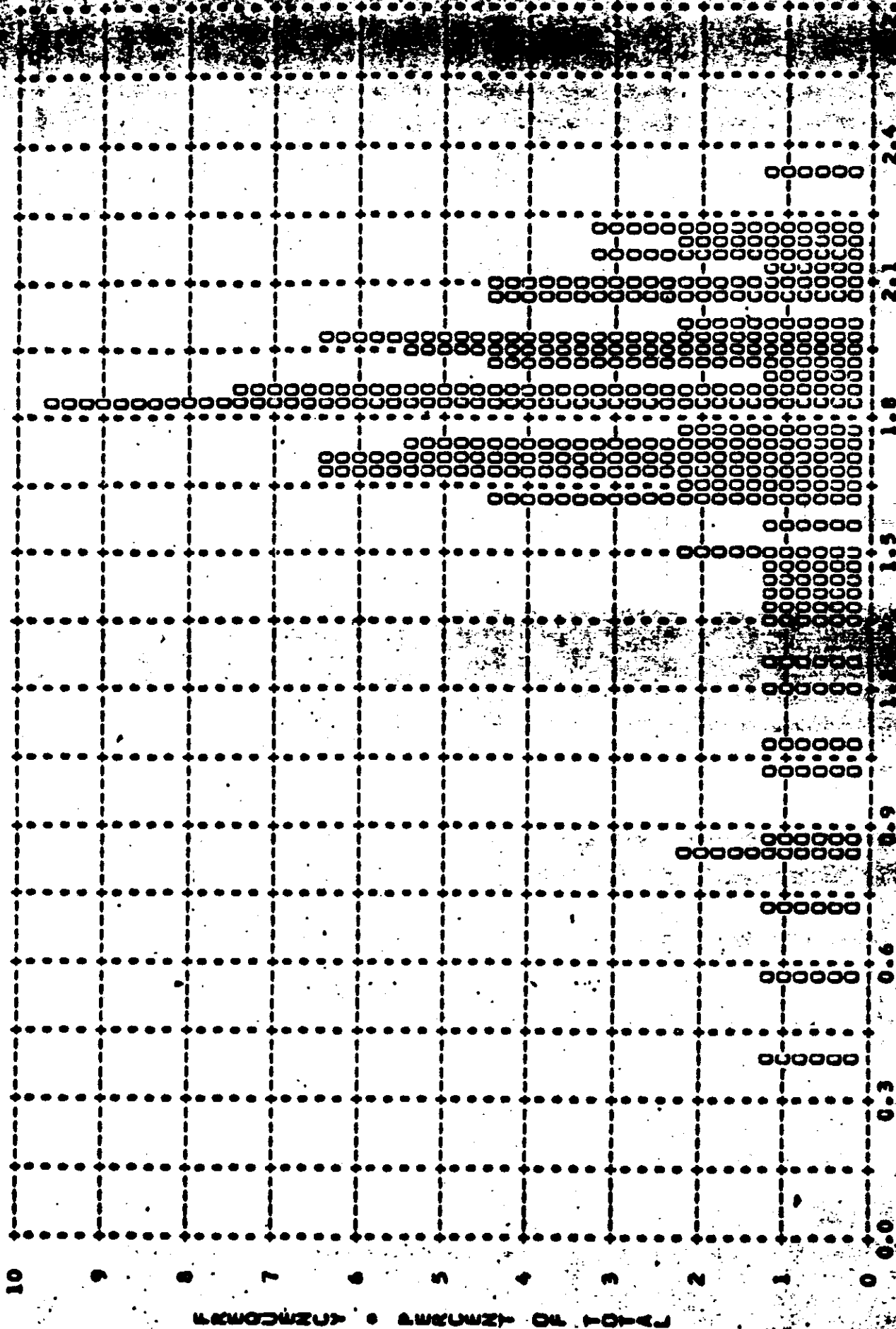


FIGURE A-12

TOP SECRET

TOP SECRET

CONTROL NO.

MISSION • 1026-1 • INSTR • AFT • 12/28/65 PLOT OF U MIN • TERRAIN • PROCESSING • FULL
ARITH MEAN • 0.41 • MEDIAN • 0.35 • STD DEV • 0.16 • RANGE • 0.20 TO 1.16 WITH 150 SAMPLES

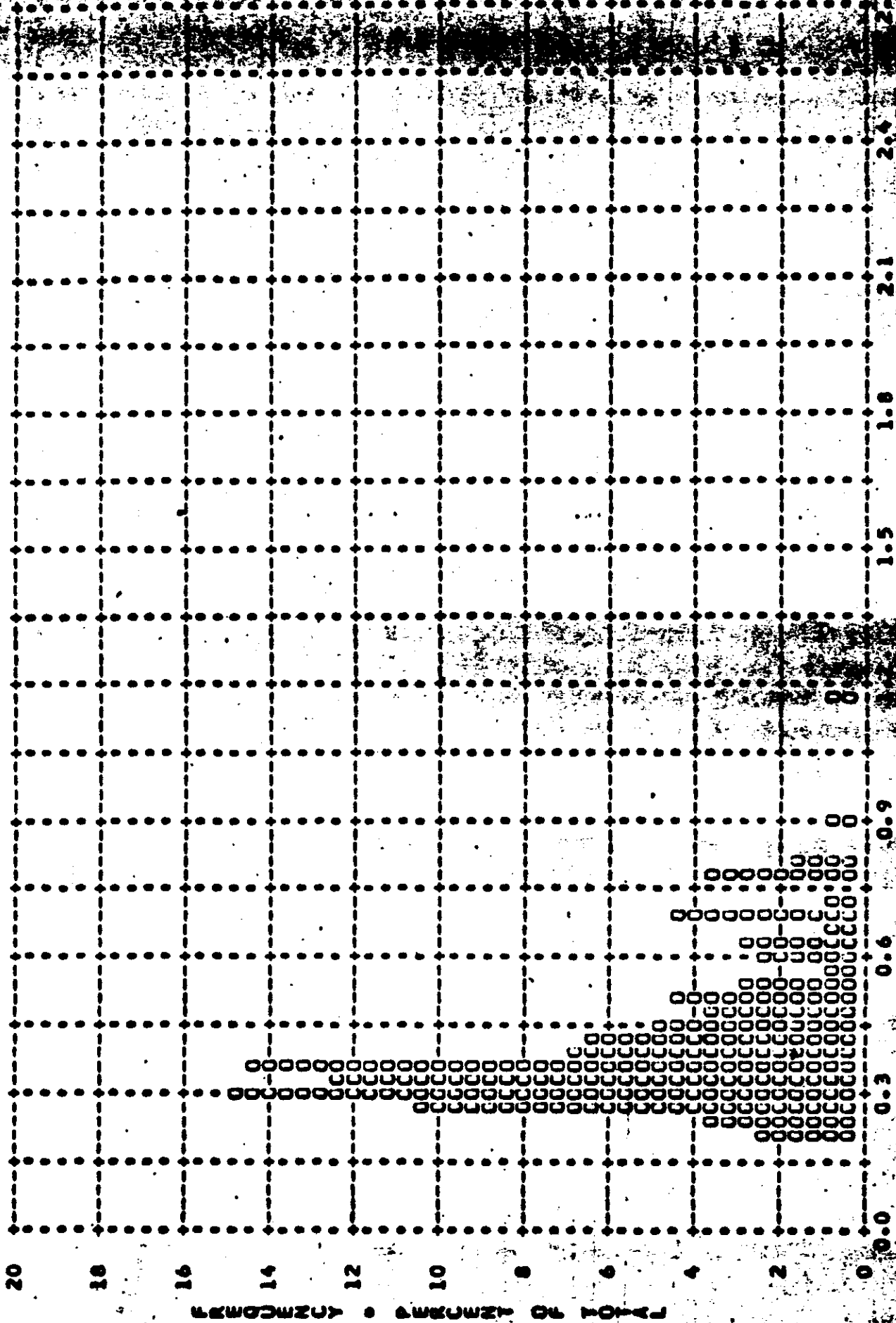


FIGURE A-13

DENSITY

CONTROL NO.

TOP SECRET

CONTROL NO.

MISSION • 1026-1 • INSTR • AFT • 12/28/65 PLOT OF D MAX • TERRAIN • PROCESSING • FULL
ARITH MEAN • 1.33 • MEDIAN • 1.35 • STD DEV • 0.47 • RANGE • 0.24 TO 2.36 WITH 150 SAMPLES

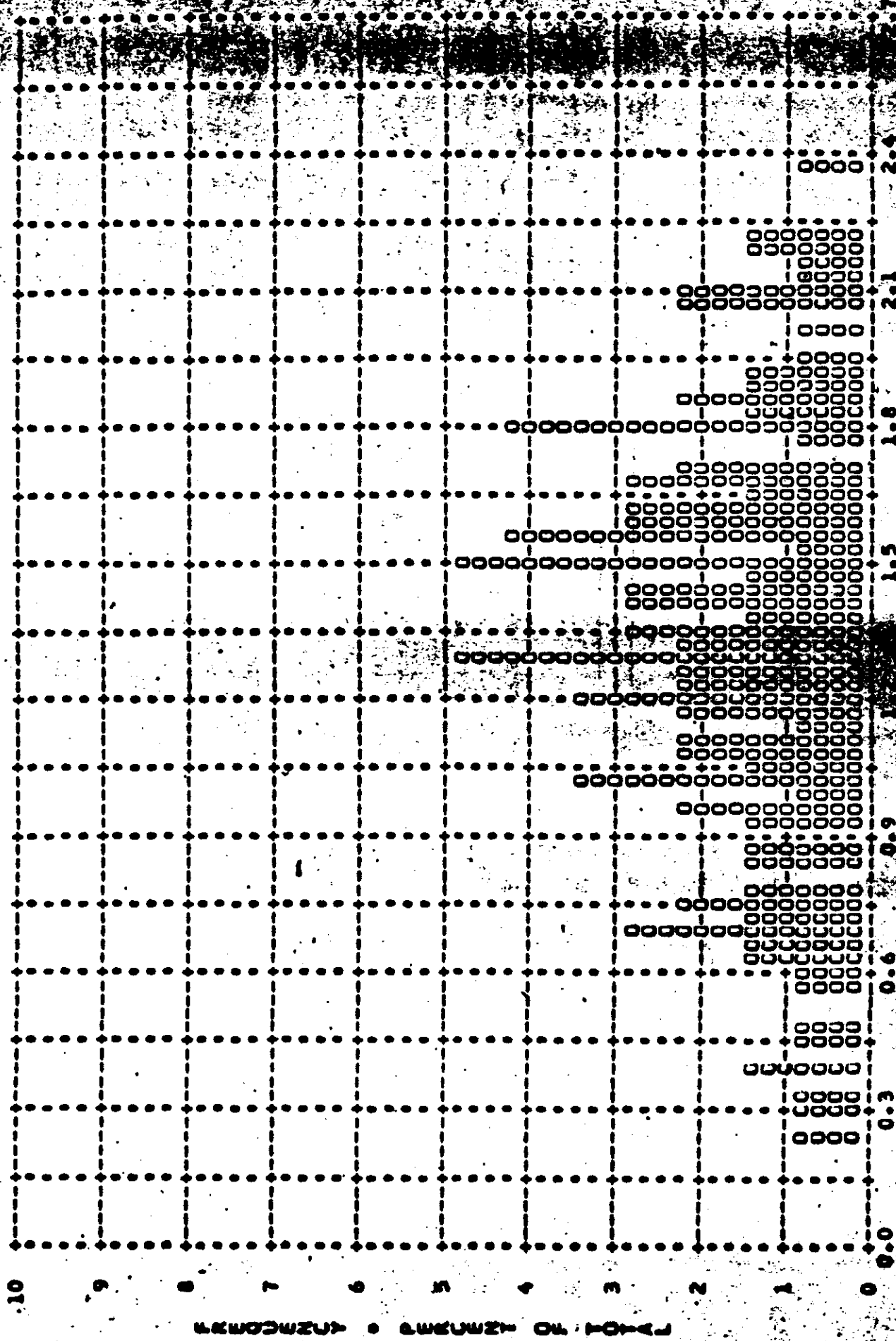


FIGURE A-14

~~TOP SECRET~~

CONTROL NO. [REDACTED]

MISSION • 1026-1 • INSTR • AFT • 12/28/65 PLOT OF D MAX • CLOUD • PROCESSING • FULL
ARITH MEAN • 1.81 • MEDIAN • 1.91 • STD DEV • 0.41 • RANGE • 0.64 TO 2.40 WITH 130 SAMPLES

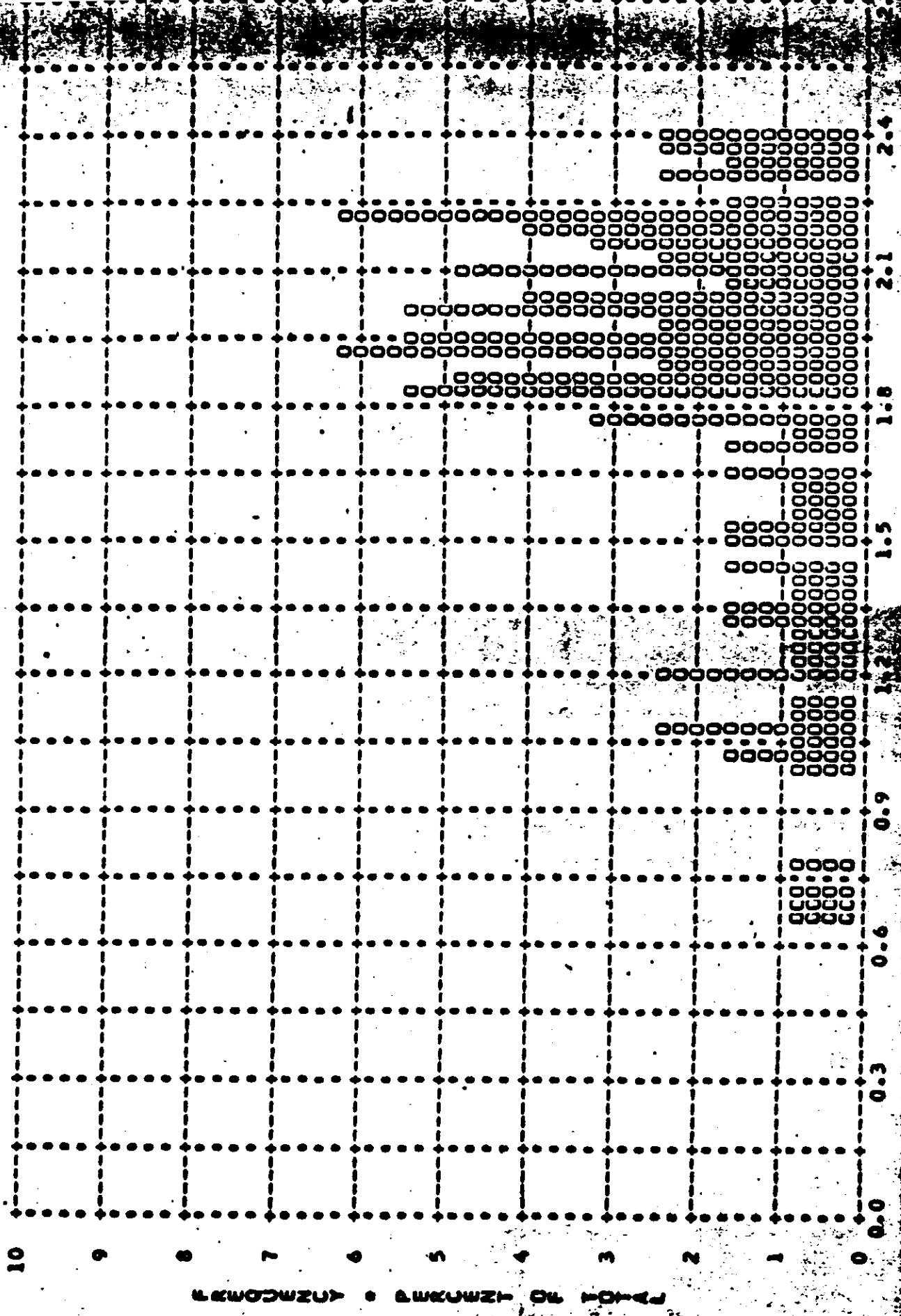


FIGURE A-15

CONTROL NO. [REDACTED]

~~TOP SECRET~~

MISSION • 1026-1 • INSTR • AFT • 12/28/65 PLOT OF 0 MIN • TERRAIN • PROCESSING • ALL LEVELS
ARITH MEAN • 0.39 • MEDIAN • 0.34 • STD DEV • 0.16 • RANGE • 0.20 TO 1.16 WITH 240 SAMPLES

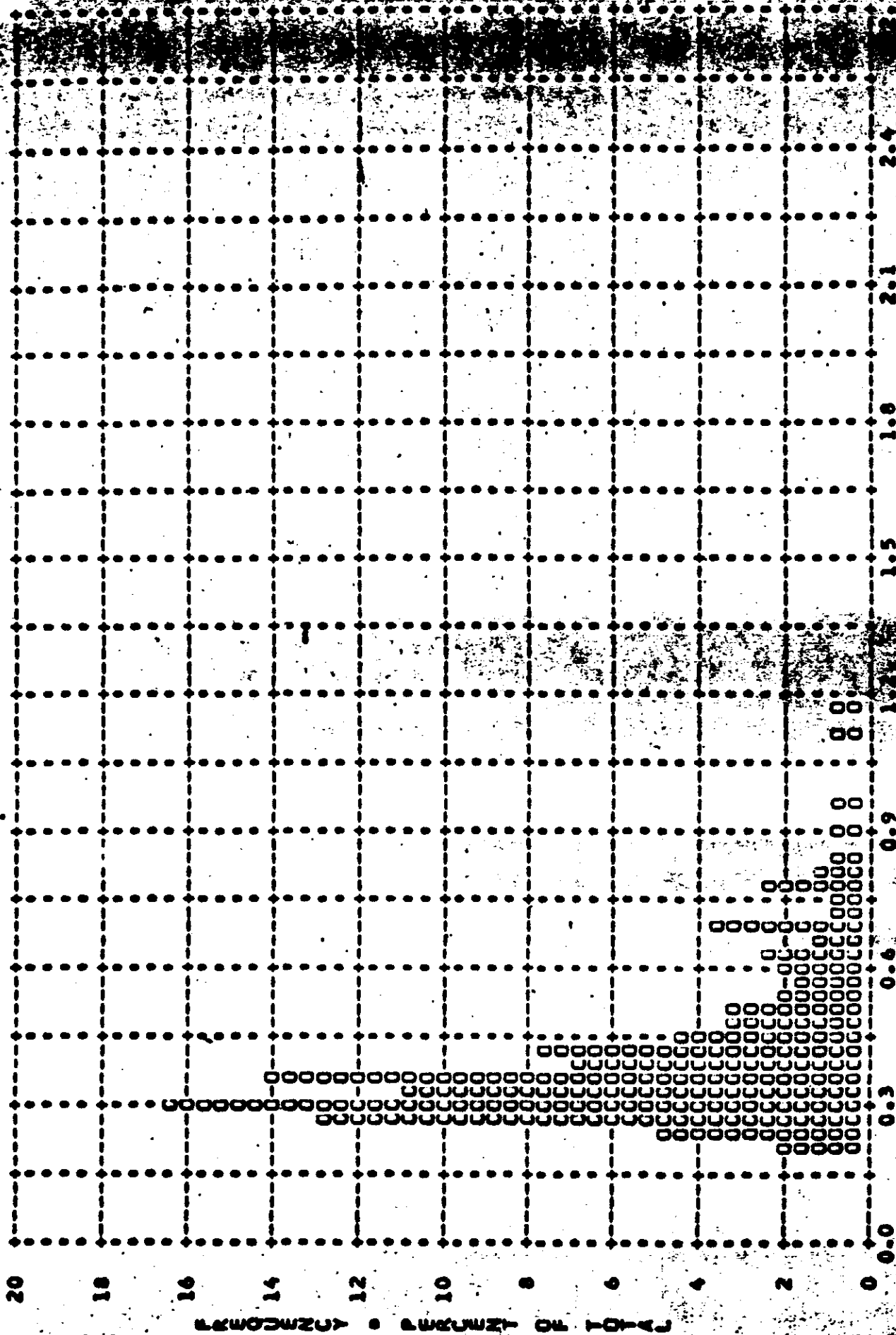


FIGURE A-16

~~TOP SECRET~~

- CONTROL NO.

MISSION • 1026-1 • INSTR • AFT • 12/28/65 PLOT OF D MAX • TERRAIN • PROCESSING • ALL LEVELS
ARITH MEAN • 1.29 • MEDIAN • 1.30 • STD DEV • 0.47 • RANGE • 0.24 TO 2.36 WITH 240 SAMPLES

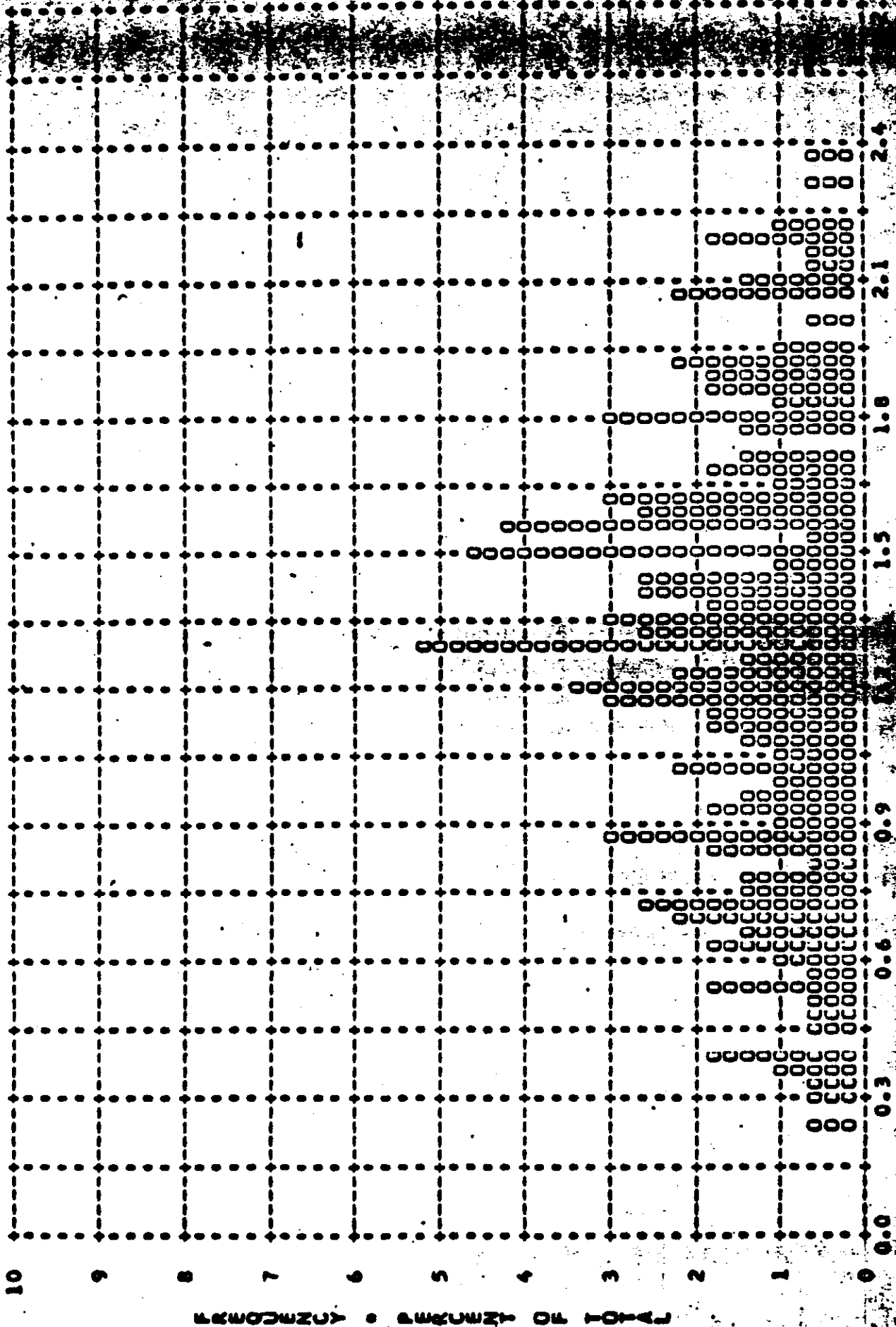


FIGURE A-17

TOP SECRET

CONTROL NO

MISSION • 1026-1 • INSTR • AFT • 12/28/65 PLOT OF D MAX • CLOUD • PROCESSING • ALL LEVELS
ARITH MEAN • 1.78 • MEDIAN • 1.86 • STD DEV • 0.40 • RANGE • 0.37 TO 2.40 WITH 225 SAMPLES

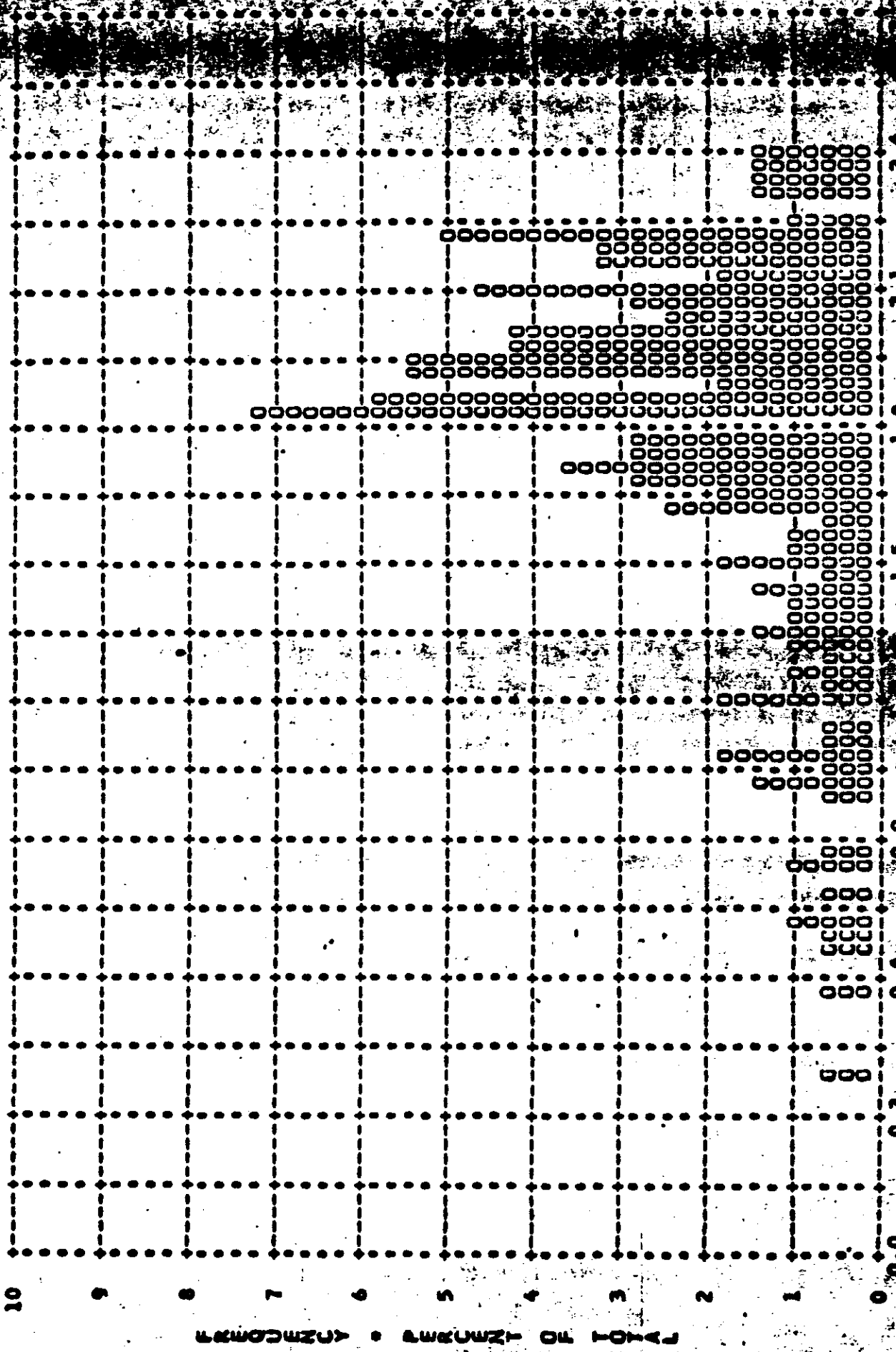


FIGURE A-18

DENSITY

TOP SECRET

DENSITY VALUE	PRIMARY			INTERMEDIATE			HIGH			ALL LEVEL											
	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN									
00.00	000	000	000	000	000	000	000	000	000	000	000	000									
00.01	000	000	000	000	000	000	000	000	000	000	000	000									
00.02	000	000	000	000	000	000	000	000	000	000	000	000									
00.03	000	000	000	000	000	000	000	000	000	000	000	000									
00.04	000	000	000	000	000	000	000	000	000	000	000	000									
00.05	000	000	000	000	000	000	000	000	000	000	000	000									
00.06	000	000	000	000	000	000	000	000	000	000	000	000									
00.07	000	000	000	000	000	000	000	000	000	000	000	000									
00.08	000	000	000	000	000	000	000	000	000	000	000	000									
00.09	000	000	000	000	000	000	000	000	000	000	000	000									
00.10	000	000	000	000	000	000	000	000	000	000	000	000									
00.11	000	000	000	000	000	000	000	000	000	000	000	000									
00.12	000	000	000	000	000	000	000	000	000	000	000	000									
00.13	000	000	000	000	000	000	000	000	000	000	000	000									
00.14	000	000	000	000	000	000	000	000	000	000	000	000									
00.15	000	000	000	000	000	000	000	000	000	000	000	000									
00.16	000	000	000	000	000	000	000	000	000	000	000	000									
00.17	000	000	000	000	000	000	000	000	000	000	000	000									
00.18	000	000	000	000	000	000	000	000	000	000	000	000									
00.19	000	000	000	000	000	000	000	000	000	000	000	000									
00.20	000	000	000	000	000	000	000	000	000	000	000	000									
00.21	000	000	000	000	000	000	000	000	000	000	000	000									
00.22	000	000	000	000	000	000	000	000	000	000	000	000									
00.23	000	000	000	000	000	000	000	000	000	000	000	000									
00.24	000	000	000	000	000	000	000	000	000	000	000	000									
00.25	000	000	000	000	000	000	000	000	000	000	000	000									
00.26	000	000	000	000	000	000	000	000	000	000	000	000									
00.27	000	000	000	000	000	000	000	000	000	000	000	000									
00.28	000	000	000	000	000	000	000	000	000	000	000	000									
00.29	000	000	000	000	000	000	000	000	000	000	000	000									
00.30	000	000	000	000	000	000	000	000	000	000	000	000									
00.31	000	000	000	000	000	000	000	000	000	000	000	000									
00.32	000	000	000	000	000	000	000	000	000	000	000	000									
00.33	000	000	000	000	000	000	000	000	000	000	000	000									
00.34	000	000	000	000	000	000	000	000	000	000	000	000									
00.35	000	000	000	000	000	000	000	000	000	000	000	000									
00.36	000	000	000	000	000	000	000	000	000	000	000	000									
00.37	000	000	000	000	000	000	000	000	000	000	000	000									
00.38	000	000	000	000	000	000	000	000	000	000	000	000									
00.39	000	000	000	000	000	000	000	000	000	000	000	000									
00.40	000	000	000	000	000	000	000	000	000	000	000	000									
00.41	000	000	000	000	000	000	000	000	000	000	000	000									
00.42	000	000	000	000	000	000	000	000	000	000	000	000									
00.43	000	000	000	000	000	000	000	000	000	000	000	000									
00.44	000	000	000	000	000	000	000	000	000	000	000	000									
00.45	000	000	000	000	000	000	000	000	000	000	000	000									
00.46	000	000	000	000	000	000	000	000	000	000	000	000									
00.47	000	000	000	000	000	000	000	000	000	000	000	000									
00.48	000	000	000	000	000	000	000	000	000	000	000	000									
00.49	000	000	000	000	000	000	000	000	000	000	000	000									
00.50	000	000	000	000	000	000	000	000	000	000	000	000									
SUBTOTAL							198			33			203			3			100		

TOP SECRET

CONTROL NO.

TABLE A-3

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVEL		
	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN
100												
101												
102												
103												
104												
105												
106												
107												
108												
109												
110												
111												
112												
113												
114												
115												
116												
117												
118												
119												
120												
121												
122												
123												
124												
125												
126												
127												
128												
129												
130												
131												
132												
133												
134												
135												
136												
137												
138												
139												
140												
141												
142												
143												
144												
145												
146												
147												
148												
149												
150												
151												
152												
153												
154												
155												
156												
157												
158												
159												
160												
161												
162												
163												
164												
165												
166												
167												
168												
169												
170												
171												
172												
173												
174												
175												
176												
177												
178												
179												
180												
181												
182												
183												
184												
185												
186												
187												
188												
189												
190												
191												
192												
193												
194												
195												
196												
197												
198												
199												
200												
SUBTOTAL												

TOP SECRET

CONTROL NO.

TABLE A-3

DENSITY VALUE	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN
.51	0	0	0	0	0	0	0	0	0	0	0	0
.52	0	0	0	0	0	0	0	0	0	0	0	0
.53	0	0	0	0	0	0	0	0	0	0	0	0
.54	0	0	0	0	0	0	0	0	0	0	0	0
.55	0	0	0	0	0	0	0	0	0	0	0	0
.56	0	0	0	0	0	0	0	0	0	0	0	0
.57	0	0	0	0	0	0	0	0	0	0	0	0
.58	0	0	0	0	0	0	0	0	0	0	0	0
.59	0	0	0	0	0	0	0	0	0	0	0	0
.60	0	0	0	0	0	0	0	0	0	0	0	0
.61	0	0	0	0	0	0	0	0	0	0	0	0
.62	0	0	0	0	0	0	0	0	0	0	0	0
.63	0	0	0	0	0	0	0	0	0	0	0	0
.64	0	0	0	0	0	0	0	0	0	0	0	0
.65	0	0	0	0	0	0	0	0	0	0	0	0
.66	0	0	0	0	0	0	0	0	0	0	0	0
.67	0	0	0	0	0	0	0	0	0	0	0	0
.68	0	0	0	0	0	0	0	0	0	0	0	0
.69	0	0	0	0	0	0	0	0	0	0	0	0
.70	0	0	0	0	0	0	0	0	0	0	0	0
.71	0	0	0	0	0	0	0	0	0	0	0	0
.72	0	0	0	0	0	0	0	0	0	0	0	0
.73	0	0	0	0	0	0	0	0	0	0	0	0
.74	0	0	0	0	0	0	0	0	0	0	0	0
.75	0	0	0	0	0	0	0	0	0	0	0	0
.76	0	0	0	0	0	0	0	0	0	0	0	0
.77	0	0	0	0	0	0	0	0	0	0	0	0
.78	0	0	0	0	0	0	0	0	0	0	0	0
.79	0	0	0	0	0	0	0	0	0	0	0	0
.80	0	0	0	0	0	0	0	0	0	0	0	0
.81	0	0	0	0	0	0	0	0	0	0	0	0
.82	0	0	0	0	0	0	0	0	0	0	0	0
.83	0	0	0	0	0	0	0	0	0	0	0	0
.84	0	0	0	0	0	0	0	0	0	0	0	0
.85	0	0	0	0	0	0	0	0	0	0	0	0
.86	0	0	0	0	0	0	0	0	0	0	0	0
.87	0	0	0	0	0	0	0	0	0	0	0	0
.88	0	0	0	0	0	0	0	0	0	0	0	0
.89	0	0	0	0	0	0	0	0	0	0	0	0
.90	0	0	0	0	0	0	0	0	0	0	0	0
.91	0	0	0	0	0	0	0	0	0	0	0	0
.92	0	0	0	0	0	0	0	0	0	0	0	0
.93	0	0	0	0	0	0	0	0	0	0	0	0
.94	0	0	0	0	0	0	0	0	0	0	0	0
.95	0	0	0	0	0	0	0	0	0	0	0	0
.96	0	0	0	0	0	0	0	0	0	0	0	0
.97	0	0	0	0	0	0	0	0	0	0	0	0
.98	0	0	0	0	0	0	0	0	0	0	0	0
.99	0	0	0	0	0	0	0	0	0	0	0	0
.00	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	0	0	0	0	0	0	0	0

~~TOP SECRET~~ [REDACTED] CONTROL NO. [REDACTED]

TABLE A-3

DENSITY VALUE PRIMARY INTERMEDIATE ALL LEVEL

DENSITY VALUE	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN
01	0	0	0	0	0	0	0	0	0	0	0	0
02	0	0	0	0	0	0	0	0	0	0	0	0
03	0	0	0	0	0	0	0	0	0	0	0	0
04	0	0	0	0	0	0	0	0	0	0	0	0
05	0	0	0	0	0	0	0	0	0	0	0	0
06	0	0	0	0	0	0	0	0	0	0	0	0
07	0	0	0	0	0	0	0	0	0	0	0	0
08	0	0	0	0	0	0	0	0	0	0	0	0
09	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0	0
45	0	0	0	0	0	0	0	0	0	0	0	0
46	0	0	0	0	0	0	0	0	0	0	0	0
47	0	0	0	0	0	0	0	0	0	0	0	0
48	0	0	0	0	0	0	0	0	0	0	0	0
49	0	0	0	0	0	0	0	0	0	0	0	0
50	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	0	0	0	0	0	0	0	0

~~TOP SECRET~~

CONTROL NO. [REDACTED]

TABLE A-3

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL LEVELS			ALL LEVELS		
	MIN	MAX	CIN	MIN	MAX	CIN	MIN	MAX	CIN	MIN	MAX	CIN
.51	0	0	0	0	0	0	0	0	0	0	0	0
.52	0	0	0	0	0	0	0	0	0	0	0	0
.53	0	0	0	0	0	0	0	0	0	0	0	0
.54	0	0	0	0	0	0	0	0	0	0	0	0
.55	0	0	0	0	0	0	0	0	0	0	0	0
.56	0	0	0	0	0	0	0	0	0	0	0	0
.57	0	0	0	0	0	0	0	0	0	0	0	0
.58	0	0	0	0	0	0	0	0	0	0	0	0
.59	0	0	0	0	0	0	0	0	0	0	0	0
.60	0	0	0	0	0	0	0	0	0	0	0	0
.61	0	0	0	0	0	0	0	0	0	0	0	0
.62	0	0	0	0	0	0	0	0	0	0	0	0
.63	0	0	0	0	0	0	0	0	0	0	0	0
.64	0	0	0	0	0	0	0	0	0	0	0	0
.65	0	0	0	0	0	0	0	0	0	0	0	0
.66	0	0	0	0	0	0	0	0	0	0	0	0
.67	0	0	0	0	0	0	0	0	0	0	0	0
.68	0	0	0	0	0	0	0	0	0	0	0	0
.69	0	0	0	0	0	0	0	0	0	0	0	0
.70	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	0	0	0	0	0	0	0	0
TOTAL	0	0	0	12	12	26	224	224	215	236	236	241

MISSION 1026-2 INSTR - FRWD 12/28/65 PROCESSING AND EXPOSURE ANALYSIS

PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0	0 PC	0 PC	0 PC	0 PC	0 PC
INTERMEDIATE	12	0 PC	33 PC	58 PC	8 PC	0 PC
FULL	224	82 PC	0 PC	17 PC	1 PC	0 PC
ALL LEVELS	236	78 PC	2 PC	19 PC	1 PC	0 PC

PROCESS LEVEL	BASE + FOG	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0.01-0.09	0.01-0.13	0.14-0.39	0.40-0.90	-----	0.91 AND UP
INTERMED	0.10-0.17	0.01-0.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35 AND UP
FULL	0.18 AND UP	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70 AND UP

TOP SECRET



CONTROL NO.



TABLE A-3

~~TOP SECRET~~

CONTROL NO.

MISSION • 1026-2 • INSTR • FRWD • 12/28/65 PLOT OF 0 MIN • TERRAIN • PROCESSING • INTERMEDIATE
ARITH MEAN • 0.54 • MEDIAN • 0.55 • STD DEV • 0.26 • RANGE • 0.23 TO 1.21 WITH 12 SAMPLES

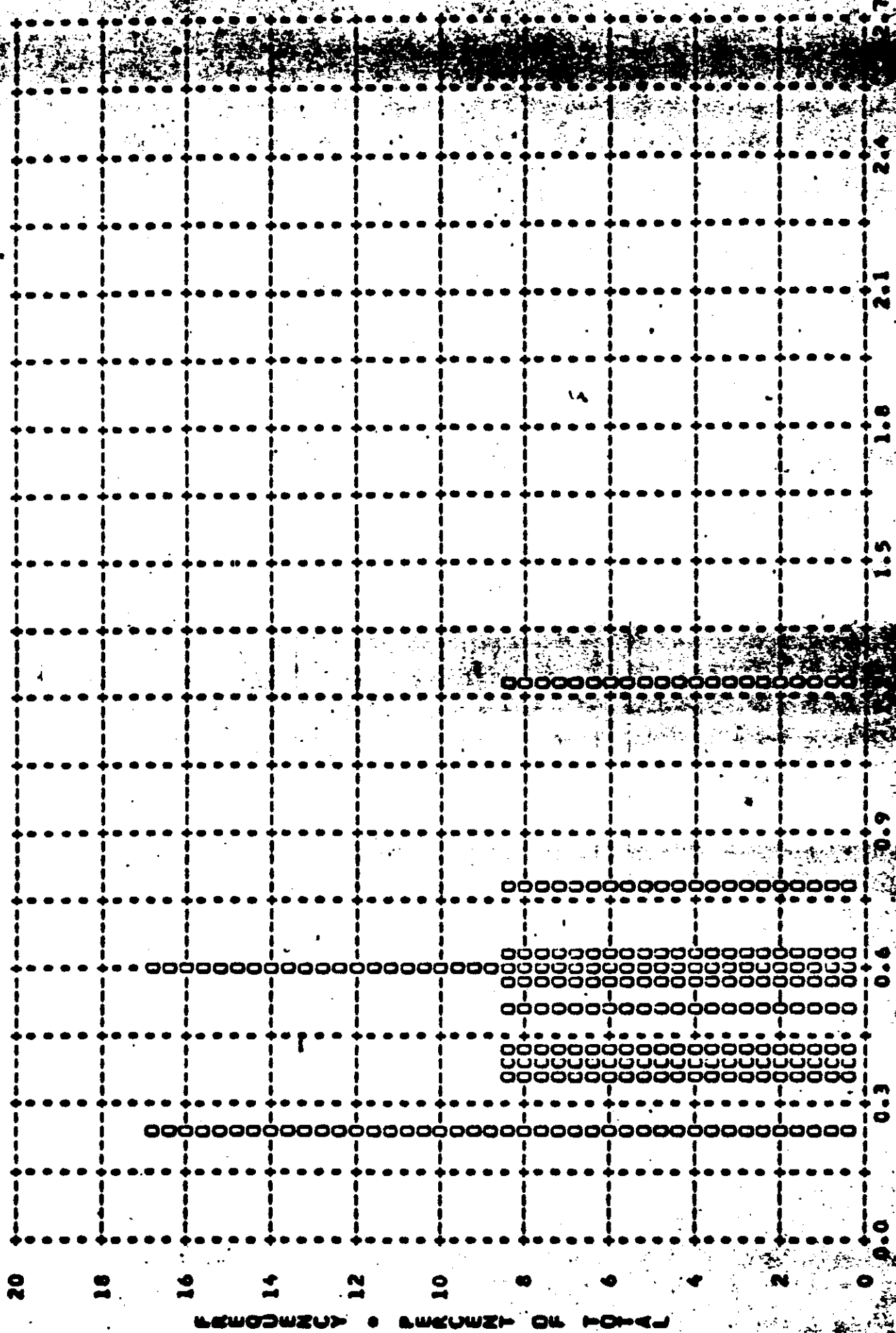


FIGURE A-19

TOP SECRET

CL.ROL NO.

MISSION • 1026-2 • INSTR • FRMD • 12/28/65 PLOT OF U MAX • TERRAIN • PROCESSING • INTERMEDIATE
ARITH MEAN • 1.32 • MEDIAN • 1.50 • STD DEV • 0.35 • RANGE • 0.65 TO 1.79 WITH 12 SAMPLES

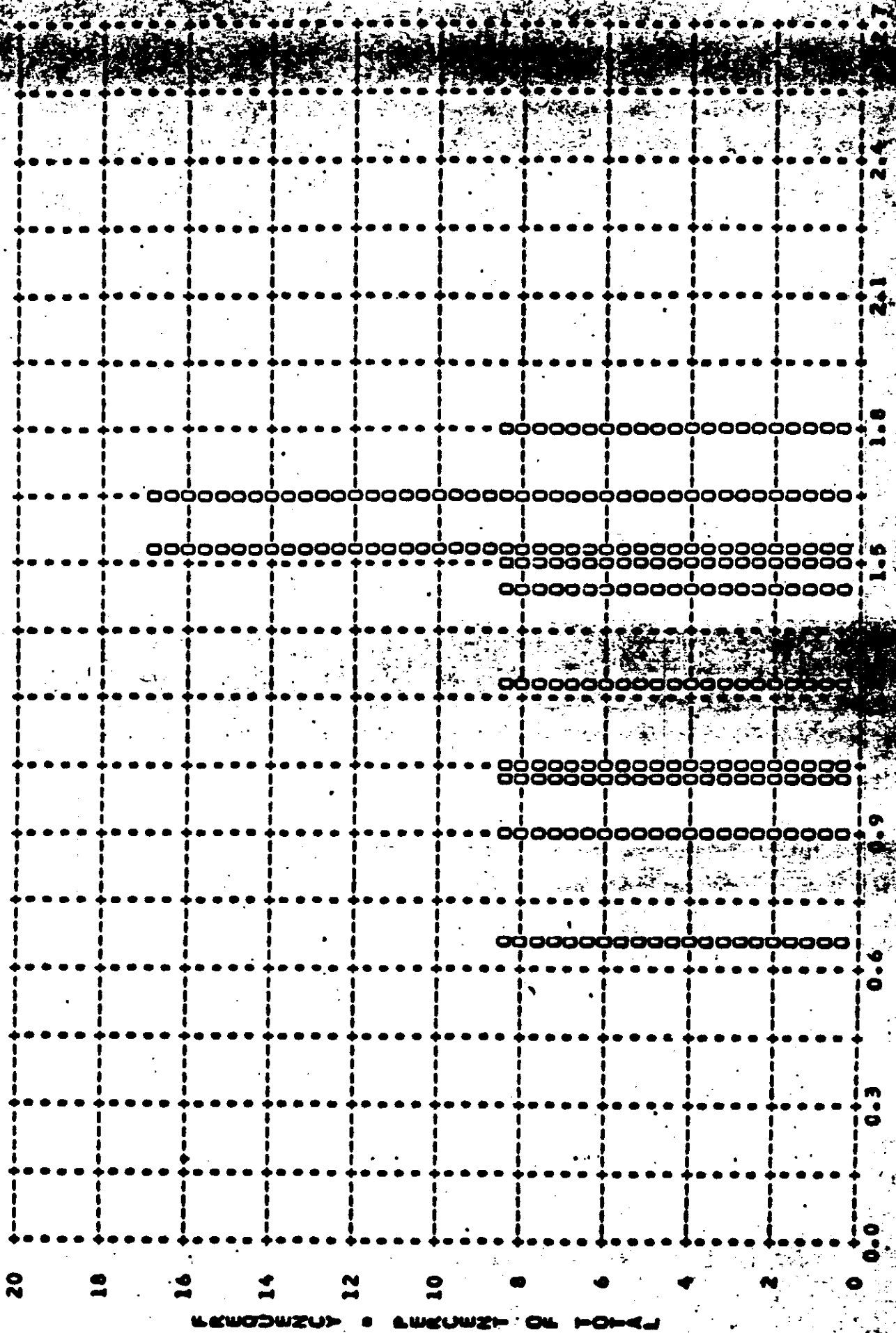


FIGURE A-20

TOP SECRET

CL.ROL NO.

TOP SECRET

CONTROL NO.

MISSION • 1026-2 • INSTR • FRWD • 12/28/65 PLOT OF D MAX • CLOUD • PROCESSING • INTERMEDIATE
ARITH MEAN • 1.49 • MEDIAN • 1.56 • STD DEV • 0.32 • RANGE • 0.94 TO 2.14 WITH 26 SAMPLES

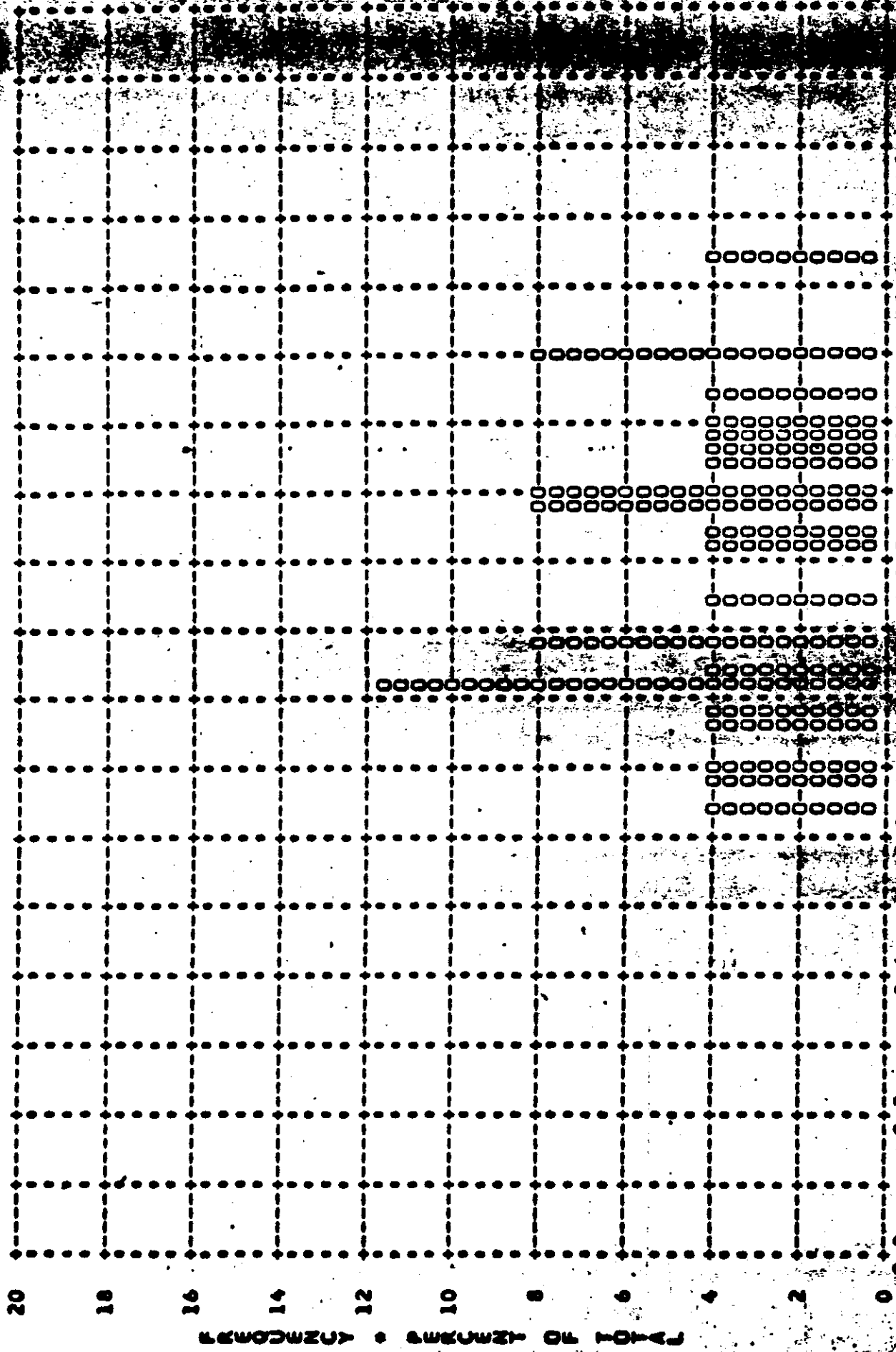


FIGURE A-21

TOP SECRET

TOP SECRET

C. ROL NO.

MISSION • 1026-2 • INSTR • FRWD • 12/28/65 PLOT OF D MIN • TERRAIN • PROCESSING • FULL
ARITH MEAN • 0.35 • MEDIAN • 0.30 • STD DEV • 0.14 • RANGE • 0.19 TO 1.32 WITH 224 SAMPLES

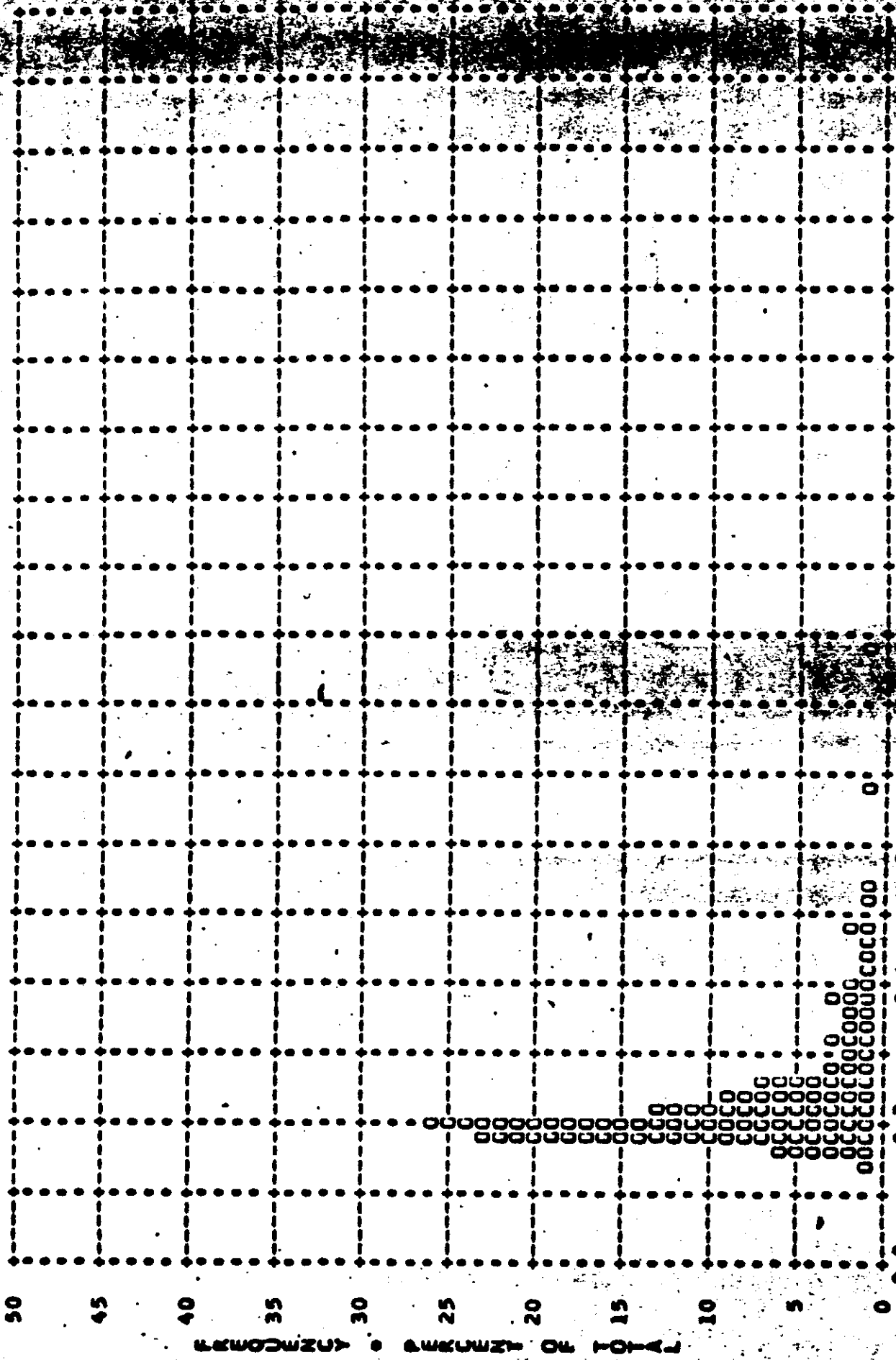


FIGURE A-22

DENSITY

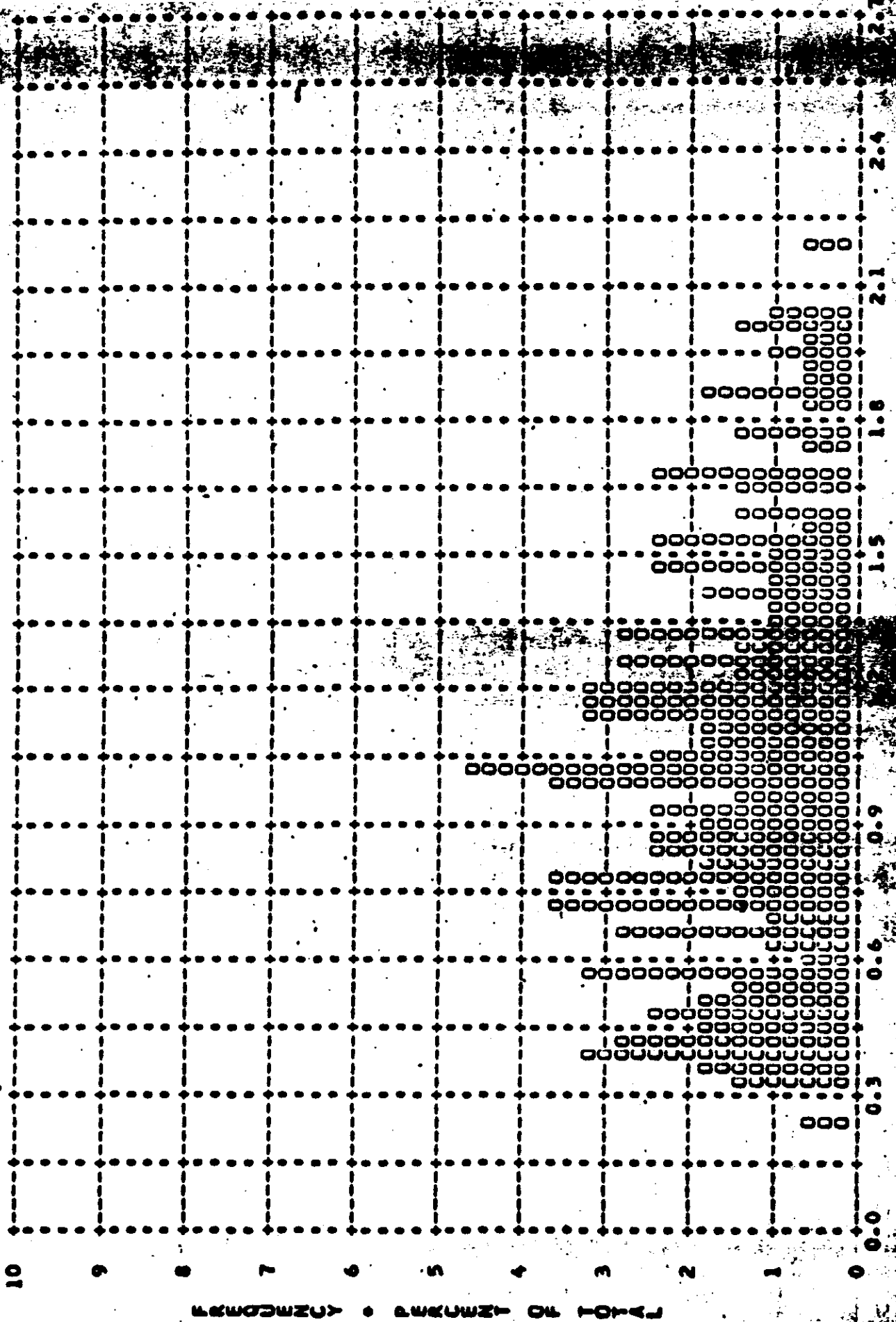
TOP SECRET

C. ROL NO.

TOP SECRET

CONTROL NO.

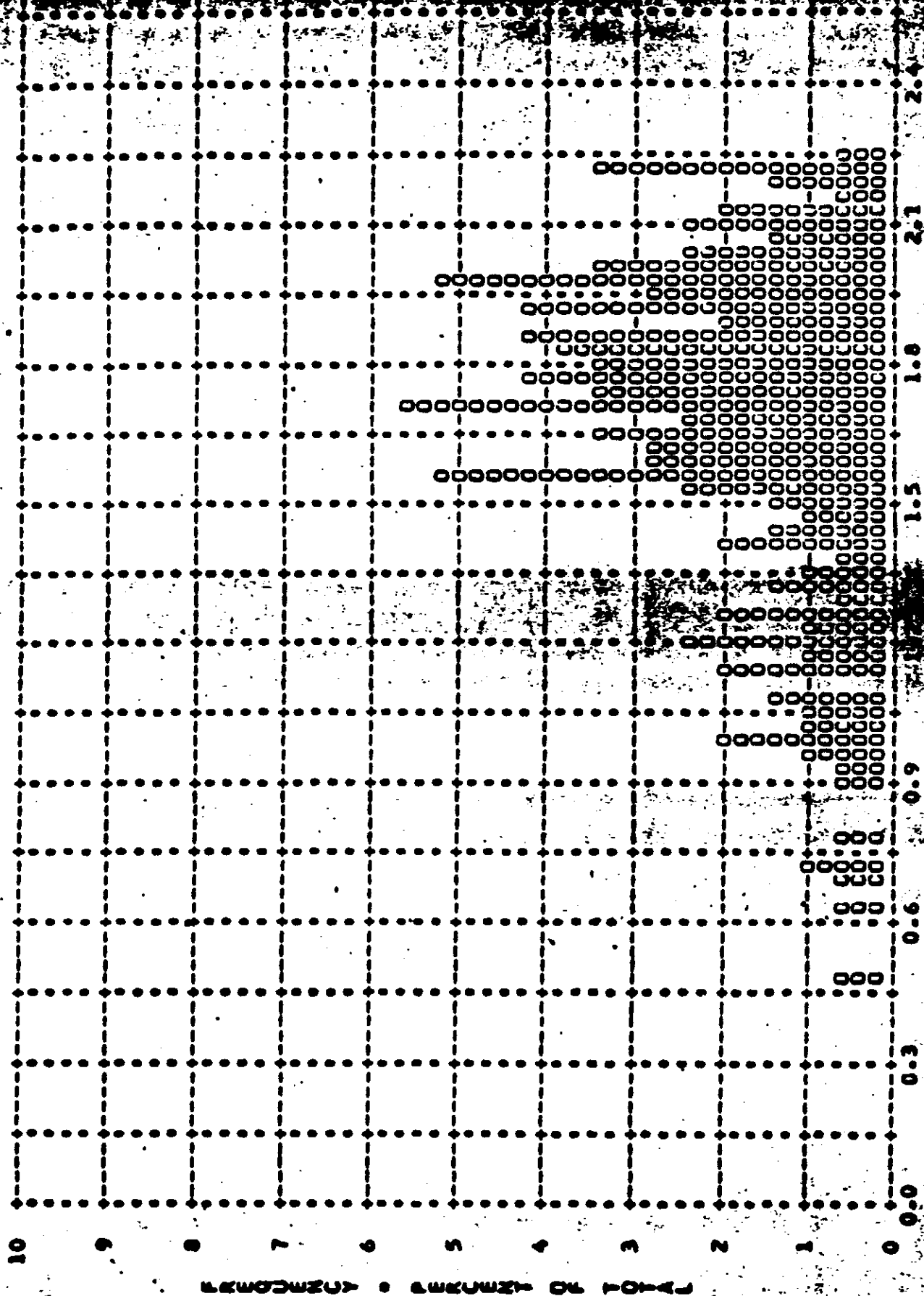
MISSION • 1026-2 • INSTR • FRWD • 12/28/65 PLOT OF D MAX • TERRAIN • PROCESSING • FULL
ARITH MEAN • 1.03 • MEDIAN • 1.01 • STD DEV • 0.45 • RANGE • 0.23 TO 2.17 WITH 224 SAMPLES



TOP SECRET

CONFIDENTIAL NO.

MISSION • 1026-2 • INSTR • FRMD • 12/28/65 PLOT OF 0 MAX • CLOUD • PROCESSING • FULL
ARITH MEAN • 1.65 • MEDIAN • 1.71 • STD DEV • 0.36 • RANGE • 0.48 TO 2.24 WITH 215 SAMPLES



FREQUENCY • TOTAL

TOP SECRET

CONTROL NO.

MISSION • 1026-2 • INSTR • FRWD • 12/28/65 PLOT OF D MIN • TERRAIN • PROCESSING • ALL LEVELS
ARITH MEAN • 0.36 • MEDIAN • 0.30 • STD DEV • 0.15 • RANGE • 0.19 TO 1.32 WITH 236 SAMPLES.

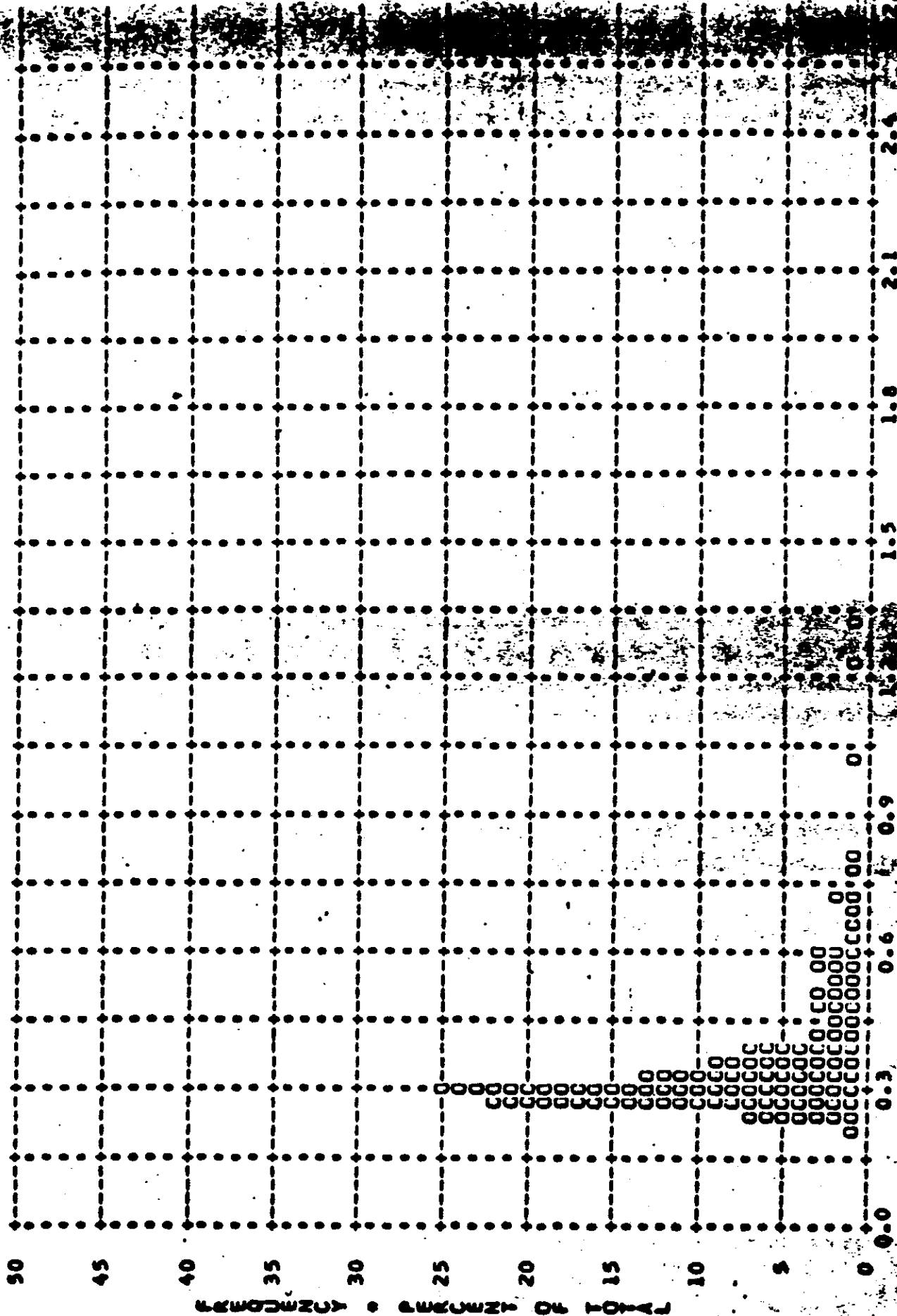


FIGURE A-25

TOP SECRET

CONTROL NO.

MISSION • 1026-2 • INSTR • FRWD • 12/28/65 PLOT OF D MAX • TERRAIN • PROCESSING • ALL LEVELS
ARITH MEAN • 1.05 • MEDIAN • 1.02 • STD DEV • 0.45 • RANGE • 0.23 TO 2.17 WITH 236 SAMPLES

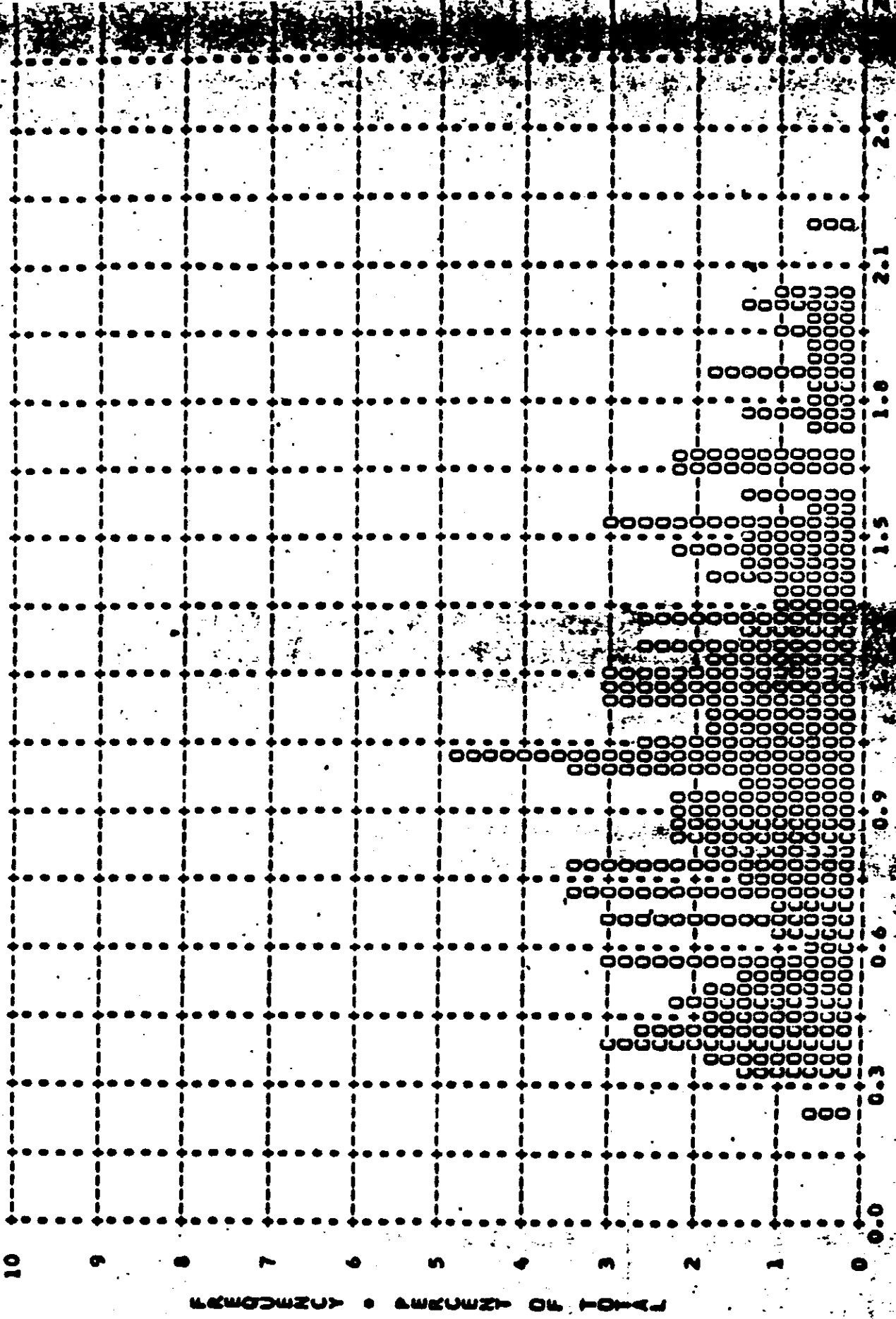


FIGURE A-26

TOP SECRET

CONFIDENTIAL NO.

MISSION • 1026-2 • INSTR • FRWD • 12/28/65 PLOT OF D MAX • CLOUD • PROCESSING • ALL LEVELS
ARITH MEAN • 1.63 • MEDIAN • 1.70 • STD DEV • 0.36 • RANGE • 0.48 TO 2.24 WITH 241 SAMPLES

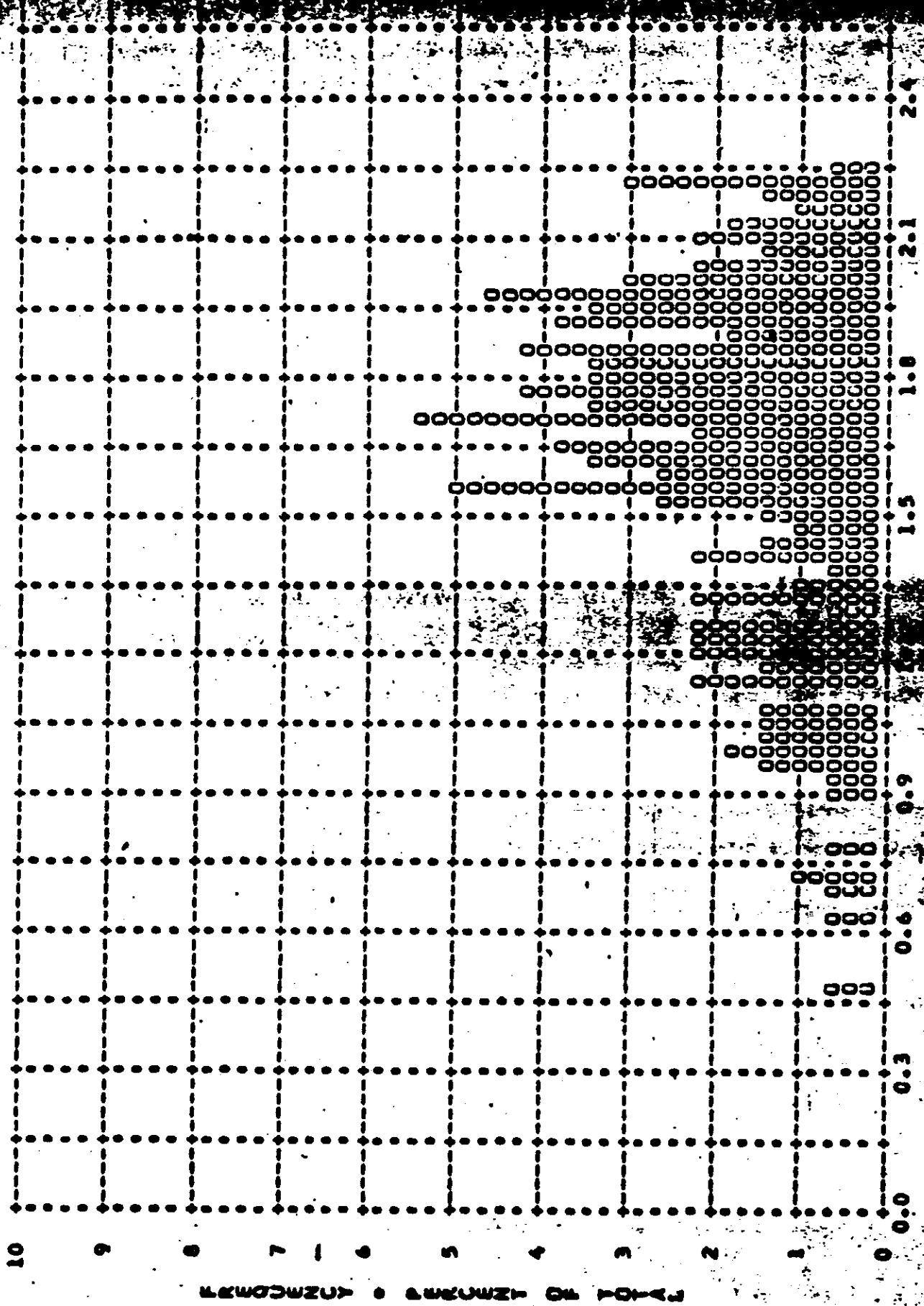


FIGURE A-27

TOP SECRET

SUB
TOTAL

TOP SECRET



CONTROL NO.



TABLE A-4

DENSITY VALUE	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN	MIN	MAX	LIN
0.51	0	0	0	0	0	0	0	0	0	0	0	0
0.52	0	0	0	0	0	0	0	0	0	0	0	0
0.53	0	0	0	0	0	0	0	0	0	0	0	0
0.54	0	0	0	0	0	0	0	0	0	0	0	0
0.55	0	0	0	0	0	0	0	0	0	0	0	0
0.56	0	0	0	0	0	0	0	0	0	0	0	0
0.57	0	0	0	0	0	0	0	0	0	0	0	0
0.58	0	0	0	0	0	0	0	0	0	0	0	0
0.59	0	0	0	0	0	0	0	0	0	0	0	0
0.60	0	0	0	0	0	0	0	0	0	0	0	0
0.61	0	0	0	0	0	0	0	0	0	0	0	0
0.62	0	0	0	0	0	0	0	0	0	0	0	0
0.63	0	0	0	0	0	0	0	0	0	0	0	0
0.64	0	0	0	0	0	0	0	0	0	0	0	0
0.65	0	0	0	0	0	0	0	0	0	0	0	0
0.66	0	0	0	0	0	0	0	0	0	0	0	0
0.67	0	0	0	0	0	0	0	0	0	0	0	0
0.68	0	0	0	0	0	0	0	0	0	0	0	0
0.69	0	0	0	0	0	0	0	0	0	0	0	0
0.70	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	0	0	0	0	0	0	0	0
TOTAL	0	0	0	34	34	54	194	194	175	228	228	229

MISSION 1026-2 INSTR - AFT 12/28/65 PROCESSING AND EXPOSURE ANALYSIS

PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0	0 PC	0 PC	0 PC	0 PC	0 PC
INTERMEDIATE	34	0 PC	79 PC	12 PC	6 PC	10 PC
FULL	194	70 PC	0 PC	27 PC	2 PC	2 PC
ALL LEVELS	228	60 PC	12 PC	25 PC	3 PC	12 PC

PROCESS LEVEL	BASE + FOG	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	0.01-0.09	0.01-0.13	0.14-0.39	0.40-0.90	-----	0.91 AND UP
INTERMED	0.10-0.17	0.01-0.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35 AND UP
FULL	0.18 AND UP	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70 AND UP

~~TOP SECRET~~ [REDACTED] - CONTROL NO. [REDACTED]

TABLE A-4

TOP SECRET

██████████ - C. /ROL NO. ██████████

MISSION • 1026-2 • INSTR • AFT • 12/28/65 PLOT OF D MIN • TERRAIN • PROCESSING • INTERMEDIATE
ARITH MEAN • 0.42 • MEDIAN • 0.32 • STD DEV • 0.29 • RANGE • 0.22 TO 1.35 WITH 34 SAMPLES

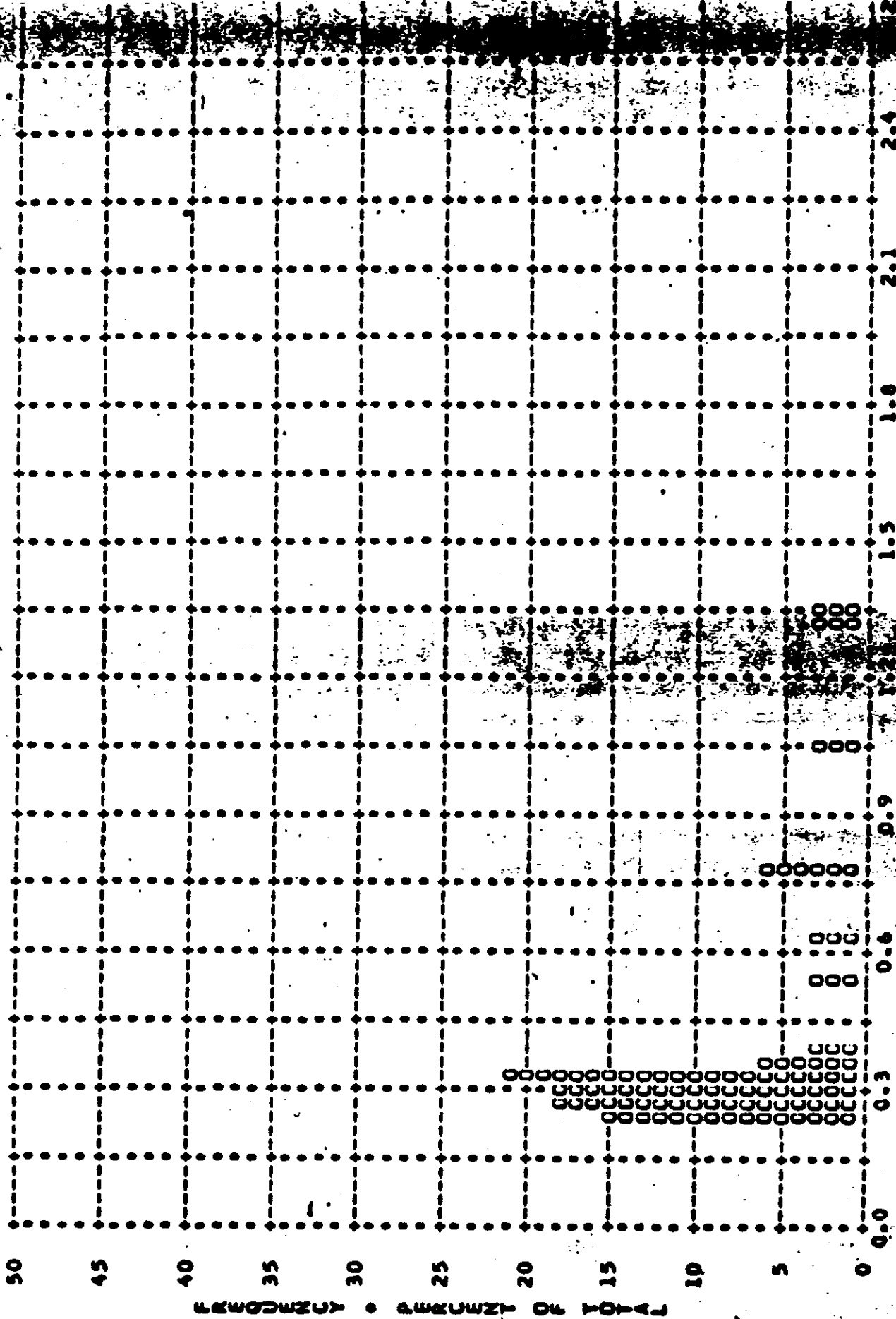


FIGURE A-28

TOP SECRET

CL-7ROL NO.

MISSION • 1026-2 • INSTR • AFT • 12/28/65 PLOT OF O MAX • TERRAIN • PROCESSING • INTERMED
ARITH MEAN • 1.11 • MEDIAN • 1.15 • STD DEV • 0.35 • RANGE • 0.37 TO 1.78 WITH 34 SAMPLES

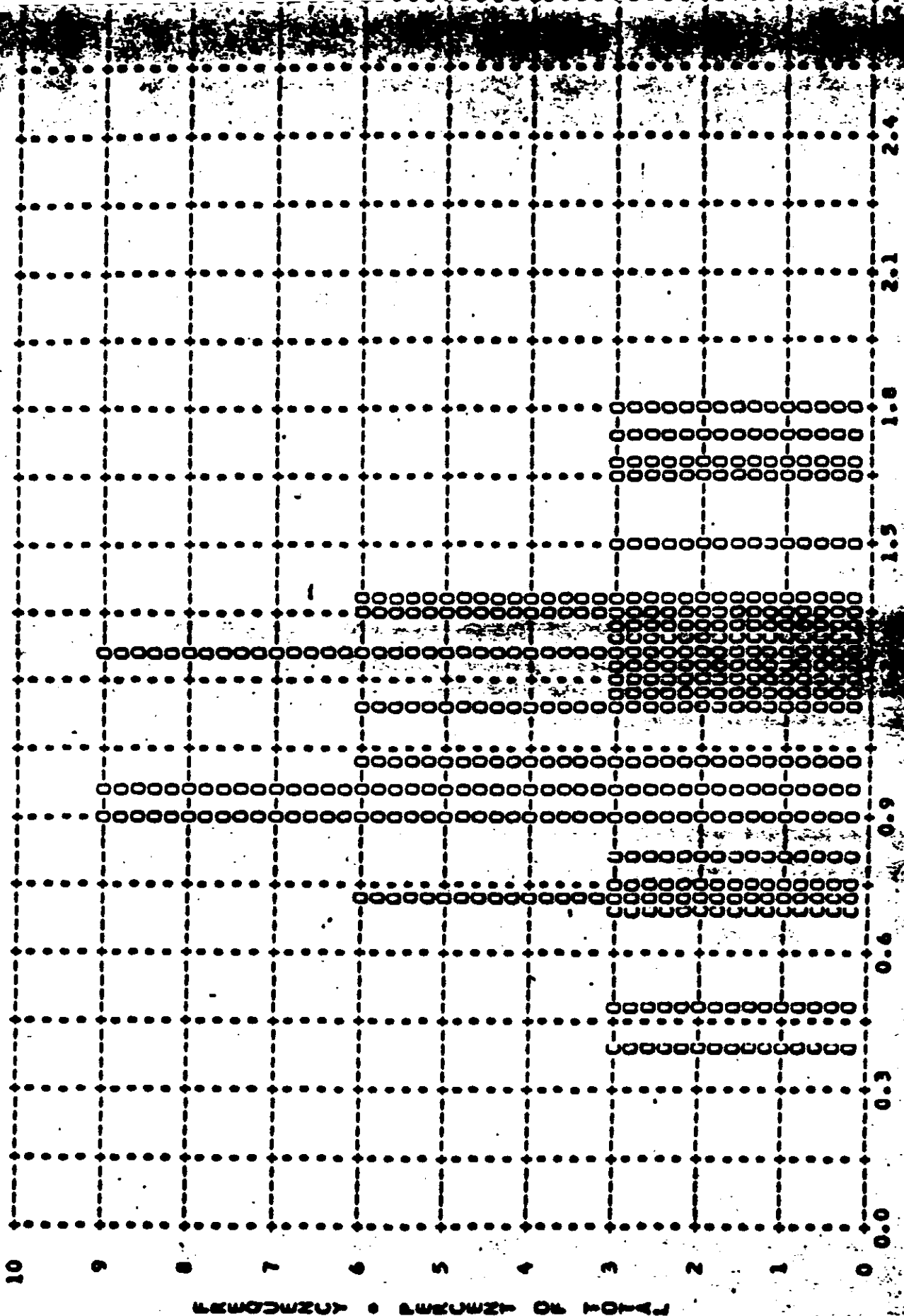


FIGURE A-20

TOP SECRET

CO. SOL NO.

MISSION • 1026-2 • INSTR • AFT • 12/28/65 PLOT OF O MAX • CLOUD • PROCESSING • INTERMED
ARITH MEAN • 1.78 • MEDIAN • 1.86 • STD DEV • 0.35 • RANGE • 0.80 TO 2.24 WITH 54 SAMPLES

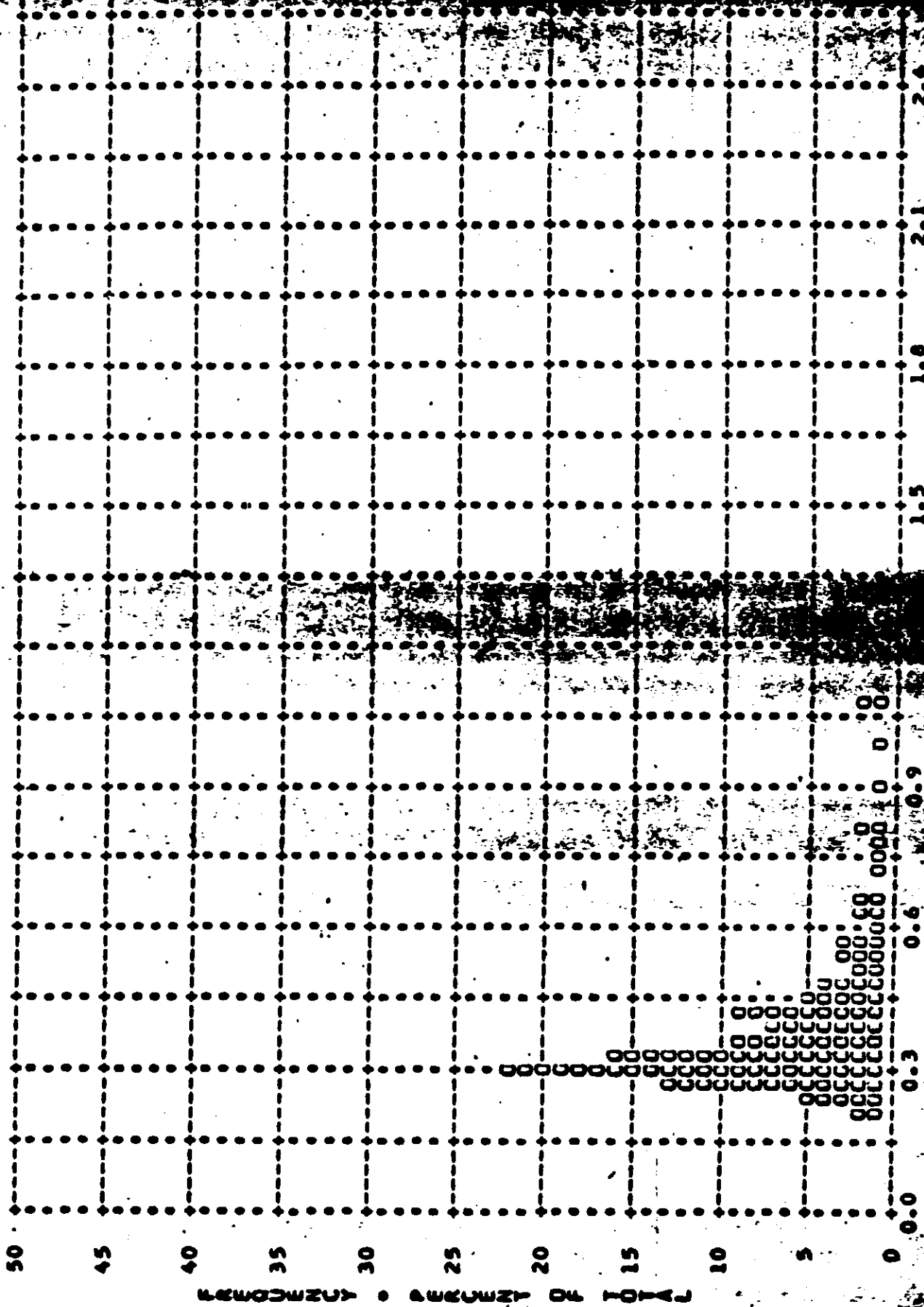


FIGURE A-30

TOP SECRET

CO. INCL. NO.

MISSION • 1026-2 • INSTR • AFI • 12/28/65 PLOT OF 0 MIN • TERRAIN • PROCESSING • FULL
ARITH MEAN • 0.38 • MEDIAN • 0.33 • STD DEV • 0.17 • RANGE • 0.21 TO 1.26 WITH 194 SAMPLES



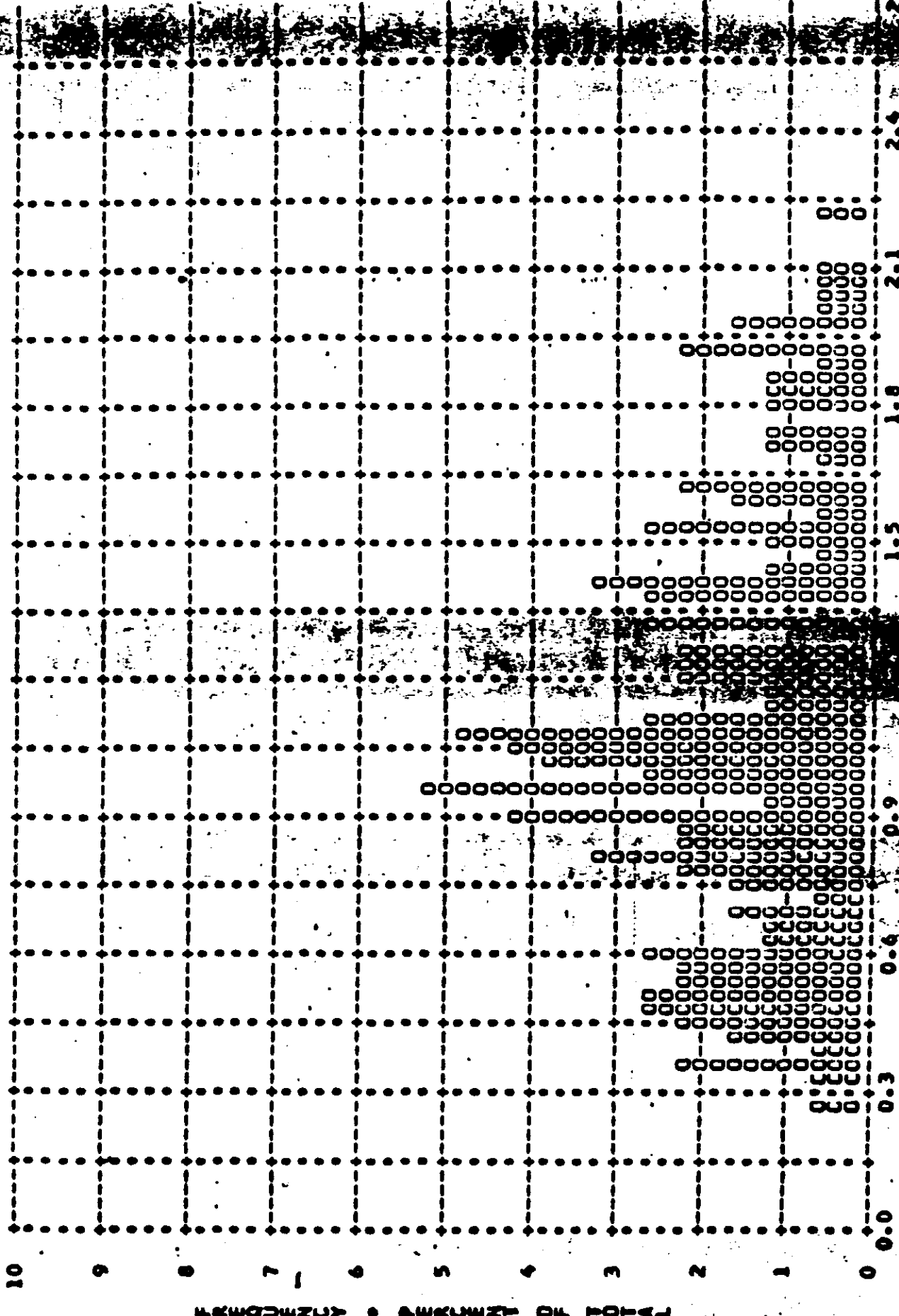
A-55

FIGURE A-31

TOP SECRET

CONTROL NO.

MISSION • 1026-2 • INSTR • AFT • 12/28/65 PLOT OF D MAX • TERRAIN • PROCESSING • FULL
ARITH MEAN • 1.07 • MEDIAN • 1.02 • STD DEV • 0.45 • RANGE • 0.27 TO 2.20 WITH 194 SAMPLES



FREQUENCY • D MAX

TOP SECRET

CL. NO.

MISSION • 1026-2 • INSTN • AFT • 12/28/65 PLOT OF D MAX • CLOUD • PROCESSING • FULL
ARITH MEAN • 1.55 • MEDIAN • 1.61 • STD DEV • 0.48 • RANGE • 0.30 TO 2.36 WITH 175 SAMPLES

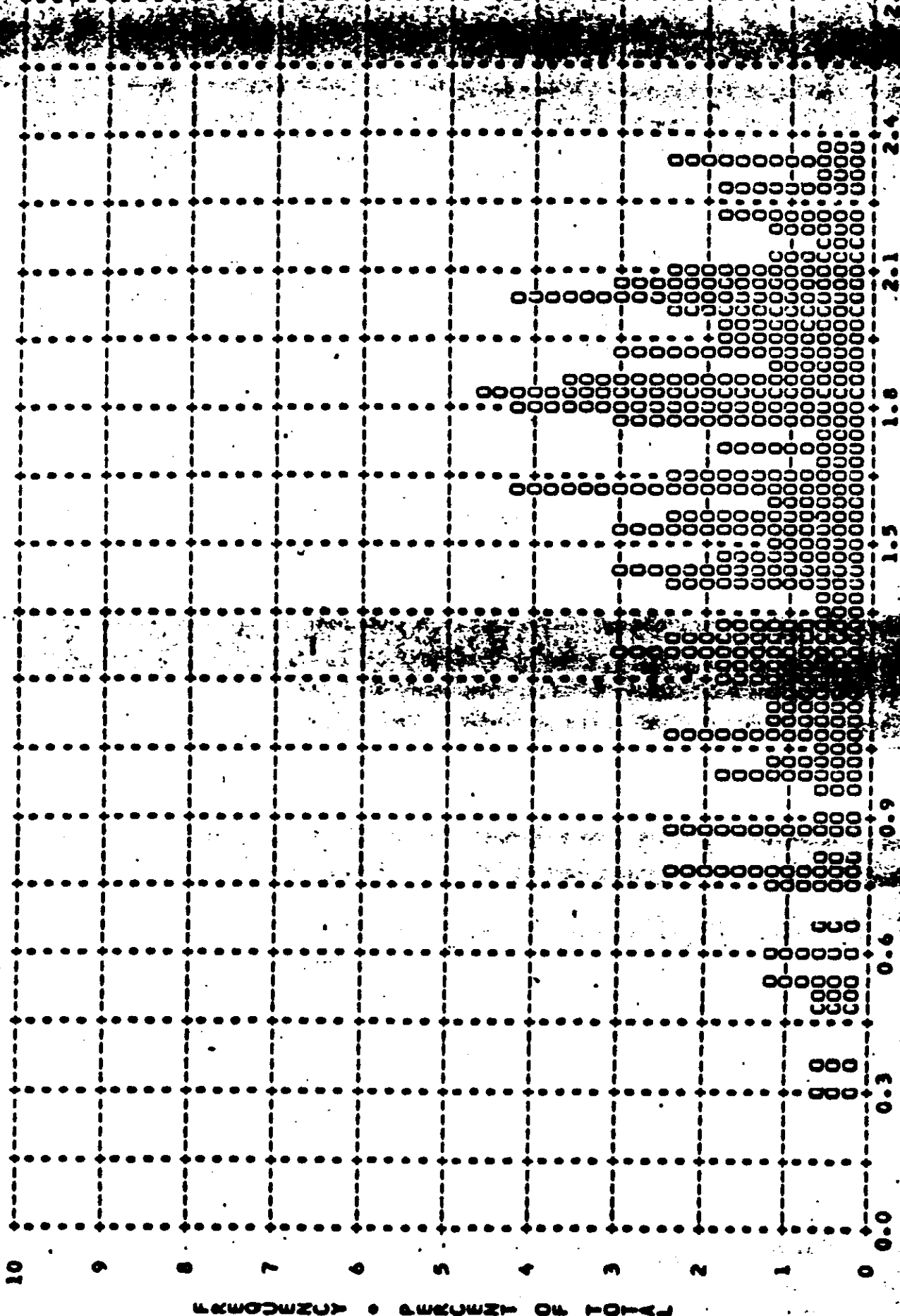


FIGURE A-33

~~TOP SECRET~~

██████████ - CU-190L NO.

MISSION • 1026-2 • INSTR • AFT • 12/28/65 PLOT OF 0 MIN • TERRAIN • PROCESSING • ALL LEVELS
ARITH MEAN • 0.39 • MEDIAN • 0.32 • STD DEV • 0.19 • RANGE • 0.21 TO 1.35 WITH 228 SAMPLES

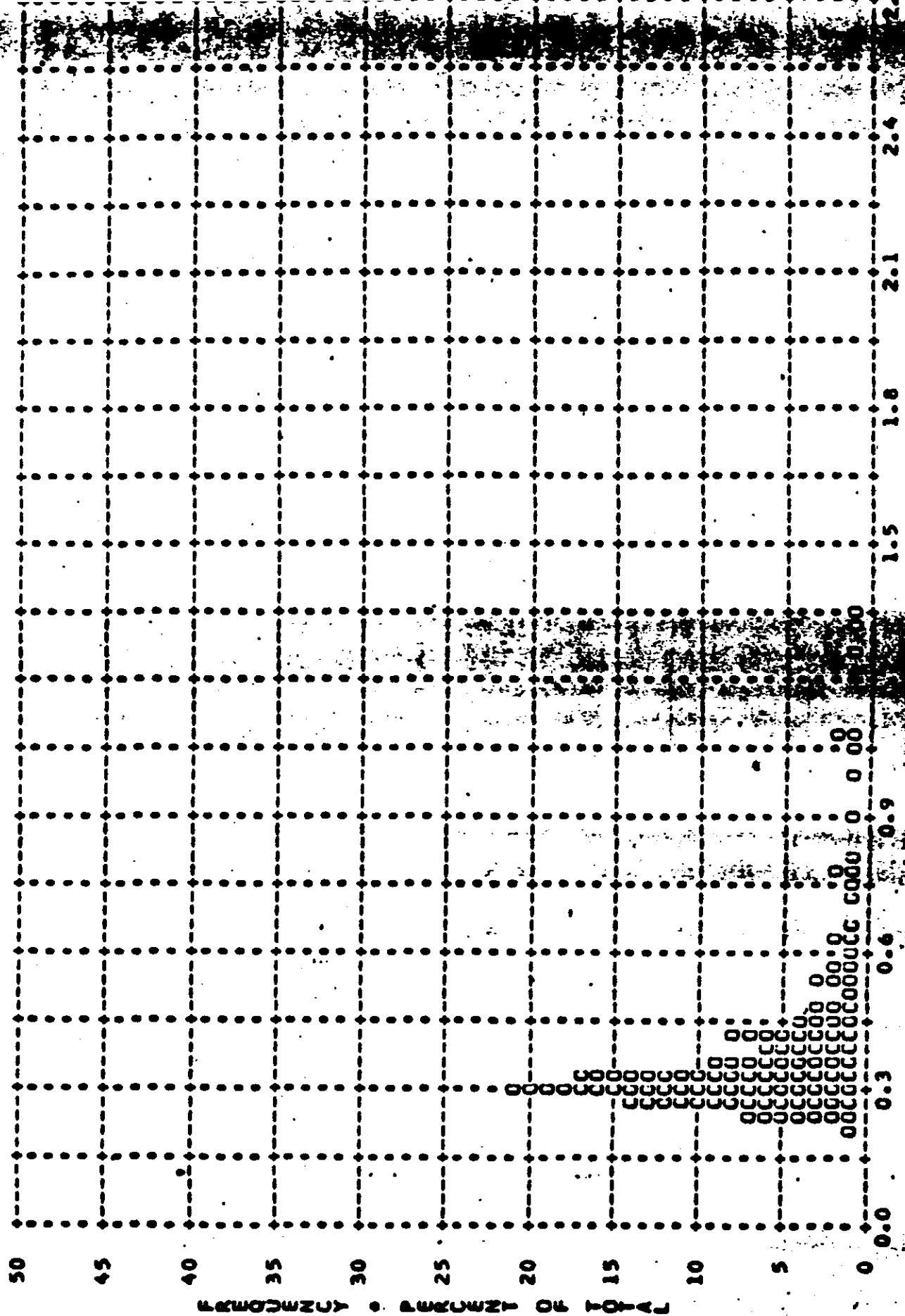


FIGURE A-34

TOP SECRET

CL. / ADL. NO.

MISSION • 1026-2 • INSTR • AFT • 12/28/65 PLOT OF D MAX • TERRAIN • PROCESSING • ALL LEVELS
ARITH MEAN • 1.08 • MEDIAN • 1.03 • STD DEV • 0.43 • RANGE • 0.27 TO 2.20 WITH 228 SAMPLES

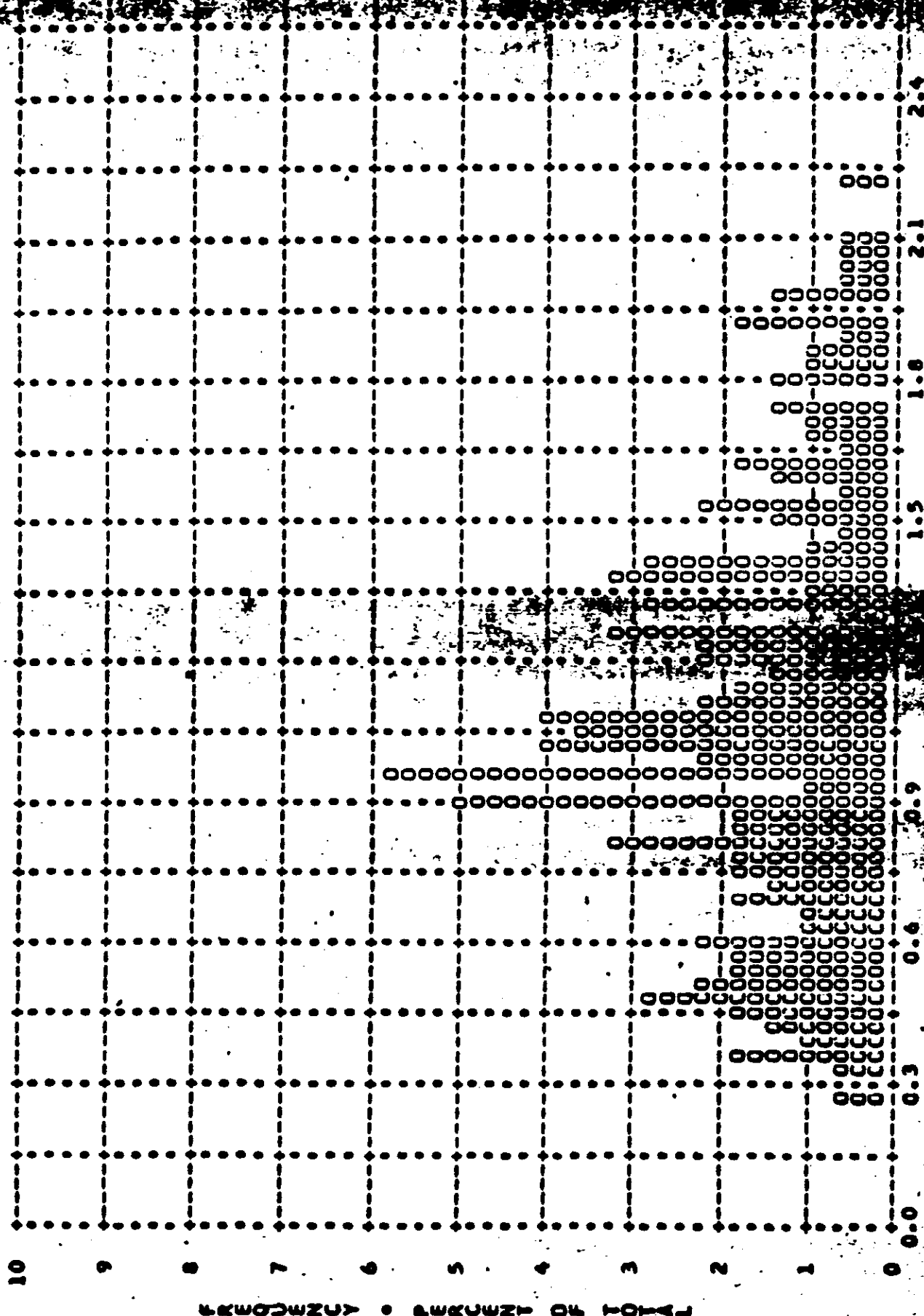
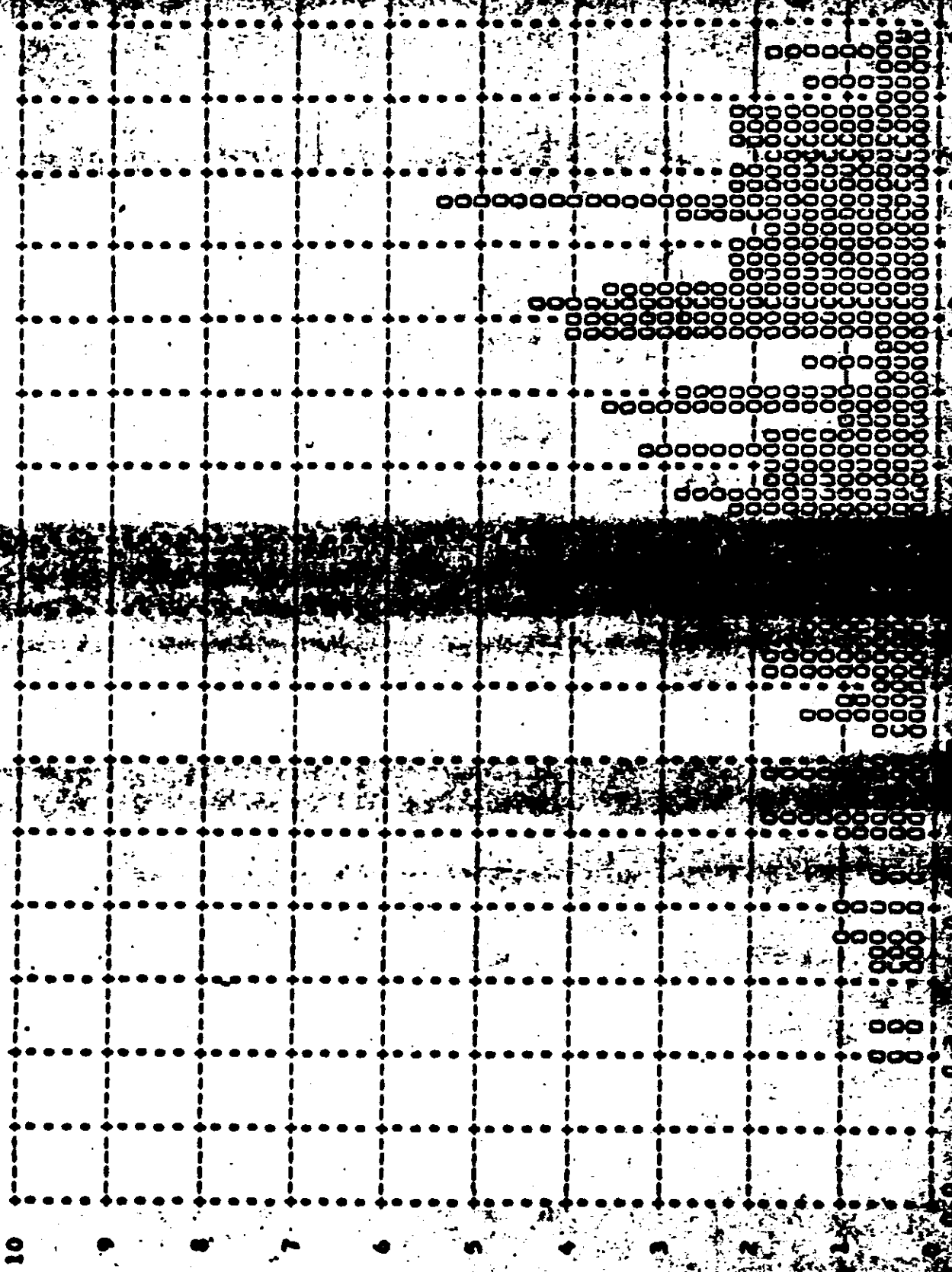


FIGURE A-35

TOP SECRET

MISSION • 1026-2 • INSTR • AFT 12/20/65 • D MAX • CLOUD • PROCESSING • ALL
ARITH MEAN • 1.61 • MEDIAN • 1.70 • STD DEV • 0.95 • RANGE • 0.30 TO 2.36 WITH 229 SAMPLES



12-20-65 1026-2

Distribution:

Copy No.

To

[REDACTED]

[REDACTED]